

APPENDIX 1: GANTT CHART

Table: Gantt chart for Final Year Project I

| NO | MONTH DETAIL | JULY | | AUGUST | | | | SEPTEMBER | | | | OCTOBER | | | | NOVEMBER | | | | |
|----|--|------|---|--------|---|---|---|--|---|---|----|---------|----|----|----|---|--|----|----|--|
| | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| 1. | SELECTION OF PROJECT | █ | | | | | | | | | | | | | | | | | | |
| 2. | PRELIMINARY PROJECT RESEARCH - Background study of project - Identify problem statement - Identify objectives - Literature review | █ | | | | | | M I D S E M E S T E R B R E A K | | | | | | | | | | | | |
| | | █ | | | | | | | █ | | | | | | | S T U D Y W E E K | F I N A L E X A M I N A T I O N | | | |
| 3. | PROJECT WORK - Determine ASTM standard - Determine empirical expression - Familiarize with ANSYS - Modeling specimen in ANSYS | | | █ | | █ | | | | | | | | | | | | | | |
| | | | | | | | | | █ | | | | | | | | | | | |
| 4. | SUBMISSION - Preliminary report - Progress report - Seminar - Interim report - Oral presentation | | | | | | | | | | | | | | | | | | | |
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Table: Gantt chart for Final Year Project II

| N O | MONTH DETAIL | JAN | | FEBRUARY | | | | MARCH | | | | APRIL | | | | MAY | | | |
|--------|---|-----|---|----------|---|---|---|-------|---|---|----|-------|----|----|----|-----|---|--|----|
| | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 |
| 1. | EVALUATION OF FYP I | ■ | | | | | | | M I D S E M E S T E R | | | | | | | | S T U D Y W E E K | F I N A L E X A M I N A T I O N | |
| 2. | PROJECT WORK CONTINUE - Design graph of Stress Intensity Factor vs $\frac{a}{W}$ from 0.45 to 0.55 -Design graph of Stress Intensity Factor vs $\frac{W}{B}$ from 2.0 to 4.0 | ■ | | | | | | | | | ■ | | | | | | | | |
| 3. | ANALYSES - Analyses result and further recommendation of the project | | | | | | | | | | ■ | | | | | | | | |
| 4. | SUBMISSION - Progress Report I - Progress Report II - Seminar - Poster Submission - Dissertation (Soft bound) - Oral Presentation - Dissertation (Hardbound) | | | | ● | | | ● | | | ● | | ● | | | | | | |

APPENDIX 2:
PROCEDURE IN USING ANSYS
SOFTWARE

In order to using KCALC command for plane strain analysis. Several steps and procedures must be followed in order to conduct the analysis. The steps are as follows:

1. Preprocessing

a. Give the jobname for the analysis

i. **Utility menu > File > Change Jobname. Insert jobname**

b. Define element type

i. **Main Menu > Preprocessor > Element Type > Add/Edit/Delete**

ii. **Select PLANE2 and SOLID95**

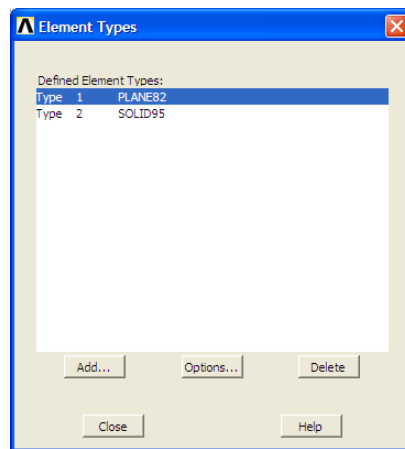


Figure 1.1: Selecting Element Types

iii. **Click Options and select Plane Strain**

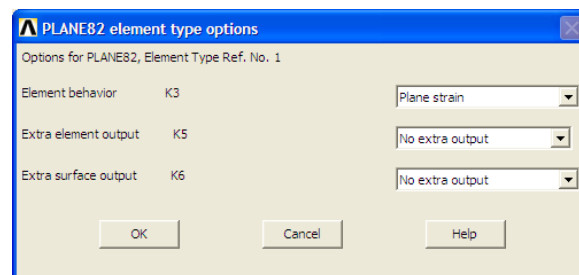


Figure 1.2: Plane element type options

c. Define material properties

- i. **Main Menu > Preprocessor > Material Props > Material Models**
- ii. **Structural > Linear > Elastic > Isotropic**
- iii. **Insert the material properties of Young Modulus (EX) and Poisson's Ratio (PRXY)**

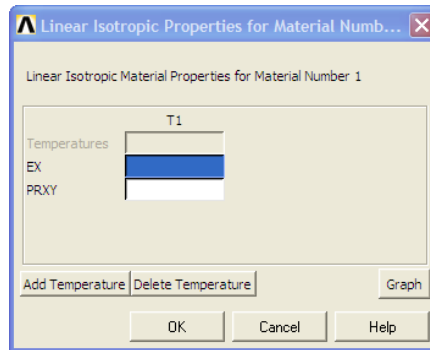


Figure 1.3: Material Properties

d. Define key points

- i. **Main Menu > Preprocessor > Modeling > Create > Keypoints > In Active CS**

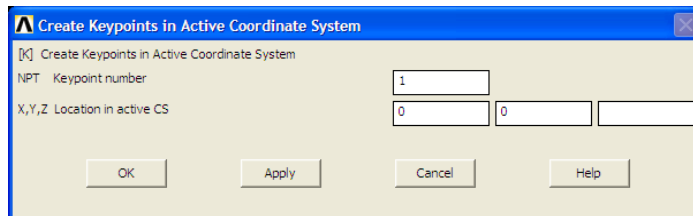


Figure 1.4: Creating key-points by coordinate

- ii. **Insert key-points coordinate according to the model**

e. Create the Area

- i. **Main Menu > Preprocessor > Modeling > Create > Areas > Arbitrary > through KP > pick > OK**

- f. Create circle
 - i. **Main Menu > Preprocessor > modeling > create > areas > circle > solid circle**
 - ii. **Insert radius, x and y coordinate**
 - iii. **Main menu > Preprocessor > modeling > operate > Booleans > Subtract > areas > pick all > pick circle**

g. Meshing the Area

- i. **Main Menu > Preprocessor > Meshing > Size Cntrls > Concentrated KPs. > create > OK**
- ii. **Pick crack tip key-point.** Fill appropriate value. Click OK
- iii. **Main menu > Preprocessor > meshing > manual sizes > lines > pick lines > OK**

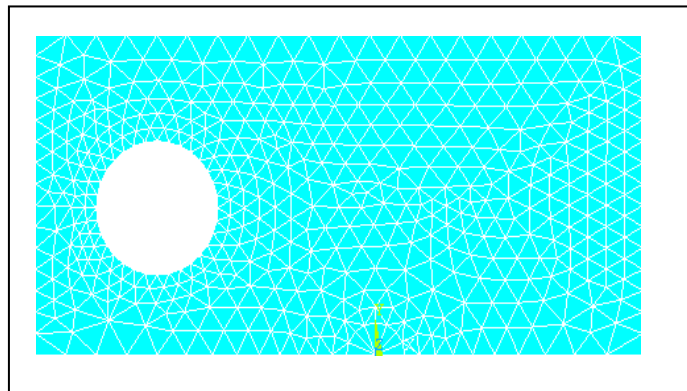


Figure 1.5: Meshed Areas

- i. **Choose every line at the model**
- ii. **Main Menu > Preprocessor > Meshing > Mesh > Areas > Free**
- iii. **Select the area to be meshed. Click OK**

h. Extrude the model

- i. **Main Menu > Preprocessor > Modeling > Operate > Extrude > Element Ext Opts**

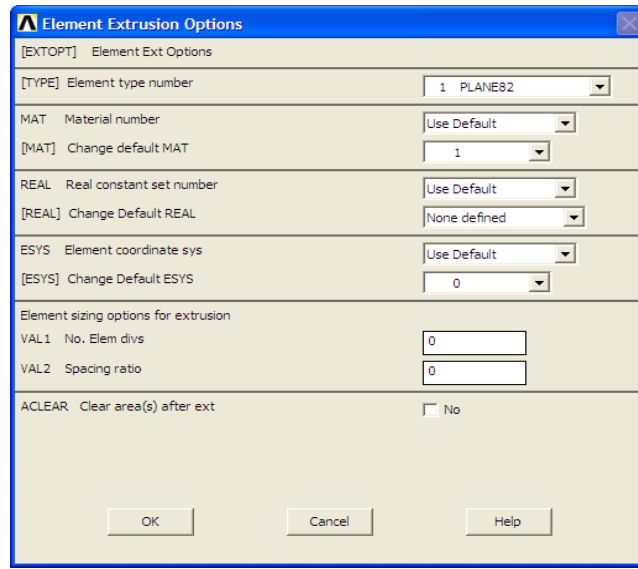


Figure 1.6: Element extrusion option

- ii. **Put No of element division and spacing ratio**

- iii. **Main Menu > Preprocessor > Modeling > Operate > Extrude > Areas > by xyz offset > Ok**

- iv. **Put thickness value. Click OK**

2. Solution

a. Define boundary condition

- i. **Utility menu > select > select everything > select entities > area > by numpick > apply**

- ii. **Main Menu > Solution > Define Loads > Apply > Structural > displacement > symmetry boundary condition > on nodes > pick all**
- iii. **Insert Y axis = 0 then click OK**
- iv. **Main menu > Solution > define loads apply > structural > displacement > lines > pick lines > OK**
- v. **Set DOF = 0**
- vi. **To see the boundary condition at that line use plot lines**

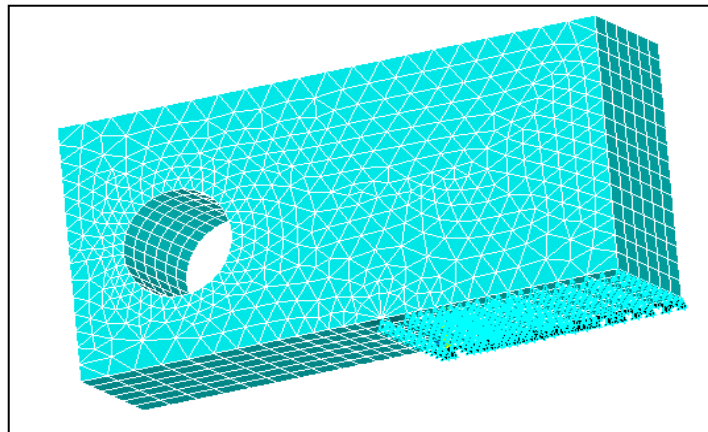


Figure 1.7: Boundary condition on nodes

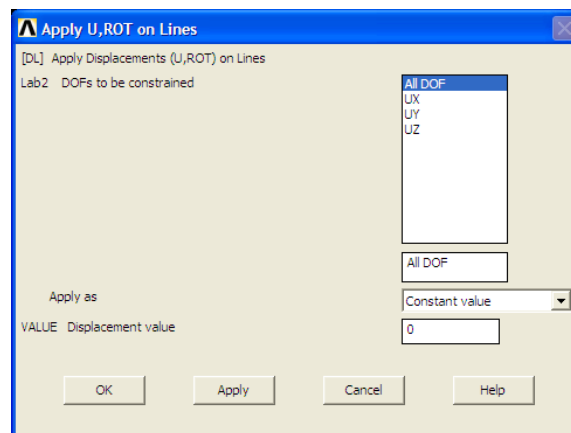


Figure 1.8: Displacement value is set for 0 for all DOF

- b. Define load
 - i. **Utility menu > select > select entities > ares > by numpick > apply**
 - ii. **Choose area at the top of the circle**
 - iii. **Utility menu > select > select entities > nodes > attached to > area, all > apply**
 - iv. **Main Menu > Solution > Define Loads > Apply > Structural > Force/Moment > > on nodes > pick all > OK**
 - v. **Set the applied load equal to applied load divide by the no of nodes**

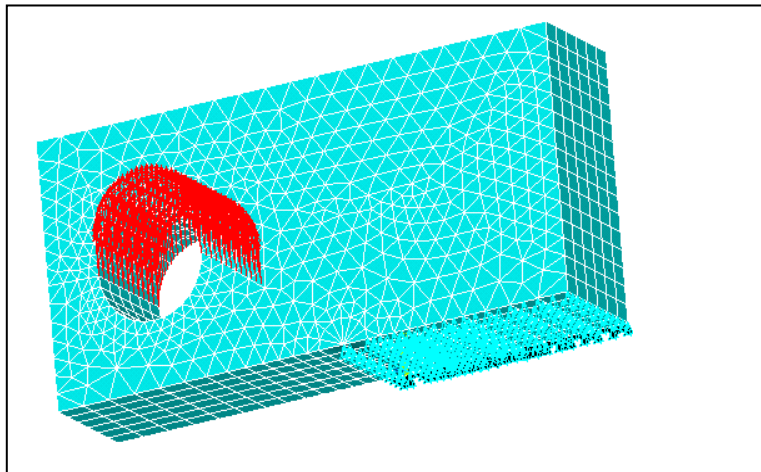


Figure1.9: Applied load to the area selected

- c. Solve
 - i. **Main menu > solution > solve > Current LS > OK**

3. General Postprocessor

- a. Plot result
 - i. **Main menu > General Postproc > Plot result > Contour plot > nodal solution > Von Stress Misses > OK**
- b. Define Path

- i. **Main menu > General Postproc > Define Path > By nodes**
- ii. **Select 3 nodes of crack from the crack tip to the direction of crack. Click OK.**
- iii. **Set Path = K1**

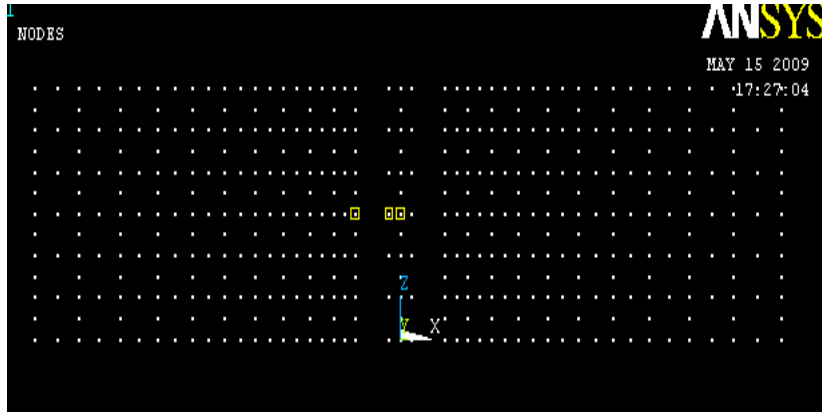


Figure 1.10: Select nodes at crack tip which is in the direction from crack tip to the crack

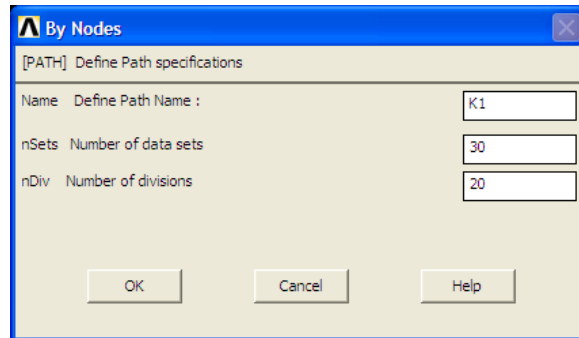
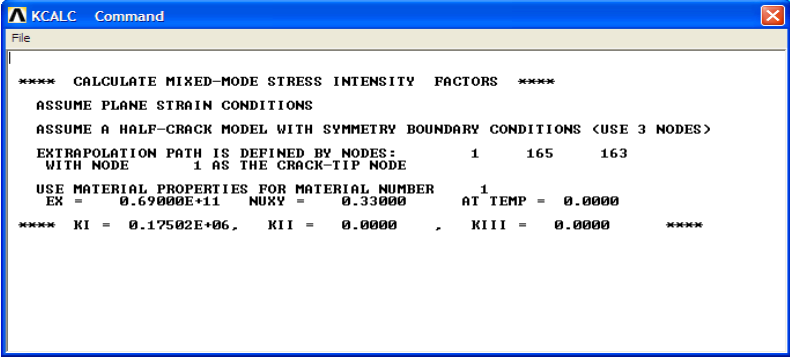


Figure 1.11: Define pathname of the path

- c. Define Stress Intensity Factor, K
 - i. General Postproc > Nodal Calc > Stress Intensity Factor > OK

ii. The result will appear



```
File
**** CALCULATE MIXED-MODE STRESS INTENSITY FACTORS ****
ASSUME PLANE STRAIN CONDITIONS
ASSUME A HALF-CRACK MODEL WITH SYMMETRY BOUNDARY CONDITIONS <USE 3 NODES>
EXTRAPOLATION PATH IS DEFINED BY NODES:      1      165      163
WITH NODE      1 AS THE CRACK-TIP NODE
USE MATERIAL PROPERTIES FOR MATERIAL NUMBER      1
EX = 0.69000E+11  NUXX = 0.33000  AT TEMP = 0.0000
**** KI = 0.17502E+06,  KII = 0.0000 ,  KIII = 0.0000 ****
```

Figure 1.12: Stress intensity factor KCALC results

APPENDIX 3:
RESULT FOR EMPIRICAL
CALCULATION AND
NUMERICAL METHOD

Table 4.1: K value for $\frac{a}{w}$ ratio from 0.45 to 0.49 for empirical method

| W/B | B (m) | 0.45 | 0.46 | 0.47 | 0.48 | 0.49 |
|------|--------|--------|--------|--------|--------|--------|
| 2.00 | 0.0250 | 1.4919 | 1.5348 | 1.5796 | 1.6261 | 1.6762 |
| 2.10 | 0.0238 | 1.5665 | 1.6116 | 1.6585 | 1.7074 | 1.7600 |
| 2.20 | 0.0227 | 1.6411 | 1.6883 | 1.7375 | 1.7887 | 1.8438 |
| 2.30 | 0.0217 | 1.7157 | 1.7651 | 1.8165 | 1.8700 | 1.9276 |
| 2.40 | 0.0208 | 1.7903 | 1.8418 | 1.8955 | 1.9513 | 2.0114 |
| 2.50 | 0.0200 | 1.8649 | 1.9185 | 1.9744 | 2.0326 | 2.0952 |
| 2.60 | 0.0192 | 1.9395 | 1.9953 | 2.0534 | 2.1139 | 2.1790 |
| 2.70 | 0.0185 | 2.0141 | 2.0720 | 2.1324 | 2.1952 | 2.2628 |
| 2.80 | 0.0179 | 2.0887 | 2.1488 | 2.2114 | 2.2765 | 2.3466 |
| 2.90 | 0.0172 | 2.1633 | 2.2255 | 2.2904 | 2.3578 | 2.4304 |
| 3.00 | 0.0167 | 2.2379 | 2.3023 | 2.3693 | 2.4391 | 2.5142 |
| 3.10 | 0.0161 | 2.3125 | 2.3790 | 2.4483 | 2.5204 | 2.5980 |
| 3.20 | 0.0156 | 2.3870 | 2.4557 | 2.5273 | 2.6017 | 2.6819 |
| 3.30 | 0.0152 | 2.4616 | 2.5325 | 2.6063 | 2.6830 | 2.7657 |
| 3.40 | 0.0147 | 2.5362 | 2.6092 | 2.6852 | 2.7643 | 2.8495 |
| 3.50 | 0.0143 | 2.6108 | 2.6860 | 2.7642 | 2.8456 | 2.9333 |
| 3.60 | 0.0139 | 2.6854 | 2.7627 | 2.8432 | 2.9269 | 3.0171 |
| 3.70 | 0.0135 | 2.7600 | 2.8394 | 2.9222 | 3.0082 | 3.1009 |
| 3.80 | 0.0132 | 2.8346 | 2.9162 | 3.0012 | 3.0895 | 3.1847 |
| 3.90 | 0.0128 | 2.9092 | 2.9929 | 3.0801 | 3.1708 | 3.2685 |
| 4.00 | 0.0125 | 2.9838 | 3.0697 | 3.1591 | 3.2521 | 3.3523 |

Table 4.2: K value for $\frac{a}{w}$ ratio from 0.45 to 0.49 for numerical method

| B | W/B | 0.45 | 0.46 | 0.47 | 0.48 | 0.49 |
|--------|------|--------|--------|--------|--------|--------|
| 0.0250 | 2.00 | 1.6210 | 1.6670 | 1.7150 | 1.7650 | 1.8176 |
| 0.0238 | 2.10 | 1.7027 | 1.7505 | 1.8006 | 1.8531 | 1.9083 |
| 0.0227 | 2.20 | 1.7836 | 1.8337 | 1.8862 | 1.9444 | 1.9992 |
| 0.0217 | 2.30 | 1.8644 | 1.9168 | 1.9717 | 2.0290 | 2.0899 |
| 0.0208 | 2.40 | 1.9452 | 1.9999 | 2.0573 | 2.1174 | 2.1807 |
| 0.0200 | 2.50 | 2.0259 | 2.0829 | 2.1427 | 2.2054 | 2.2713 |
| 0.0192 | 2.60 | 2.1067 | 2.1660 | 2.2282 | 2.2934 | 2.3620 |
| 0.0185 | 2.70 | 2.1874 | 2.2490 | 2.3136 | 2.3814 | 2.4526 |
| 0.0179 | 2.80 | 2.2682 | 2.3321 | 2.3991 | 2.4694 | 2.5433 |
| 0.0172 | 2.90 | 2.3489 | 2.4152 | 2.4846 | 2.5574 | 2.6340 |
| 0.0167 | 3.00 | 2.4296 | 2.4976 | 2.5694 | 2.6448 | 2.7240 |
| 0.0161 | 3.10 | 2.5103 | 2.5811 | 2.6554 | 2.7333 | 2.8152 |
| 0.0156 | 3.20 | 2.5910 | 2.6641 | 2.7408 | 2.8212 | 2.9058 |
| 0.0152 | 3.30 | 2.6716 | 2.7470 | 2.8261 | 2.9090 | 2.9963 |
| 0.0147 | 3.40 | 2.7523 | 2.8300 | 2.9115 | 2.9970 | 3.0869 |
| 0.0143 | 3.50 | 2.8330 | 2.9130 | 2.9969 | 3.0849 | 3.1775 |
| 0.0139 | 3.60 | 2.9137 | 2.9960 | 3.0823 | 3.1756 | 3.2681 |
| 0.0135 | 3.70 | 2.9943 | 3.0789 | 3.1676 | 3.2607 | 3.3586 |
| 0.0132 | 3.80 | 3.0751 | 3.1620 | 3.2531 | 3.3488 | 3.4493 |
| 0.0128 | 3.90 | 3.1557 | 3.2449 | 3.3385 | 3.4388 | 3.5398 |
| 0.0125 | 4.00 | 3.2366 | 3.3281 | 3.4240 | 3.5247 | 3.6306 |

Table: K_I value for $\frac{a}{w}$ ratio from 0.50 to 0.55 for empirical method

| B (m) | w/b | 0.50 | 0.51 | 0.52 | 0.53 | 0.54 | 0.55 |
|--------|------|--------|--------|--------|--------|--------|--------|
| 0.0250 | 2.00 | 1.7280 | 1.7817 | 1.8407 | 1.9016 | 1.9642 | 2.0321 |
| 0.0238 | 2.10 | 1.8144 | 1.8708 | 1.9328 | 1.9966 | 2.0624 | 2.1337 |
| 0.0227 | 2.20 | 1.9008 | 1.9599 | 2.0248 | 2.0917 | 2.1606 | 2.2354 |
| 0.0217 | 2.30 | 1.9872 | 2.0490 | 2.1168 | 2.1868 | 2.2588 | 2.3370 |
| 0.0208 | 2.40 | 2.0736 | 2.1380 | 2.2089 | 2.2819 | 2.3570 | 2.4386 |
| 0.0200 | 2.50 | 2.1600 | 2.2271 | 2.3009 | 2.3769 | 2.4552 | 2.5402 |
| 0.0192 | 2.60 | 2.2464 | 2.3162 | 2.3930 | 2.4720 | 2.5534 | 2.6418 |
| 0.0185 | 2.70 | 2.3328 | 2.4053 | 2.4850 | 2.5671 | 2.6516 | 2.7434 |
| 0.0179 | 2.80 | 2.4192 | 2.4944 | 2.5770 | 2.6622 | 2.7498 | 2.8450 |
| 0.0172 | 2.90 | 2.5056 | 2.5835 | 2.6691 | 2.7573 | 2.8480 | 2.9466 |
| 0.0167 | 3.00 | 2.5920 | 2.6725 | 2.7611 | 2.8523 | 2.9462 | 3.0482 |
| 0.0161 | 3.10 | 2.6785 | 2.7616 | 2.8531 | 2.9474 | 3.0445 | 3.1498 |
| 0.0156 | 3.20 | 2.7649 | 2.8507 | 2.9452 | 3.0425 | 3.1427 | 3.2514 |
| 0.0152 | 3.30 | 2.8513 | 2.9398 | 3.0372 | 3.1376 | 3.2409 | 3.3530 |
| 0.0147 | 3.40 | 2.9377 | 3.0289 | 3.1292 | 3.2326 | 3.3391 | 3.4546 |
| 0.0143 | 3.50 | 3.0241 | 3.1180 | 3.2213 | 3.3277 | 3.4373 | 3.5562 |
| 0.0139 | 3.60 | 3.1105 | 3.2071 | 3.3133 | 3.4228 | 3.5355 | 3.6578 |
| 0.0135 | 3.70 | 3.1969 | 3.2961 | 3.4054 | 3.5179 | 3.6337 | 3.7595 |
| 0.0132 | 3.80 | 3.2833 | 3.3852 | 3.4974 | 3.6129 | 3.7319 | 3.8611 |
| 0.0128 | 3.90 | 3.3697 | 3.4743 | 3.5894 | 3.7080 | 3.8301 | 3.9627 |
| 0.0125 | 4.00 | 3.4561 | 3.5634 | 3.6815 | 3.8031 | 3.9283 | 4.0643 |

Table: K_I value for $\frac{a}{w}$ ratio from 0.50 to 0.55 for numerical method

| B (m) | w/b | 0.5 | 0.51 | 0.52 | 0.53 | 0.54 | 0.55 |
|--------|-----|--------|--------|--------|--------|--------|--------|
| 0.0250 | 2 | 1.8728 | 1.9311 | 1.9925 | 2.0574 | 2.1259 | 2.1987 |
| 0.0238 | 2.1 | 1.9664 | 2.0276 | 2.0922 | 2.1604 | 2.2324 | 2.309 |
| 0.0227 | 2.2 | 2.0601 | 2.1243 | 2.1919 | 2.2635 | 2.339 | 2.4193 |
| 0.0217 | 2.3 | 2.1536 | 2.2208 | 2.2916 | 2.3665 | 2.4455 | 2.5295 |
| 0.0208 | 2.4 | 2.2472 | 2.3173 | 2.3913 | 2.4695 | 2.552 | 2.6397 |
| 0.0200 | 2.5 | 2.3407 | 2.4138 | 2.4908 | 2.5724 | 2.6584 | 2.7499 |
| 0.0192 | 2.6 | 2.4341 | 2.5102 | 2.5904 | 2.6752 | 2.7648 | 2.86 |
| 0.0185 | 2.7 | 2.5276 | 2.6066 | 2.6899 | 2.7781 | 2.8712 | 2.9701 |
| 0.0179 | 2.8 | 2.6211 | 2.7031 | 2.7896 | 2.881 | 2.9776 | 3.0803 |
| 0.0172 | 2.9 | 2.7146 | 2.7995 | 2.8891 | 2.9839 | 3.084 | 3.1904 |
| 0.0167 | 3 | 2.8074 | 2.8953 | 2.988 | 3.0861 | 3.1896 | 3.2997 |
| 0.0161 | 3.1 | 2.9013 | 2.9922 | 3.0881 | 3.1895 | 3.2966 | 3.4104 |
| 0.0156 | 3.2 | 2.9947 | 3.0886 | 3.1876 | 3.2923 | 3.4029 | 3.5204 |
| 0.0152 | 3.3 | 3.088 | 3.1848 | 3.2869 | 3.395 | 3.509 | 3.6303 |
| 0.0147 | 3.4 | 3.1815 | 3.281 | 3.3865 | 3.4978 | 3.6154 | 3.7404 |
| 0.0143 | 3.5 | 3.2748 | 3.3775 | 3.4859 | 3.6006 | 3.7216 | 3.8503 |
| 0.0139 | 3.6 | 3.3683 | 3.4739 | 3.5854 | 3.7034 | 3.8279 | 3.9603 |
| 0.0135 | 3.7 | 3.4739 | 3.5702 | 3.6864 | 3.806 | 3.9341 | 4.0702 |
| 0.0132 | 3.8 | 3.5551 | 3.6666 | 3.7844 | 3.9089 | 4.0405 | 4.1803 |
| 0.0128 | 3.9 | 3.6484 | 3.7629 | 3.8838 | 4.0116 | 4.1467 | 4.2902 |
| 0.0125 | 4 | 3.7419 | 3.8594 | 3.9834 | 4.1146 | 4.2531 | 4.4004 |

Table: K_I value for $\frac{b}{w}$ ratio from 2.0 to 2.4 for empirical method

| a/w | A (m) | 2 | 2.1 | 2.2 | 2.3 | 2.4 |
|------|--------|-------|-------|-------|-------|-------|
| 0.45 | 0.0225 | 1.492 | 1.566 | 1.641 | 1.716 | 1.790 |
| 0.46 | 0.023 | 1.535 | 1.612 | 1.688 | 1.765 | 1.842 |
| 0.47 | 0.0235 | 1.580 | 1.659 | 1.738 | 1.816 | 1.895 |
| 0.48 | 0.0240 | 1.626 | 1.707 | 1.789 | 1.870 | 1.951 |
| 0.49 | 0.0245 | 1.676 | 1.760 | 1.844 | 1.928 | 2.011 |
| 0.50 | 0.025 | 1.728 | 1.814 | 1.901 | 1.987 | 2.074 |
| 0.51 | 0.0255 | 1.782 | 1.871 | 1.960 | 2.049 | 2.138 |
| 0.52 | 0.0260 | 1.841 | 1.933 | 2.025 | 2.117 | 2.209 |
| 0.53 | 0.0265 | 1.902 | 1.997 | 2.092 | 2.187 | 2.282 |
| 0.54 | 0.027 | 1.964 | 2.062 | 2.161 | 2.259 | 2.357 |
| 0.55 | 0.0275 | 2.032 | 2.134 | 2.235 | 2.337 | 2.439 |

Table: K_I value for $\frac{B}{w}$ ratio from 2.0 to 2.4 for numerical method

| a/w | A (m) | 2 | 2.1 | 2.2 | 2.3 | 2.4 |
|------|--------|-------|-------|-------|-------|-------|
| 0.45 | 0.0225 | 1.621 | 1.703 | 1.784 | 1.864 | 1.945 |
| 0.46 | 0.0230 | 1.667 | 1.751 | 1.834 | 1.917 | 2.000 |
| 0.47 | 0.0235 | 1.715 | 1.801 | 1.886 | 1.972 | 2.057 |
| 0.48 | 0.0240 | 1.765 | 1.853 | 1.944 | 2.029 | 2.117 |
| 0.49 | 0.0245 | 1.818 | 1.908 | 1.999 | 2.090 | 2.181 |
| 0.50 | 0.025 | 1.873 | 1.966 | 2.060 | 2.154 | 2.247 |
| 0.51 | 0.0255 | 1.931 | 2.028 | 2.124 | 2.221 | 2.317 |

| | | | | | | |
|------|--------|-------|-------|-------|-------|-------|
| 0.52 | 0.0260 | 1.993 | 2.092 | 2.192 | 2.292 | 2.391 |
| 0.53 | 0.0265 | 2.057 | 2.160 | 2.264 | 2.367 | 2.470 |
| 0.54 | 0.027 | 2.126 | 2.232 | 2.339 | 2.446 | 2.552 |
| 0.55 | 0.0275 | 2.199 | 2.309 | 2.419 | 2.530 | 2.640 |

Table: K_I value for $\frac{B}{W}$ ratio from 2.5 to 2.9 for empirical method

| a/w | A (m) | 2.5 | 2.6 | 2.7 | 2.8 | 2.9 |
|------|--------|-------|-------|-------|-------|-------|
| 0.45 | 0.0225 | 1.865 | 1.939 | 2.014 | 2.089 | 2.163 |
| 0.46 | 0.023 | 1.919 | 1.995 | 2.072 | 2.149 | 2.226 |
| 0.47 | 0.0235 | 1.974 | 2.053 | 2.132 | 2.211 | 2.290 |
| 0.48 | 0.0240 | 2.033 | 2.114 | 2.195 | 2.276 | 2.358 |
| 0.49 | 0.0245 | 2.095 | 2.179 | 2.263 | 2.347 | 2.430 |
| 0.50 | 0.025 | 2.160 | 2.246 | 2.333 | 2.419 | 2.506 |
| 0.51 | 0.0255 | 2.227 | 2.316 | 2.405 | 2.494 | 2.583 |
| 0.52 | 0.0260 | 2.301 | 2.393 | 2.485 | 2.577 | 2.669 |
| 0.53 | 0.0265 | 2.377 | 2.472 | 2.567 | 2.662 | 2.757 |
| 0.54 | 0.027 | 2.455 | 2.553 | 2.652 | 2.750 | 2.848 |
| 0.55 | 0.0275 | 2.540 | 2.642 | 2.743 | 2.845 | 2.947 |

Table: K_I value for $\frac{B}{W}$ ratio from 2.5 to 2.9 for numerical method

| a/w | A (m) | 2.5 | 2.6 | 2.7 | 2.8 | 2.9 |
|------|--------|-------|-------|-------|-------|-------|
| 0.45 | 0.0225 | 2.026 | 2.107 | 2.187 | 2.268 | 2.349 |
| 0.46 | 0.023 | 2.083 | 2.166 | 2.249 | 2.332 | 2.415 |
| 0.47 | 0.0235 | 2.143 | 2.228 | 2.314 | 2.399 | 2.485 |
| 0.48 | 0.024 | 2.205 | 2.293 | 2.381 | 2.469 | 2.557 |
| 0.49 | 0.0245 | 2.271 | 2.362 | 2.453 | 2.543 | 2.634 |
| 0.50 | 0.025 | 2.341 | 2.434 | 2.528 | 2.621 | 2.715 |
| 0.51 | 0.0255 | 2.414 | 2.510 | 2.607 | 2.703 | 2.800 |
| 0.52 | 0.026 | 2.491 | 2.590 | 2.690 | 2.790 | 2.889 |
| 0.53 | 0.0265 | 2.572 | 2.675 | 2.778 | 2.881 | 2.984 |
| 0.54 | 0.027 | 2.658 | 2.765 | 2.871 | 2.978 | 3.084 |
| 0.55 | 0.0275 | 2.750 | 2.860 | 2.970 | 3.080 | 3.190 |

Table: K_I value for $\frac{B}{W}$ ratio from 3.0 to 3.4 for empirical method

| a/w | A (m) | 3 | 3.1 | 3.2 | 3.3 | 3.4 |
|------|--------|-------|-------|-------|-------|-------|
| 0.45 | 0.0225 | 2.238 | 2.312 | 2.387 | 2.462 | 2.536 |
| 0.46 | 0.023 | 2.302 | 2.379 | 2.456 | 2.532 | 2.609 |
| 0.47 | 0.0235 | 2.369 | 2.448 | 2.527 | 2.606 | 2.685 |
| 0.48 | 0.024 | 2.439 | 2.520 | 2.602 | 2.683 | 2.764 |
| 0.49 | 0.0245 | 2.514 | 2.598 | 2.682 | 2.766 | 2.849 |
| 0.50 | 0.025 | 2.592 | 2.678 | 2.765 | 2.851 | 2.938 |

| | | | | | | |
|------|--------|-------|-------|-------|-------|-------|
| 0.51 | 0.0255 | 2.673 | 2.762 | 2.851 | 2.940 | 3.029 |
| 0.52 | 0.026 | 2.761 | 2.853 | 2.945 | 3.037 | 3.129 |
| 0.53 | 0.0265 | 2.852 | 2.947 | 3.042 | 3.138 | 3.233 |
| 0.54 | 0.027 | 2.946 | 3.044 | 3.143 | 3.241 | 3.339 |
| 0.55 | 0.0275 | 3.048 | 3.150 | 3.251 | 3.353 | 3.455 |

Table: K_I value for $\frac{b}{w}$ ratio from 3.0 to 3.4 for numerical method

| a/w | a | 3 | 3.1 | 3.2 | 3.3 | 3.4 |
|------|--------|--------|--------|--------|--------|--------|
| 0.45 | 0.0225 | 2.4296 | 2.5103 | 2.5910 | 2.6716 | 2.7523 |
| 0.46 | 0.0230 | 2.4976 | 2.5811 | 2.6641 | 2.7470 | 2.8300 |
| 0.47 | 0.0235 | 2.5694 | 2.6554 | 2.7408 | 2.8261 | 2.9115 |
| 0.48 | 0.0240 | 2.6448 | 2.7333 | 2.8212 | 2.9090 | 2.9970 |
| 0.49 | 0.0245 | 2.7240 | 2.8152 | 2.9058 | 2.9963 | 3.0869 |
| 0.50 | 0.0250 | 2.8074 | 2.9013 | 2.9947 | 3.0880 | 3.1815 |
| 0.51 | 0.0255 | 2.8953 | 2.9922 | 3.0886 | 3.1848 | 3.2810 |
| 0.52 | 0.0260 | 2.9880 | 3.0881 | 3.1876 | 3.2869 | 3.3865 |
| 0.53 | 0.0265 | 3.0861 | 3.1895 | 3.2923 | 3.3950 | 3.4978 |
| 0.54 | 0.0270 | 3.1896 | 3.2966 | 3.4029 | 3.5090 | 3.6154 |
| 0.55 | 0.0275 | 3.2997 | 3.4104 | 3.5204 | 3.6303 | 3.7404 |

Table: K_I value for $\frac{B}{W}$ ratio from 3.5 to 4.0 for empirical method

| a/w | A (m) | 3.5 | 3.6 | 3.7 | 3.8 | 3.9 | 4.0 |
|------|--------|--------|--------|--------|--------|--------|--------|
| 0.45 | 0.0225 | 2.6108 | 2.6854 | 2.7600 | 2.8346 | 2.9092 | 2.9838 |
| 0.46 | 0.0230 | 2.6860 | 2.7627 | 2.8394 | 2.9162 | 2.9929 | 3.0697 |
| 0.47 | 0.0235 | 2.7642 | 2.8432 | 2.9222 | 3.0012 | 3.0801 | 3.1591 |
| 0.48 | 0.0240 | 2.8456 | 2.9269 | 3.0082 | 3.0895 | 3.1708 | 3.2521 |
| 0.49 | 0.0245 | 2.9333 | 3.0171 | 3.1009 | 3.1847 | 3.2685 | 3.3523 |
| 0.50 | 0.0250 | 3.0241 | 3.1105 | 3.1969 | 3.2833 | 3.3697 | 3.4561 |
| 0.51 | 0.0255 | 3.1180 | 3.2071 | 3.2961 | 3.3852 | 3.4743 | 3.5634 |
| 0.52 | 0.0260 | 3.2213 | 3.3133 | 3.4054 | 3.4974 | 3.5894 | 3.6815 |
| 0.53 | 0.0265 | 3.3277 | 3.4228 | 3.5179 | 3.6129 | 3.7080 | 3.8031 |
| 0.54 | 0.0270 | 3.4373 | 3.5355 | 3.6337 | 3.7319 | 3.8301 | 3.9263 |
| 0.55 | 0.0275 | 3.5562 | 3.6578 | 3.7595 | 3.8611 | 3.9627 | 4.0643 |

Table: K_I value for $\frac{B}{W}$ ratio from 3.5 to 4.0 for numerical method

| a/w | A (m) | 3.5 | 3.6 | 3.7 | 3.8 | 3.9 | 4 |
|------|--------|--------|--------|--------|--------|--------|--------|
| 0.45 | 0.0225 | 2.8330 | 2.9137 | 2.9944 | 3.0751 | 3.1557 | 3.2366 |
| 0.46 | 0.0230 | 2.9130 | 2.9960 | 3.0789 | 3.1620 | 3.2449 | 3.3281 |
| 0.47 | 0.0235 | 2.9969 | 3.0823 | 3.1676 | 3.2531 | 3.3385 | 3.4240 |
| 0.48 | 0.0240 | 3.0849 | 3.1756 | 3.2607 | 3.3488 | 3.4366 | 3.5247 |
| 0.49 | 0.0245 | 3.1775 | 3.2681 | 3.3586 | 3.4493 | 3.5398 | 3.6306 |
| 0.50 | 0.0250 | 3.2748 | 3.3683 | 3.4616 | 3.5551 | 3.6484 | 3.7419 |

| | | | | | | | |
|------|--------|--------|--------|--------|--------|--------|--------|
| 0.51 | 0.0255 | 3.3775 | 3.4739 | 3.5702 | 3.6666 | 3.7629 | 3.8594 |
| 0.52 | 0.0260 | 3.4859 | 3.5854 | 3.6848 | 3.7844 | 3.8838 | 3.9834 |
| 0.53 | 0.0265 | 3.6006 | 3.7034 | 3.8060 | 3.9089 | 4.0116 | 4.1146 |
| 0.54 | 0.0270 | 3.7216 | 3.8279 | 3.9341 | 4.0405 | 4.1467 | 4.2531 |
| 0.55 | 0.0275 | 3.8503 | 3.9603 | 4.0702 | 4.1803 | 4.2902 | 4.4004 |