

ANALYSIS ON VARIOUS FACTORS AFFECTING PRESSURE DROP ALONG THE GAS TRANSPORTATION PIPELINE DESIGN

By

WIN AHKAR MEIN

Dissertation submitted in partial fulfillment of
the requirements for the
Bachelor of Engineering (Hons)
(Petroleum Engineering)

SEPTEMBER 2012

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CERTIFICATION OF APPROVAL

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approved by,			
	 -		
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SEPTEMBER 2012

CERTIFICATION OF ORIGINALITY

This is to certify that I, WIN AHKAR MEIN (A006116), am responsible for the work submitted in this project, that the original work is my own except as specified in the references and acknowledgements, and that the original work contained herein have not been undertaken or done by unspecified sources or persons.

WIN AHKAR MEIN

ABSTRACT

The final year project in its present form is to analyze the various factors effecting on pressure drop along the gas transportation pipeline design by using PIPESIM software. Initially to analyze the effect of factor that can cause the pressure drop along the gas transportation design. Typically author will focus on four main factors, Elevation: conversion of fluid potential energy into hydrostatic pressure, Friction (roughness): shear stress between pipe wall and gas, Start node Temperature, Pipe sizing, which will cause the pressure drop along the gas pipeline. Consideration of pipeline transportation is very important before designing the gas transportation pipeline. There are majors problem may occur if failure to analyze on the pressure drop during designing the gas transportation pipeline. The result will be failure to fulfill the customer desire pressure and flow rate and it may lost the large amount of profit.

Author will develop the graphical relationship between these five main factors effecting on the pressure drop in this research. Designing a small model of gas transportation pipeline, simulating by PIPESIM software, analysis on outcome results are main criteria of this project. Brief introduction on project, theory and literature review of the project, methodology and project activities will be included in the report.

ACKNOLEDGEMENT

I would like to take this opportunity to express my utmost gratitude to the individual that have taken the time and effort to assist me in completing the project. First and foremost, my utmost gratitude goes to my supervisor, A.P Aung Kyaw. Without his guidance and patience, I would not be succeeded to complete the project. A warmness thankful to the Final Year Project Coordinator, for provide me with all the initial information required to begin the project. Last but not least, thanks to all individuals that has helped me in any way, but whose name is not mentioned here.

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CHAPTER 1

INTRODUCTION

1.1 BACKGROUND OF STUDY

Pipelines transportation have become an important means of moving natural gas and with the expansion of market and large demand, millions of pipeline have been laid. Pipelines are long and continuously welded, they have a minimum number of curves, they have no sharp bends, and they are most often buried underground. Pipeline transportation is mostly considerable for gas because it takes large amount of volume to transport by mean of shipping and tanker. Pipeline is the most preferred option to transport oil, gas or products in bulk. It could be thousands of km long, branched and networked.

Configuration of both oil & gas pipeline are very similar. A cross country oil or gas pipeline system, normally starts with pumping of oil or compression of gas to develop the requisite pressure to travel a long distance. The pressure required for pumping of oil or compression of gas depends on pipeline length, pipe diameter, & destination pressure requirements. For long pipelines (hundreds of km), booster compressor for gas pipeline and booster pumps for oil pipeline are required along the length as in the graph below.

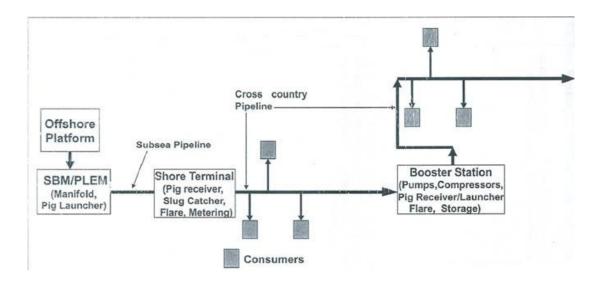


Figure 1: Simple Pipeline Design Process flow

In the past few decades, researchers have devoted much of their attention on consideration of pressure drop on gas transportation pipeline design. There are much pipelines simulation software that have been developed by developers including PIPESIM software to design the oil and gas transportation pipeline. In this final year project, author will be develop on graphical relationship within all the factors effecting on pressure drop along gas transportation pipeline. This software is used in some oil and gas companies to design and operate production-gathering and distribution systems with confidence. PIPESIM software produces details flow regime maps at the existing pipeline operating conditions, incorporating all angles of inclination. PIPESIM software uses the in-situ superficial gas and liquid velocities to identify the flow pattern at every node in the system, it make easy to determine the pressure distribution in pipeline system. Author will be analyze on how these distribution of pressure will affect on specific gravity of oil and gas. A wide varieties of methods can be simulate model in PIPESIM. In this project, Author will design the single phase (gas) flow.

1.2 PROBLEM STATEMENT

During natural gas transportation in pipeline, pressure drop along the pipeline will occur due to fraction factor, elevation and fittings.

It may result in

- reduce the maximum deliverability for gas
- to install additional pressure boost up equipment

1.3 OBJECTIVES

The objective of this work is:

- to analyze the factors that effecting on pressure drop on gas flow performance modelling the simple pipeline design by using PIPESIM simulation software.
- to develop graphical relationship within all the factors.

1.4 SCOPE OF STUDY

The scope of study involved would be starting from information gathering on toward simulating the simple gas transportation pipeline design. Necessary data and Information would be gathered from Myanmar Gas field case study to create

pipeline model for analyzing factors affecting on pressure drop along gas transportation pipeline. Study will be divided into two stages as FYP 1 and FYP 1. In FYP-1, and research will be made theoretical application of pressure drop on fluid flow calculation, necessary data will be collected to develop the simple pipeline design.

1.5 SIGNIFICANT OF PROJECT

Pressure drop is major problem to consider when designing the transportation pipeline. If it was not studied and pipeline designer could not do necessary research on pressure drop, it may failure to deliver the amount of customers desire pressure and flow rate and result in losing the large amount of profit from the project. That is a reason for author to motivate to study and analyze on factors which will cause the pressure drop along pipeline. Through this project, there are propose variables that need to be investigate such as pipeline design (pipe wall thickness, material of pipe, sizing of pipe), phase envelope, pressure drops (inlet temperature, pipe sizing, elevation) and gas flow rate. In ASME 31.8 specifications, steel pipe design formula and design factor can be considered.

1.6 FEASIBILITY OF THE PROJECT

There are total two semesters, 8 months of period to finish the final year projects. Since there will two semesters to analyze and develop model in PIPESIM, final year project was divided into two sections, FYP-1 and FYP-2. Especially for FYP-1, author will get one semester to do research on the projects and to gather necessary information and data. In FYP-2, the project will be finished by building model and analyze the results. Forty percentage of process will be occupied by finding research and gathering data before building model. Twenty percentage of process is building the model with different types of fluid properties and the rest will be more to the analysis on the specific gravity effect on fluid flow performance in transportation of oil and gas. Author will get 14 week to complete some research on theoretical application of specific gravity effect and case study of PIPESIM software. For FYP-2, there will have 14 week to construct the pipeline design and to develop the graphical relationship within all the factors that cause pressure drop. To achieve the goal of this project, author need to follow on the procedures and schedule of the work.

CHAPTER 2

THEORY AND LITERATURE REVIEW

2.1 THEORY

Several equations are used to calculate pressure drop along the gas transportation pipeline and these equation will be discussed.

2.1.1 Pressure Drop Calculation

Several equations are available that relate the gas flow rate with gas properties, pipe diameter and length, and upstream and downstream pressures.

2.1.1.1 General Flow equation

The General Flow equation, also called the Fundamental Flow equation, for the steady-state isothermal flow in a gas pipeline is the basic equation for relating the pressure drop with flow rate. The most common form of this equation in the U.S. Customary System (USCS) of units is given in terms of the pipe diameter, gas properties, pressures, temperatures, and flow rate as (eq.2.0) follows.

$$Q = 1.1494 \times 10^{-3} \left(\frac{T_b}{P_b}\right) \left[\frac{\left(P_1^2 - P_2^2\right)}{GT_f LZf}\right]^{0.5} D^{2.5} \quad (SI \text{ units})$$
Eq.2.0

Note: General Equation for flow rate calculation vs pressure drop without elevation effect

The general flow equation for considerating with elevation effect, and frictional effect in SI unit is.

$$Q = (11.4946 \times 10^{-4}) \frac{1}{\sqrt{f}} \frac{T_b}{P_b} \left(\frac{{P_1}^2 - e^s {P_2}^2}{G T_f L_e Z} \right)^{0.5} D^{2.5} \qquad \text{Eq.2.1}$$

Where,

Q = gas flow rate at standard conditions, m3/day

 $Tb = base temperature, K(273 + {}^{\circ}C)$

Pb = base pressure, kPa

Tf = average gas flow temperature, $K(273 + {}^{\circ}C)$

P1 = upstream pressure, kPa

P2 = downstream pressure, kPa

 $H1 = upstream \ elevation, m$

H2 = downstream elevation, m

Le = equivalent length of pipe, km

L = pipe length, k

The parameters depend on the elevation difference H2 – H1, and the value of constant S can be calculate from the following Equation (Eq.2.2)

$$s = \frac{0.0375G(H_2 - H_1)}{T_f Z}$$
 Eq.2.2

To find the slot between the elevation is,

$$j = \frac{e^s - 1}{s}$$
 Eq.2.3

To find the Equivalent length,

$$L_e = j_1 L_1 + j_2 L_2 e^{s1} + j_3 L_3 e^{s2} + \cdots$$
 Eq.2.4

Note: The term j must be calculated for each slope of each pipe segment of length L1, L2, etc., that make up the length L. where j1, j2, etc., are calculated for each rise or fall in the elevation for pipe segments between the upstream and downstream ends.

where,

Le = equivalent length of pipe, mi

 $L = length \ of \ pipe \ between \ upstream \ and \ downstream \ ends \ (miles)$

s = elevation correction factor, dimensionless

2.1.1.2 Weymouth Equation

The Weymouth, Panhandle A, and Panhandle B equations were developed to simulate compressible gas flow in long pipelines. The Weymouth is the oldest and most common out of three. It was initially developed in 1912.

$$q_{h} = \frac{18.062T_{b}}{p_{b}} \sqrt{\frac{\left(p_{1}^{2} - p_{2}^{2}\right)D^{16/3}}{\gamma_{g}\overline{T}\overline{z}L}}$$
 Eq.2.5

L = length of pipe (mile)

D = Diameter of pipe(in.)

P1 = upstream pressure

P2 = downstream pressure

z = compressibility factor

Tb = base temperature

Pb = base pressure

 $qh = Flow \ rate \ (scf/hr)$

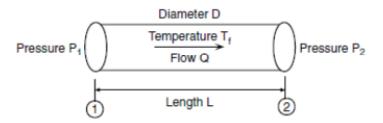


Figure 2 Steady flow in gas pipeline

2.1.1.3. Calculation for Friction Factor

Colebrook-White equation. The Colebrook-White equation for obtaining the friction factor is applicable for a wide range of flow in gas pipelines. Friction factor f is given for turbulent flow as:

$$\frac{1}{\sqrt{f}} = -2\log_{10}\left(\frac{e}{3.7D} + \frac{2.51}{\text{Re}\sqrt{f}}\right)$$
 Eq.2.6

for Re > 4000.

where f = Darcy friction factor

D = pipe inside diameter, in

e = absolute pipe roughness, in

Re = Reynolds number of flow

In SI units the Reynolds number is given by,

$$\mathrm{Re} = 0.5134 \, \frac{P_b}{T_b} \frac{GQ}{\mu D} \qquad _{\mathrm{Eq.2.7}}$$

where Pb = base pressure, kPa

```
Tb = base temperature, K
```

 $G = gas\ gravity\ (air = 1.0)$

Q = gas flow rate, m3/day

D = pipe internal diameter, mm

 $\mu = gas\ viscosity,\ P$

2.2 LITERATURE REVIEW

In this project, there are several factors effecting on pressure drop that need to be understand before developing the graphical relationship between them. The efficient and effective movement of natural gas from producing regions to consumption regions requires an extensive and elaborate transportation system. In many instances, natural gas produced from a particular well will have to travel a great distance to reach its point of use. The transportation system for natural gas consists of a complex network of pipelines, designed to quickly and efficiently transport natural gas from its origin, to areas of high natural gas demand. Transportation of natural gas is closely linked to its storage: should the natural gas being transported not be immediately required, it can be put into storage facilities for when it is needed.

There are five main factors which cause pressure drop along gas pipeline.

- Elevation: conversion of fluid potential energy into hydrostatic pressure.
- Friction: shear stress between pipe wall and gas
- Fittings such as valves & pipeline elbow
- Start node Temperature
- Pipe sizing

Mohammed A. Milan, *Petroleum Engineering Handbook for the practicing engineer*, *Volume 1*, Pressure drop plays a role in calculation of deliverability of a gas production system starting from the pipeline and to compressors calculations, gathering system calculations and production string. In the end, the pipeline capacity will affect in maximum system deliverability for gas. According to the PIPESIM, training course, The contribution from the major terms; elevation and frictional can be summarized as; In well, the effect of elevation term will be (85-100%) with

compare to effect of frictional (0-15%). In pipeline transportation, the effect of elevation term will be (0-30%) and effect of frictional pressure drop will be (70-100%).

Based on 'Distribution Piping: Understanding Pressure Drop' by Compressed Air Challenge, excessive pressure drop will result in poor system performance and excessive energy consumption. Flows restrictions of any type in a system require higher operating pressures than are needed, resulting in higher energy consumption. The particular pressure rise resulting from resistance to flow can involve increasing the drive energy on the compressor by 1% of the connected power for each 2 psi of differential.

H. Dale Beggs stated in his 'Production Optimization Using Nodal Analysis' that the final design of a production system cannot be separated into reservoir performance and piping system performance and handled independently. The amount of oil and gas flowing into the well from the reservoir depends on the pressure drop in the piping system and the pressure drop in the piping system depends on the amount of fluid flowing through it. Therefore, the entire production system must be analyzed as a unit.

Donald F.B Jackson stated that in single phase flowing conditions, the effect of elevation on pressure loss calculations is generally limited to the net elevation change between the start and end of the pipeline. For gas pipelines, the elevation profile affects the in situ pressure, and hence the gas velocity and frictional pressure losses. The low density of natural gas mitigates the effect of hydrostatic head on the in situ pressure, and for most systems, the elevation profile has only minimal impact on the total pressure loss. The effect of the elevation profile on pressure losses in a multiphase pipeline is much more significant. He tried to compare this to single phase gas since the existence of single phase black oil is nearly zero nowadays. In multiphase flow, the different velocities of the gas and liquid phases create a gas liquid slip condition in which the denser liquid phase tends to accumulate in the uphill sections of the pipeline. This accumulation of liquid reduces the area for flow for the gas phase, which increases its velocity until an equilibrium condition is reached. At this steady state condition, the volume of liquid lifted up the hill is equal to the volume of liquid arriving at the base of the hill.

In Petroleum Engineering Handbook for the practicing engineer, Volume 1, by Mohammed A. Milan, pressure drop plays a role in calculation of deliverability of a gas production system starting from the pipeline and it works backward to compressors calculations, gathering system calculations, production string and reservoir. In the end, the pipeline capacity will affect the total system and result in maximum system deliverability for gas.

There are several companies developed the different types of pipeline design simulation software. According to the CanQualPro Training Systems, there are some pipeline design factors need to be consider before designing the pipeline.

2.2.1 Pressure Drop Due to Friction

Pressure drop is the pressure decrease from the inlet to the outlet as the flow increases. Pressure drop is important to know when understanding hydraulics and liquid behavior within a pipeline as the operator will be in a position to prevent pipeline incidents such of Maximum Allowable Working Pressure exceedances or low suction pressure to pipeline pumping facilities. The amount of pressure drop due to friction depends on the velocity of the liquid (laminar or turbulent flow), the liquid viscosity (determined by the products density and specific gravity) and the piping friction factor. These three factors are used to create the Reynolds numbers that reflects velocity variations due to laminar flow (low flow rates) and turbulent flow (high flow rates). This number is then used to determine the product's drag characteristics which are then used to determine the friction factor of the product at a given flow.

Example: Comparing crude oil and liquid propane, liquid propane will have a higher Reynolds number meaning that it will reach turbulent flow much sooner than crude oil in the same size pipe at the same flow rate.

The friction factor for the product within the pipe is now calculated using a Moody Diagram. This is used to calculate the pressure drop within the pipeline per kilometer. The Moody Diagram is a graph that relates the friction factor, the Reynolds number and relative roughness for flow within a pipe. This calculation can determine if the liquid will reach its destination with the proper amount of pressure for pump suction or to storage facilities. Moody Diagrams are found on the internet. Just enter Moody Diagrams in your search engine

2.2.2 Pressure Drop due to elevation

In a flat pipeline, the pressure needed to deliver the product is based on the delivery point requirements and the pressure drop within the pipeline. Final delivery point pressure takes into consideration such things as storage tank farm pressure requirements.

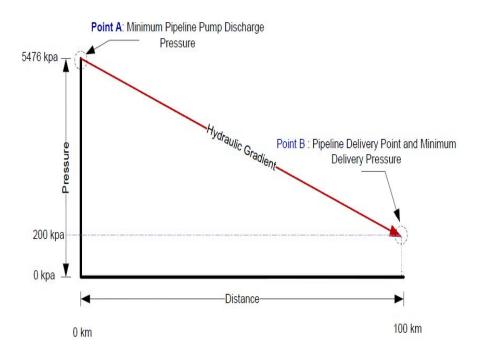


Figure 3 Flat Elevation – Red Line Represents Pressure Drop

As with a flat elevation, pressure requirements within an increased elevation pipeline are determined based on the final delivery point requirements. Within elevation changes there may be peaks that must be taken into consideration

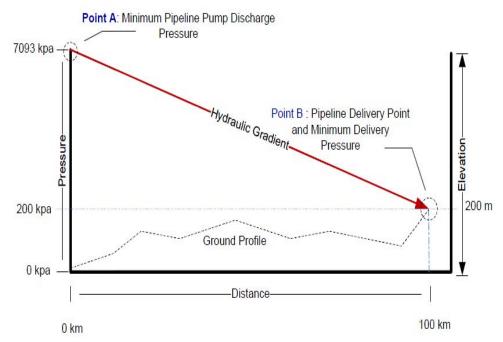


Figure 4 Increasing Elevation – Red Line Represents Pressure Drop

2.2.3 Pressure Drop due to Inlet node Temperature

Based on the research, according to the PIPSIM training course, the effect of inlet node temperature also may cause the minimum amount of pressure drop. Basically the starting node point of transportation pipeline start from Compressor station. Most of the natural gas are being treatment under the some process such as, Dehydration, Separation, H2S removal. From the Separation unit, most of the temperature set point are different base on the well head condition. According to the PIPESIM training course, the following graph can be seen as relationship between Inlet node temperature and Pressure drop.

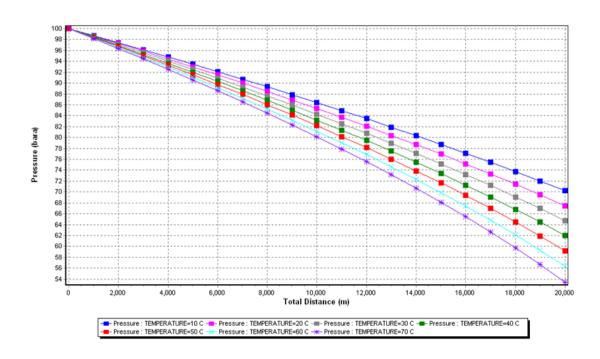


Figure 5 Relationship between Pressure Vs Inlet Temperature

2.2.4 Pressure drop due to Pipeline Sizing

There are different pipeline sizing can be consider during designing the pipeline. According to the PIPESIM Training Course, the different sizes of pipeline diameters may also effect the pressure drop along the gas transportation pipeline. The area of the inner pipeline is larger, or the diameter of the pipeline is large, there may be reduce in some pressure drop as describe in the Figure below. Vice Versa, minimum diameter of the pipeline will give the highest pressure drop along gas transportation pipeline.

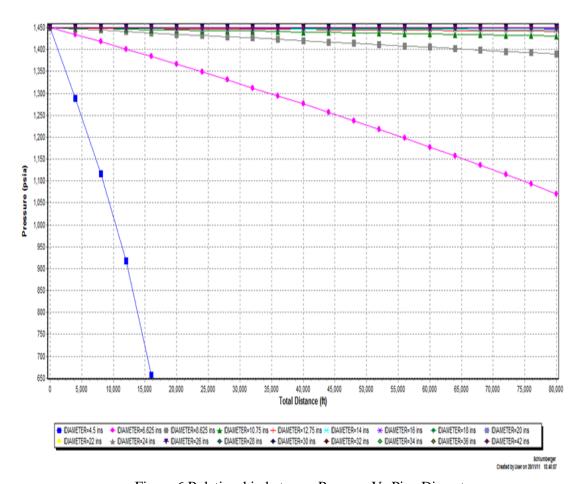


Figure 6 Relationship between Pressure Vs Pipe Diameter

CHAPTER 3

METHODOLOGY

3.1 RESEARCH METHODOLOGY

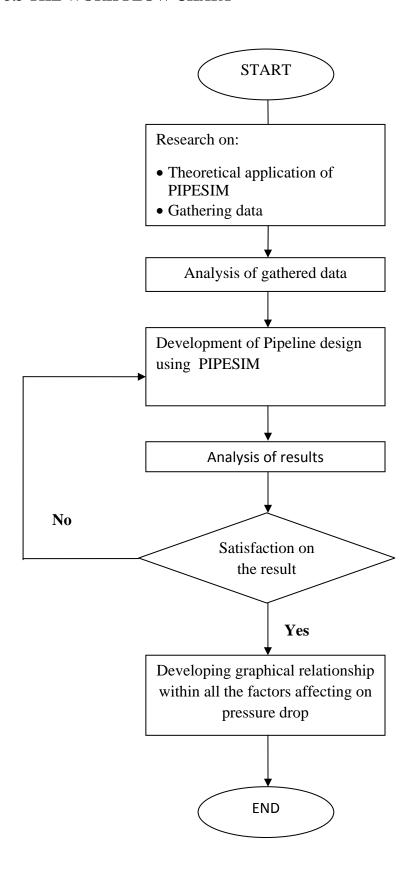
The research methodology to be carried out is as follows:

- to make research work on factors that affect on pressure drop in pipeline transportation, Understanding fundamental theories and concepts, performing a literature review, tools identification
- to obtain available software for this research work.
- to obtain data that required for simulating pipeline transportation design.
- to familiarize with the PIPESIM software

3.2 PROJECT ACTIVITIES

There are several steps included to analyze factors effect on pressure drop along the gas transportation pipeline. firstly author will gather the information about PIPESIM software to familiar with software. The data gathering and theoretical calculation needed to be done during FYP-1 period. During data gathering, author needed to get real performance compositional data for different types of fluid. After gathering data and information, author need to study on PIPESIM soft on how to build a new pipeline designs model using single phase flow system. As a final stage, basic simple pipeline design will construct and by inputting different types parameters and test on how these parameters will effect on the pressure drop along gas transportation pipeline. Author will illustrate by using graphs of flow rate Vs pressure drop, temperature Vs pressure drop to analyze on the effect. Author will describe basic work flow chart in below for the activities of work flow system.

3.3 THE WORK FLOW CHART



3.4 GANT CHART

Milestones Weeks	1 2	3	4	5	9	7	00	6	10	=	12	13	14
Preliminary research													
Literature review (Theory)													
Learning the software													
Data gathering													
Estimating the outcome results													
Final Report (FYP-1)													
	15 16	17	18	19	20	21	22	23	24	25	36	27	28
Evaluating the Data to stimulate													
Modeling with software													
Evaluating the results													
Developing Graphical Relationship													
Analyze the final results													
Final Report (FYP-2)													

3.5 TOOLS AND SOFTWARE

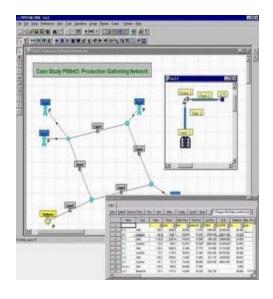
PIPESIM-Optimizing pipeline facilities design

In Universiti Teknologi PETRONAS, simulation software available regarding pipeline and facilities is PIPESIM by Schlumberger. PIPESIM is an applicable tool for modeling single phase gas flow from the reservoir through the production facilities to delivery point. In facilities modeling, PIPESIM can also be used to design systems by varying key system parameters, thus enabling optimal pipeline and equipment sizes to be determined.

Typical applications of module include:

- Multiphase flow in flowlines and pipelines
- Point by point generation of pressure and temperature profiles
- Transportation pipeline design and calculation flow rate
- Flowline & equipment performance modeling (system analysis)





CHAPTER 4

RESULTS AND DISCUSSION

In Final Year Project, Author used Pipe Simulation Software to run a Pipeline design with gas compositional model to analyze the various factors which effecting the pressure drop along the gas transportation pipeline. In this project, author used the following data to run the simulation without including facilities and pipeline will be started from compressor discharge point.

For simulation of gas transportation pipeline design

Pipeline Distance - 200 Miles (for Sensitivity Analysis)

- 177.10 Miles (for real case)

Pipeline Diameter - 24 inches

Wall Thickness - 0.77 inches

Compressor Discharge Pressure - 2325 Psi

Ambient Temp - 28

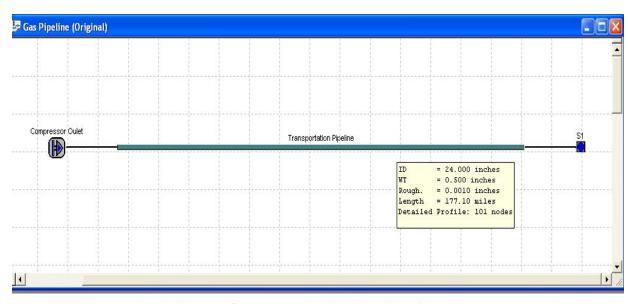


Figure 7 Gas Transportation Pipeline diagram

Real Gas field data is used for gas compositional phase envelope to simulate model.

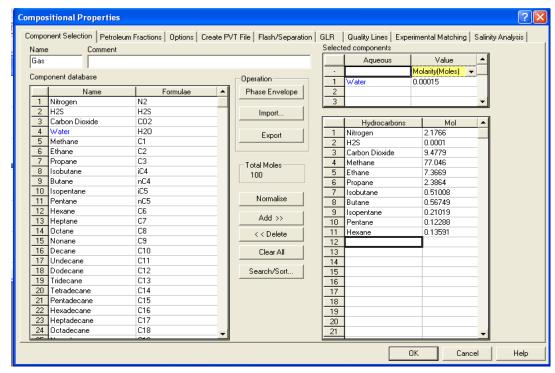


Figure 8 Gas compositional properties table

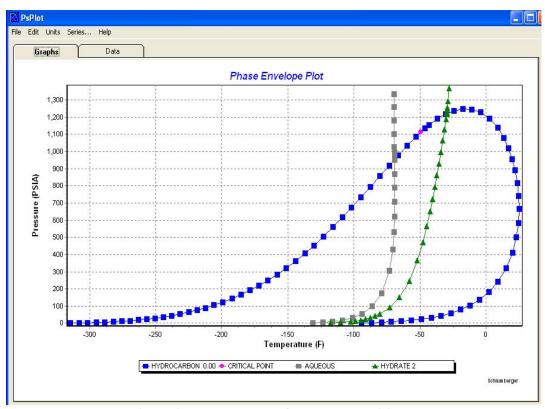


Figure 9 Phase envelope for gas compositional

4.1 Effect of elevation on pressure drop

To analyze the effect of elevation on pressure drop, author used two different scenarios. Firstly author used the real gas field data with zero pipeline elevation started from compressor outlet until it reached to the delivery point. For the another cases author used real gas field data with actual elevation to simulate the gas transportation pipeline model. The relationships graphs between pressure drops vs distances for each of the scenarios were obtained from the simulation.

4.1.1 For zero elevation with actual gas field data,

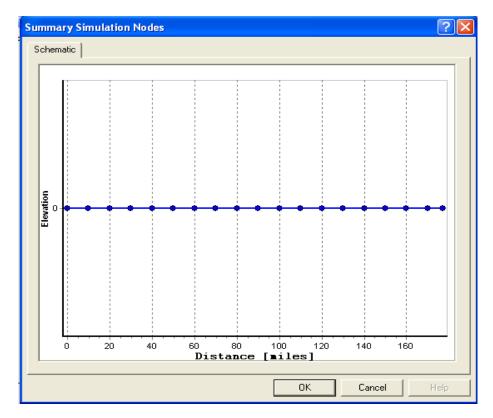


Figure 10 Schematic pipeline diagram for zero elevation

The Figure 10 above shown the schematic pipeline diagram with zero elevation for real gas field. The purpose of simulation for zero elevation with real gas data is to analyze the percentage of pressure drop caused by elevations and to compare pressure drop percentages between two of the results.. 460MMscf amount of gas were used to transport from the compressor outlet which is started node to the delivery point which is located 177.1miles away from start node.

Table 1Experiment Results for Distance Vs Pressure

Total Distance (miles)	Pressure (psia)
0.0000	2325.0145
0.0000	2325.0145
10.0000	2289.1343
20.0000	2253.8641
30.0000	2219.0638
40.0000	2184.7236
50.0000	2150.7434
60.0000	2117.0132
70.0000	2083.5530
80.0000	2050.2928
90.0000	2017.1426
100.0000	1984.0424
110.0000	1950.9122
120.0000	1917.7420
130.0000	1884.5018
140.0000	1851.1215
150.0000	1817.5513
160.0000	1783.7411
170.0000	1749.6109
177.1000	1725.1508
177.1000	1725.1508

Length of Pipeline = 177.104 miles

Gas Flow rate = 460 MMscf

Pipeline Diameter = 24 inches

Compressor Outlet Temp = 212 F

Outlet Pressure = 2325 psi

Pressure drop percentage = 25.80%

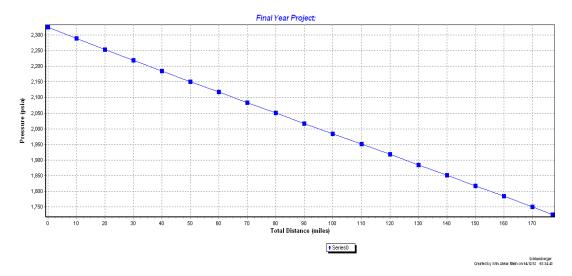


Figure 11 Pressure (Psi) Vs Pipeline Distance (miles) graph

The figure 11 above shown the relationships between Pressure vs total distance (length of pipeline). The constant slope was seen in the graph because the elevation of the pipeline was zero. It was observed that, 599.86 Psi of pressure will drop along the gas transportation pipeline which is caused by other factors such as compressor outlet temperature, pipeline diameters and pipeline roughness which will be discussed afterward. The 25.80% of pressure drop was observed from the simulation without elevation effect.

4.1.2 For elevation with actual gas field data,

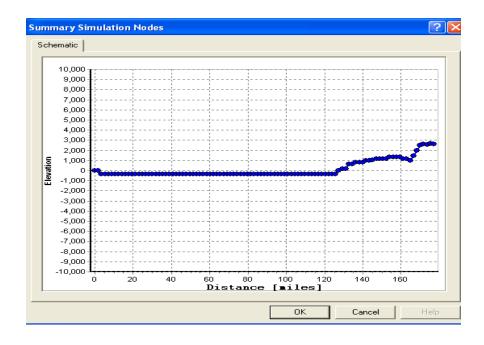


Figure 12 schematic pipeline diagram with elevation

The Figure 12 above shown the schematic pipeline diagram with elevation for real gas field. The purpose of simulation for zero real gas data with elevation is to analyze the percentage of pressure drop caused by elevations and to compare pressure drop percentages between two of the results.. 460MMscf amount of gas were used to transport from the compressor outlet which is started node to the delivery point which is located 177.1miles away from start node. In this scenario, the elevation of transportation pipeline was used as same in real gas field. Since the platform was located in offshore, the transportation pipeline start from 0 miles to 125 miles will be lied under subsea. The elevation of this portion will be zero since the seabed of oceanic was almost plain. Afterward, the elevation of pipeline on portion of 125 miles to 177.10 miles will be placed on the surface of uphill and downhill. The elevation of this portion will be positive and negative as seen in figure 12.

The simulation results can be seen in APPENDIX I. Author will be divided into three segments with zero elevation, uphill elevation and downhill elevation sections according to results. Below, Table 2-5shown different segments of pipeline elevation from the results.

Table 2 Results for subsea pipelines zero elevation

Total Distance	Total Pressure
Miles	Psi
0	2325.0145
10.6261	2304.3744
21.2511	2267.1041
30.1061	2236.4439
40.7311	2200.1137
51.3561	2164.1835

60.2112	2134.4633
70.8371	2099.0331
81.4631	2063.8529
90.317	2034.6327
100.9411	1999.6325
109.7911	1970.4623
120.4212	1935.3721
125.7311	1917.822

Table 3 Results for uphill elevation

Total Distance	Total Pressure
Miles	Psi
125.7311	1917.822
127.5023	1893.1818
132.8248	1838.2515

141.6754	1789.8912
152.3055	1744.2409
162.9259	1705.2806

Table 4 Results for downhill elevation

Total Distance	Total Pressure	
Miles	Psi	
162.9259	1705.2806	
164.6962	1709.7107	

Table 5 Results for uphill elevation

Total Distance	Total Pressure	170.0142	1609.23
Miles	Psi	171.7845	1596.55
164.6962	1709.7107	173.5644	1593.52
164.6962	1709.711	175.3347	1580.84
166.4687	1677.001	177.1045	1577.78
168.2411	1644.53	177.1045	1577.78

From the Table 2-5,

s zero elevation, (From 0 miles to 125.73 miles), Pipeline Segment 125.73 miles

Total pressure drop for = 407.178 psi

Total Pressure drop percentage = 17.51 %

Uphill elevation, (125.73 miles to 162.93 miles), Pipeline Segment 37.2 miles

Total pressure drop for = 212.5414 psi

Total Pressure drop percentage = 11.08 %

Downhill elevation, (162.93 miles to 164.70 miles), Pipeline Segment 1.7 miles

Total pressure drop for = -4.4301 psi

Total Pressure drop percentage = - 0.3 %

Uphill elevation, (164.70 miles to 177.10 miles), Pipeline Segment 12.4 miles

Total pressure drop for = 131.93 psi

Total Pressure drop percentage = 7.71%

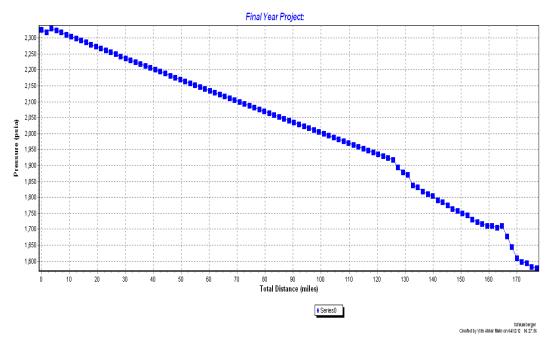


Figure 13 Pressure (Psi) Vs Pipeline Distance (Miles) graph

Based on the Figure 13, there are 4 portions of slopes can be seen according to different elevation of pipeline. Pipeline Segment 37.3 miles,11.80 percentage of pressure drop is a large number compare to 17.51 percentage of zero elevation with pipeline segment 125.73 because the pipeline segment of zero elevation is very much higher than uphill elevation. And again, downhill elevation with pipeline segments 1.7 miles have - 0.3 percentage because pressure is increase instead of decreasing in downhill elevation pipeline. It was observed that, the uphill elevation will greatly affect the pressure drop compare to zero elevation and downhill. The percentage of the pressure drop is increased compare to zero elevation case, because the upward elevation of pipeline will be result in losing some pressure due to specific gravity of the gas.

4.2 Sensitivity analysis on pipeline sizing factor

To analyze the effect of pressure drop due to pipeline sizing, author simulated the model using Gas transportation pipeline with elevation zero ft. By ranging the values of diameters, authors obtained the different types of pressure drop due to different types of pipeline sizing. "Figure 8", is the details simulation results of pressure drop according to different types of sizing ranging from 6 inch diameter to 56 inch diameter.

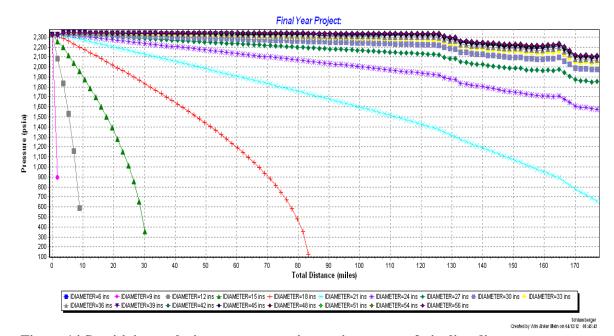


Figure 14 Sensitivity analysis on pressure using various types of pipeline diameters

The results from the sensitivity analysis of simulation can be seen in APPENDIX II. Below, Table 6 will be the summarized results of Pipeline diameter with percentage of pressure drop to analyze.

Table 6 Summarized simulation results of pipeline sizing vs pressure drop percentage

Pipeline	Pressure	Percentage
Diameter	drops	of pressure
(inch)	(psi)	drop
		(%)
6	N/A	N/A
9	N/A	N/A
12	1733.8548	N/A
15	1972.0823	N/A
18	2197.9947	94.6
21	1666.9404	<mark>71.7</mark>
24	747.2347	32.1
27	472.4629	20.3

350.0822	15.1
288.4918	12.4
255.2216	11
236.3315	10.1
225.2214	9.7
218.4914	9.2
214.3513	9.2
211.7713	9.2
210.1613	9.002
209.4613	9.009
	288.4918 255.2216 236.3315 225.2214 218.4914 214.3513 211.7713 210.1613

According to the results obtained from simulation, the minimum diameter which can handle for Gas transportation system with gas flow rate 400MMscf/D is, 12 inches diameter. But according to the Table 6, using diameter 6, 9, 12. 15 and 18 inches diameters were failure to deliver to a point which is located at 177.10 miles. Which is because, less than 20 inches diameter invalid to use for a long transportation gas pipeline. Therefore, the minimum diameter which can handle the flow rate of 400MMscf/D is 21 inches diameters pipeline which gave 71.1% pressure drop at the delivery point. Since, sustaining the maximum delivery pressure as possible at the delivery point is very important fact in oil and gas system, the most suitable diameter is 56 inches diameter pipeline with 9% pressure drop which can give minimum pressure drop But, economic consideration was also one of the factors in oil and gas system to make profit, most suitable pipeline diameters are 25 to 35 inches diameter. And it was observed that, the large amount of pressure drop will decrease as pipeline sizing increase. Choosing suitable diameter is one of the important factor to design gas transportation pipeline.

4.3 For analysis on roughness value

To analyze the frictional factors, the roughness of the pipeline is important parameter. The roughness of the pipeline is directly proportional to the friction. In this project, author simulated the gas transportation system with gas production rate of 440 MMscf/d. "APPENDIX VIII to IX," is the details for simulation results with various ranges of roughness and pressure drop.

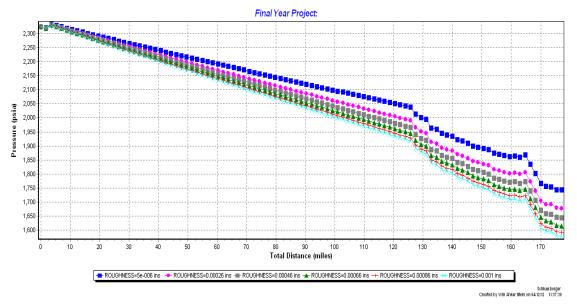


Figure 15 Sensitivity analysis on pressure drop using various roughness values

Table 7 Simulation results of different roughness values vs percentage of pressure drop

Roughness	Pressure drop	Pressure drop (%)
0.000005	581.00	<mark>25.00</mark>
0.00026	647.36	27.84
0.00046	681.71	29.32
0.00066	709.27	30.50
0.00086	732.63	31.51
0.001	727.23	<mark>31.278</mark>

Based on the results obtained, was observed that the pipeline with smallest value of roughness gave the smalles amount of pressure drop (25%) compare to other values which is 0.000005. The pressure drop due to the roughness occur due to the frictional force between wall of the pipe and gas flow are against the tendency of the flow toward. It may result in pressure drop along the gas pipeline. Most commonly used roughness is 0.0006 values which is used to calculated the frictional factor in oil and gas transportation pipeline. It was observed that, the roughness of pipeline also can give the additional pressure drop along the gas pipeline rather than elevation, pipeline sizing which are described above. It is very important to consider the roughness of the pipeline to calculate pressure drop along pipeline.

4.5 Sensitivity analysis on compressor discharge temperature

To run simulation on the sensitivity analysis of compressor discharge temperature, types of compressor with it maximum and minimum outlet temperature were studied and researched. It was obtained, the maximum and minimum outlet temperature of gas turbine compressor used in facilities were 180 F to 300F. APPENDIX X shown the results of different temperature outlet vs compressor discharge temperature.

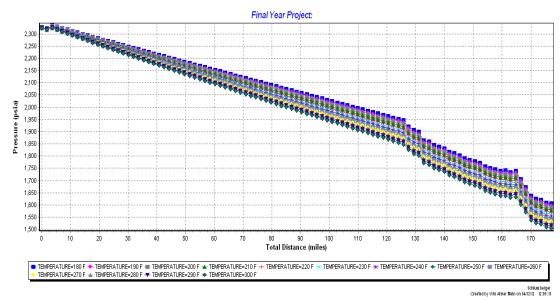


Figure 16 Sensitivity analysis on pressure drop using various compressor outlet temperature

Table 8 Simulation Results various inlet temp vs percentage of pressure drop

Temperature (F)	Pressure drop (%)
180	31.0
190	31.3
200	31.7
210	32.0
220	32.2
230	32.8
240	33.1
250	33.4
260	33.8
270	34.2
280	34.5
290	34.9
300	35.2

According to the simulation results by using different values of compressor outlet temperature, it was observed that the percentage of pressure drop for all the values of temperature is same from the result. By varying the outlet temperature of compressor is not a serious factor to consider in pipeline design. The compressor outlet temperature depending on the types of compressors which is installed for facilities. Based on the research, In oil and gas industry the maximum and minimum values of compressor outlet temperature for gas turbine would be 180F to 300F.

CHAPTER 5

CONCLUSION AND RECOMMENDATION

5.1 Conclusion

Real data from one of the Myanmar gas field will be used to simulate the pipeline design in PIPESIM Software. By simulating various different data on PIPESIM software and analyzing on the pressure drop results, it was found that there are four main major pressure drop factors which are affecting long distance transportation pipe line. Among these are

- increasing uphill elevation
- increasing roughness values
- increasing start node temperature, and
- decreasing pipe diameter.

In this report, author developed the graphical relationship within these factors after simulating the simple gas pipeline transportation designs. Furthermore, author could done some research for types of compressor with respect to outlet pressure and temperature to get better analysis result for compressor outlet temperature. As a conclusion, Pressure drop along the gas transportation pipeline is a common problem that always occur in transportation of oil and gas. These all the factors need to consider when we are designing the pipeline system to meet with customer desire pressure and flow rate.

5.2 Recommendation

In this report, the scope of work can be done within one semester to achieve objective. There are few recommendations for this project for further research. This project is focused only on four parameters which affecting pressure drop along gas transportation pipeline. For the future work, author would like to recommended that,

- To analyze on pressure drop caused by valves and pipeline fittings
- To make sensitivity analysis on various flow rate vs pressure drop
- To analyze on pressure drop caused by multi phases flow

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APPENDIX I Simulation Results for Real gas field data with elevation

Column1	Column2	54.8981	2152.2734	120.4212	1935.3721
Total	Columniz	56.6691	2132.2734	120.4212	1933.5721
Distance	Pressure (psia)				
(miles)		58.4402	2140.3933	123.9612	1923.672
		60.2112	2134.4633	125.7311	1917.822
Unit	Unit	61.9822	2128.5333	127.5023	1893.1818
0	2325.0145	63.7542	2122.6132	129.2725	1877.9417
0	2325.0145	65.5252	2116.7032	131.0424	1871.0917
1.7709	2318.6145	67.2962	2110.8032	132.8248	1838.2515
3.5428	2329.5745	69.0661	2104.9231	134.5947	1832.2714
5.3137	2323.2445	70.8371	2099.0331	136.3652	1817.0913
7.0847	2316.9344	72.6081	2093.1531	138.135	1810.1613
8.8556	2310.6444	74.3792	2087.283	139.9051	1804.1313
10.6261	2304.3744	76.1502	2081.423	141.6754	1789.8912
12.3971	2298.1143	77.9212	2075.5529	143.4453	1783.8311
14.1681	2291.8843	79.692	2069.7029	145.2153	1774.1311
15.9391	2285.6643	81.4631	2063.8529	146.9854	1762.621
17.7101	2279.4642	83.2341	2058.0028	148.7555	1756.511
19.4811	2273.2742	85.0051	2052.1528	150.5256	1750.4009
21.2511	2267.1041	86.7752	2046.3128	152.3055	1744.2409
23.0222	2260.9441	88.5462	2040.4727	154.0758	1729.1308
24.7932	2254.7941	90.317	2034.6327	155.8456	1722.9707
26.5642	2248.664	92.0881	2028.8027	157.6157	1716.7807
28.3352	2242.544	93.8591	2022.9626	159.3856	1710.5907
30.1061	2236.4439	95.6301	2017.1326	161.1559	1711.4907
31.8771	2230.3539	97.4011	2011.2925	162.9259	1705.2806
33.6481	2224.2739	99.1722	2005.4625	164.6962	1709.7107
35.4182	2218.2138	100.9411	1999.6325	166.4687	1677.0005
37.1892	2212.1738	102.7112	1993.8024	168.2411	1644.5303
38.9602	2206.1338	104.4811	1987.9724	170.0142	1609.23
40.7311	2200.1137	106.2511	1982.1324	171.7845	1596.55
42.5021	2194.0937	108.0212	1976.3023	173.5644	1593.5199
44.2731	2188.0936	109.7911	1970.4623	175.3347	1580.8399
46.0441	2182.1036	111.5612	1964.6223	177.1045	1577.7798
47.8152	2176.1236	113.3411	1958.7422	177.1045	1577.7798
49.5852	2170.1535	115.1112	1952.9022		
51.3561	2164.1835	116.8811	1947.0621		
53.1271	2158.2235	118.6511	1941.2221		

APPENDIX II

APPENDIX II Simulation results of various pipeline sizing vs pressure drop

Distance 🔻	Pressure 🔻	Distance2	Pressure3	Distance4	Pressure5	Distance6	Pressure7
(miles)	(psi)	(miles)	(psi)	(miles)	(psi)	(miles)	(psi)
D (inch)	6	D (inch)	9	D (inch)	12	D (inch)	15
0	2325.0145	0	2325.0145	0	2325.0145	0	2325.0145
0	2325.0145	0	2325.0145	0	2325.0145	0	2325.0145
2338.09		9350.35	895.8876	9350.35	2085.623	9350.35	2251.974
		11689.8		18706	1835.7114	18706	2193.8837
				28056.3	1532.8096	28056.3	2117.4132
				37407.2	1159.4172	37407.2	2038.7327
				46757.6	591.1597	46757.6	1957.6022
				51431.7		56105.8	1873.7017
						65456.7	1786.6011
						74807.6	1695.7606
						84158.4	1600.51
						93509.3	1500.0294
						102860	1393.2487
						112206	1278.528
						121557	1153.1672
						130908	1013.4763
						140259	852.1023
						149610	652.7031
						158960	352.9322
						163635	

APPENDIX III

APPENDIX III Simulation results of various pipeline sizing vs pressure drop

Distance8	Pressure9	Distance10	Pressure11 💌	Distance12	Pressure13
(miles)	(psi)	(miles)	(psi)	(miles)	(psi)
D (inch)	18 2325.0145	D (inch)	21 2325.0145	D (inch)	24 2325.0145
0	2325.0145	0	2325.0145	0	2325.0145
9350.35	2296.7543	9350.35	2312.2744	9350.35	2318.6145
18706	2285.4643	18706	2316.8244	18706	2329.5745
28056.3	2256.9841	28056.3	2304.1544	28056.3	2323.2445
37407.2	2228.3139	37407.2	2291.4943 2278.8242	37407.2 46757.6	2316.9344
46757.6 56105.8	2199.4437 2170.3735	46757.6 56105.8	2266.1741	56105.8	2310.6444 2304.3744
65456.7	2141.0834	65456.7	2253.5041	65456.7	2298.1143
74807.6	2111.5432	74807.6	2240.834	74807.6	2291.8843
84158.4	2081.763	84158.4	2228.1639	84158.4	2285.6643
93509.3	2051.7228	93509.3	2215.4838	93509.3	2279.4642
102860 112206	2021.4026 1990.8024	102860 112206	2202.8037 2190.1037	102860 112206	2273.2742 2267.1041
121557	1959.8822	121557	2177.4036	121557	2260.9441
130908	1928.622	130908	2164.6735	130908	2254.7941
140259	1897.0318	140259	2151.9334	140259	2248.664
149610	1865.0916	149610	2139.1833	149610	2242.544
158960	1832.8014	158960	2126.4133	158960	2236.4439
168311 177662	1800.1312 1767.041	168311 177662	2113.6432 2100.8531	168311 177662	2230.3539 2224.2739
187008	1733.5308	187008	2088.063	187008	2218.2138
196359	1699.5206	196359	2075.2429	196359	2212.1738
205710	1665.0104	205710	2062.4129	205710	2206.1338
215060	1629.9402	215060	2049.5628	215060	2200.1137
224411 233762	1594.2799	224411	2036.6927 2023.7926	224411	2194.0937
243113	1557.9797 1520.9795	233762 243113	2010.8725	233762 243113	2188.0936 2182.1036
252464	1483.2293	252464	1997.9325	252464	2176.1236
261810	1444.699	261810	1984.9624	261810	2170.1535
271160	1405.2988	271160	1971.9623	271160	2164.1835
280511	1364.9585	280511 289862	1958.9322	280511	2158.2235
289862 299213	1323.5883 1281.078	299213	1945.8621 1932.7621	289862 299213	2152.2734 2146.3334
308564	1237.2577	308564	1919.622	308564	2140.3933
317915	1191.9974	317915	1906.4419	317915	2134.4633
327266	1145.1571	327266	1893.2318	327266	2128.5333
336622	1096.5168	336622	1879.9817	336622	2122.6132
345973 355324	1045.8465	345973	1866.7016	345973	2116.7032
364669	992.7732 936.9238	355324 364669	1853.3816 1840.0415	355324 364669	2110.8032 2104.9231
374020	877.6585	374020	1826.6514	374020	2099.0331
383371	814.1511	383371	1813.2113	383371	2093.1531
392722	745.3326	392722	1799.7312	392722	2087.283
402073	669.7272	402073	1786.2111	402073	2081.423
411424 420774	584.4346 483.889	411424 420774	1772.6311 1759.001	411424 420774	2075.5529 2069.7029
430125	355.6702	430125	1745.3209	430125	2063.8529
439476	127.0198	439476	1731.5708	439476	2058.0028
441814		448827	1717.7707	448827	2052.1528
		458173	1703.9106	458173	2046.3128
		467524 476874	1689.9805 1675.9805	467524 476874	2040.4727 2034.6327
		486225	1661.9004	486225	2028.8027
		495576	1647.7503	495576	2022,9626
		504927	1633.5102	504927	2017.1326
		514278	1619.2001	514278	2011.2925
		523629	1604.8	523629	2005.4625
		532969 542315	1590.3199 1575.7498	532969 542315	1999.6325 1993.8024
		551660	15/3.7498	551660	1987.9724
		561006	1546.3496	561006	1982.1324
		570352	1531.5096	570352	1976.3023
		579697	1516.5695	579697	1970.4623
		589043 598441	1501.5194 1486.2693	589043 598441	1964.6223 1958.7422
		607787	1486.2693	607787	1958.7422
		617132	1455.6091	617132	1947.0621
		626478	1440.089	626478	1941.2221
		635824	1424.4389	635824	1935.3721
		645169	1408.6588	645169	1929.522
		654515 663860	1392.7287 1376.6486	654515 663860	1923.672 1917.822
		673212	1346.9384	673212	1893.1818
		682559	1323.7783	682559	1877.9417
		691904	1306.3581	691904	1871.0917
		701315	1270.6179	701315	1838.2515
		710660 720008	1253.2378	710660 720008	1832.2714 1817.0913
		720008	1229.4077 1210.8776	720008	1817.0913
		738699	1192.7074	738699	1804.1313
		748046	1168.9273	748046	1789.8912
		757391	1150.1972	757391	1783.8311
		766737	1128.897	766737	1774.1311
		776083 785429	1106.1969 1086.5668	776083 785429	1762.621 1756.511
		794775	1066.6167	794775	1750.4009
		804173	1046.2065	804173	1744.2409
		813520	1020.2364	813520	1729.1308
		822865	999.0952	822865	1722.9707
		832211	977.5191	832211	1716.7807
		841556 850903	955.472 936.8168	841556 850903	1710.5907 1711.4907
		860249	913.7687	860249	1705.2806
		869596	895.7186	869596	1709.7107
		878955	857.8854	878955	1677.0005
		888313	819.5441	888313	1644.5303
		897675	779.0799	897675	1609.23
		907022 916420	748.4147 720.9115	907022 916420	1596.55 1593.5199
		925767	688.1563	925767	1580.8399
		935112	658.0741	935112	1577.7798
		935112	658.0741	935112	1577.7798

APPENDIX IV

APPENDIX IV Simulation results of various pipeline sizing vs pressure drop

Distance14	Pressure15	Distance16	Pressure17	Distance18	Pressure19
(miles)	(psi)	(miles)	(psi)	(miles)	(psi)
D (inch)	27 2325.0145	D (inch)	30 2325.0145	D (inch)	33 2325.0145
0	2325.0145	0	2325.0145	0	2325.0145
9350.35	2321.5145	9350.35	2322.9745	9350.35	2323.7645
18706	2335.4246	18706	2338.3646	18706	2339.9546
28056.3 37407.2	2331.9745 2328.5445	28056.3 37407.2	2336.3546 2334.3646	28056.3 37407.2	2338.7246 2337.5046
46757.6	2325.1345	46757.6	2332.3845	46757.6	2336.2946
56105.8	2321.7345	56105.8	2330.4145	56105.8	2335.0846
65456.7	2318.3545	65456.7	2328.4545	65456.7	2333.8846
74807.6 84158.4	2314.9844 2311.6344	74807.6 84158.4	2326.5145 2324.5745	74807.6 84158.4	2332.6945 2331.5145
93509.3	2311.6344	93509.3	2322.6445	93509.3	2331.5145
102860	2304.9744	102860	2320.7245	102860	2329.1745
112206	2301.6644	112206	2318.8145	112206	2328.0045
121557	2298.3643	121557	2316.9144	121557	2326.8545
130908 140259	2295.0743 2291.8043	130908 140259	2315.0244 2313.1444	130908 140259	2325.7045 2324.5545
149610	2288.5343	149610	2313.1444	149610	2323 4245
158960	2285.2943	158960	2309.4144	158960	2322.2945
168311	2282.0542	168311	2307.5644	168311	2321.1745
177662	2278.8342	177662	2305.7144	177662	2320.0545
187008 196359	2275.6242 2272.4242	187008 196359	2303.8844 2302.0544	187008 196359	2318.9445 2317.8345
205710	2269.2442	205710	2302.0344	205710	2316.7344
215060	2266.0641	215060	2298.4243	215060	2315.6344
224411	2262.8941	224411	2296.6143	224411	2314.5444
233762	2259.7441	233762	2294.8243	233762	2313.4644
243113 252464	2256.5941 2253.4541	243113 252464	2293.0243 2291.2443	243113 252464	2312.3744 2311.3044
261810	2250.334	261810	2289.4643	261810	2310.2244
271160	2247.214	271160	2287.6943	271160	2309.1644
280511	2244.104	280511	2285.9243	280511	2308.0944
289862 299213	2240.994 2237.904	289862 299213	2284.1742 2282.4142	289862 299213	2307.0344 2305.9844
299213 308564	2237.904 2234.8139	299213 308564	2282.4142 2280.6742	299213 308564	2305.9844
317915	2231.7339	317915	2278.9342	317915	2303.8844
327266	2228.6639	327266	2277.2042	327266	2302.8444
336622	2225.6039	336622	2275.4742	336622	2301.8144
345973	2222.5539	345973	2273.7542	345973	2300.7743
355324 364669	2219.5138 2216.4838	355324 364669	2272.0342 2270.3242	355324 364669	2299.7443 2298.7243
374020	2213.4538	374020	2268.6241	374020	2297.6943
383371	2210.4338	383371	2266.9241	383371	2296.6743
392722	2207.4238	392722	2265.2341	392722	2295.6643
402073 411424	2204.4237 2201.4237	402073 411424	2263.5441 2261.8541	402073 411424	2294.6543 2293.6443
420774	2198.4337	420774	2260.1741	420774	2292.6343
430125	2195.4437	430125	2258.5041	430125	2291.6243
439476	2192.4637	439476	2256.8341	439476	2290.6243
448827	2189.4937	448827	2255.1641	448827	2289.6243
458173 467524	2186.5236 2183.5636	458173 467524	2253.5041 2251.844	458173 467524	2288.6343 2287.6443
476874	2180.6036	476874	2250.184	476874	2286.6543
486225	2177.6536	486225	2248.534	486225	2285.6643
495576	2174.7036	495576	2246.884	495576	2284.6742
504927	2171.7535	504927	2245.234	504927	2283.6942
514278 523629	2168.8135 2165.8835	514278 523629	2243.594 2241.954	514278 523629	2282.7142 2281.7342
532969	2162.9535	532969	2240.324	532969	2280.7542
542315	2160.0235	542315	2238.694	542315	2279.7842
551660	2157.1035	551660	2237.064	551660	2278.8142
561006 570352	2154.1834 2151.2634	561006 570352	2235.4339 2233.8139	561006 570352	2277.8442 2276.8742
579697	2148.3534	579697	2232.1939	579697	2275.9042
589043	2145.4534	589043	2230.5839	589043	2274.9442
598441	2142.5334	598441	2228.9639	598441	2273.9742
607787	2139.6333	607787 617132	2227.3539	607787 617132	2273.0142 2272.0642
617132 626478	2136.7333 2133.8433	617132 626478	2225.7439 2224.1439	617132 626478	2272.0642 2271.1042
635824	2130.9533	635824	2222.5339	635824	2270.1542
645169	2128.0633	645169	2220.9339	645169	2269.1942
654515	2125.1733	654515	2219.3438	654515	2268.2441
663860 673212	2122.2932 2098.5031	663860 673212	2217.7438 2194.0737	663860 673212	2267.2941 2243.534
682559	2085.193	682559	2181.4736	682559	2231.2039
691904	2081.253	691904	2178.7736	691904	2229.1139
701315	2048.2628	701315	2145.3634	701315	2195.2737
710660	2045.3428	710660	2143.7434	710660	2194.3137
720008 729353	2032.1027 2028.1426	720008 729353	2131.2133 2128.5033	720008 729353	2182.0636 2179.9736
738699	2025.2226	738699	2126.8933	738699	2179.0136
748046	2013.0226	748046	2115.4532	748046	2167.8835
757391	2010.0925	757391	2113.8432	757391	2166.9235
766737 776083	2003.0425 1993.9524	766737 776083	2107.8631 2099.7031	766737 776083	2161.4435 2153.7134
785429	1993.9524	785429	2098.0931	7/6083	2152.7534
794775	1988.0724	794775	2096.4731	794775	2151.7934
804173	1985.1124	804173	2094.8531	804173	2150.8334
813520	1971.9323	813520	2082.343	813520	2138.5833
822865 832211	1968.9823 1966.0323	822865 832211	2080.723 2079.103	822865 832211	2137.6233 2136.6633
832211 841556	1966.0323	832211 841556	2079.103	832211 841556	2135.7033
850903	1968.3123	850903	2084.603	850903	2143.7934
860249	1965.3723	860249	2082.993	860249	2142.8434
869596	1974.7423	869596	2094.5231	869596	2155.5134
878955	1941.1121	878955	2060.1328	878955	2120.5532
888313 897675	1907.7519 1871.0817	888313 897675	2026.0326 1988.3724	888313 897675	2085.893 2047.5228
907022	1860.7916	907022	1978.9523	907022	2038.4727
916420	1861.8116	916420	1981.6524	916420	2042.0227
925767	1851.5415	925767	1972.2323	925767	2032.9727
935112	1852.5516	935112	1974.9323	935112	2036.5227
935112	1852.5516	935112	1974.9323	935112	2036.5227

 $\label{eq:appendix} \mbox{APPENDIX V}$ APPENDIX V Simulation results of various pipeline sizing vs pressure drop

Distance20		Distance22			
(miles)	(psi)	(miles)	(psi)	(miles)	(psi)
D (inch)	36 2325.0145	D (inch)	39 2325.0145	D (inch)	42 2325.0145
0	2325.0145	0	2325.0145	0	2325.0145
9350.35	2324.2145	9350.35	2324.4745	9350.35	2324.6445
18706	2340.8746	18706	2341.4346	18706	2341.7846
28056.3	2340.0846	28056.3	2340.9046	28056.3	2341.4246
37407.2	2339.3046	37407.2	2340.3846	37407.2	2341.0746
46757.6	2338.5246	46757.6	2339.8746	46757.6	2340.7146
56105.8	2337.7546	56105.8	2339.3646	56105.8	2340.3646
65456.7	2336.9946	65456.7	2338.8546	65456.7	2340.0246
74807.6	2336.2346	74807.6	2338.3546	74807.6	2339.6746
84158.4	2335.4746	84158.4	2337.8546	84158.4	2339.3346
93509.3	2334.7246	93509.3	2337.3546	93509.3	2338.9946
102860	2333.9846	102860	2336.8646	102860	2338.6546
112206	2333.2446	112206	2336.3746	112206	2338.3246
121557	2332.5045	121557	2335.8846	121557	2337.9946
130908	2331.7745	130908	2335.4046 2334.9246	130908	2337.6646 2337.3346
140259 149610	2331.0545 2330.3245	140259 149610	2334.4446	140259 149610	2337.0146
158960	2329.6145	158960	2333.9746	158960	2336.6946
168311	2328.8945	168311	2333.5046	168311	2336.3746
177662	2328.1845	177662	2333.0346	177662	2336.0546
187008	2327.4845	187008	2332.5745	187008	2335.7346
196359	2326,7845	196359	2332.1045	196359	2335,4246
205710	2326.0845	205710	2331.6445	205710	2335.1046
215060	2325.3845	215060	2331.1945	215060	2334.7946
224411	2324.6945	224411	2330.7345	224411	2334.4846
233762	2324.0045	233762	2330.2845	233762	2334.1846
243113	2323.3245	243113	2329.8345	243113	2333.8746
252464	2322.6445	252464	2329.3845	252464	2333.5746
261810	2321.9645	261810	2328.9445	261810	2333.2646
271160	2321.2945	271160	2328.4945	271160	2332.9645
280511	2320.6145	280511	2328.0545	280511	2332.6645
289862	2319.9545	289862	2327.6145	289862 299213	2332.3745
299213	2319.2845 2318.6245	299213	2327.1845		2332.0745
308564 317915	2318.6245	308564 317915	2326.7445 2326.3145	308564 317915	2331.7845 2331.4845
327266	2317.3045	327266	2325 8845	327266	2331.1945
336622	2316.6544	336622	2325.4545	336622	2330.9045
345973	2316.0044	345973	2325,0245	345973	2330.6145
355324	2315.3544	355324	2324.5945	355324	2330.3245
364669	2314.7044	364669	2324.1745	364669	2330.0345
374020	2314.0544	374020	2323.7445	374020	2329.7445
383371	2313.4144	383371	2323.3245	383371	2329.4645
392722	2312.7744	392722	2322.9045	392722	2329.1745
402073	2312.1344	402073	2322.4845	402073	2328.8945
411424	2311.5044	411424	2322.0745	411424	2328.6045
420774	2310.8644	420774	2321.6545	420774	2328.3245
430125	2310.2344	430125	2321.2345	430125	2328.0445
439476	2309.6044	439476	2320.8245	439476	2327.7645
448827	2308.9744	448827	2320.4145	448827	2327.4845
458173	2308.3444	458173	2320.0045	458173	2327.2045
467524	2307.7244	467524	2319.5945	467524	2326.9245
476874 486225	2307.0944 2306.4744	476874 486225	2319.1845	476874 486225	2326.6545 2326.3745
495576	2305.8544	495576	2318.7745 2318.3645	495576	2326.1045
504927	2305.2344	504927	2317.9645	504927	2325.8245
514278	2304.6144	514278	2317.5545	514278	2325.5545
523629	2304.0044	523629	2317.1545	523629	2325.2745
532969	2303.3944	532969	2316.7544	532969	2325.0045
542315	2302.7744	542315	2316.3544	542315	2324.7345
551660	2302.1644	551660	2315.9544	551660	2324.4645
561006	2301.5544	561006	2315.5544	561006	2324.1945
570352	2300.9444	570352	2315.1544	570352	2323.9245
579697	2300.3443	579697	2314.7544	579697	2323.6545
589043	2299.7343	589043	2314.3544	589043	2323.3845
598441	2299.1243	598441	2313.9644	598441	2323.1145
607787	2298.5243	607787	2313.5644	607787	2322.8445
617132	2297.9243	617132	2313.1744	617132	2322.5745 2322.3045
626478	2297.3243	626478 635824	2312.7744	626478	2322.3045 2322.0445
635824 645169	2296.7243 2296.1243	645169	2312.3844 2311.9944	635824 645169	2322.0445
654515	2295.5243	654515	2311.5944	654515	2321.7745
663860	2294.9343	663860	2311.3944	663860	2321.3045
673212	2271.0042	673212	2287.1043	673212	2296.9543
682559	2258.7741	682559	2274.8842	682559	2284.7242
691904	2257.0141	691904	2273.3142	691904	2283.2542
701315	2222.7839	701315	2238.744	701315	2248.384
710660	2222.1839	710660	2238.344	710660	2248.114
720008	2210.0238	720008	2226.2039	720008	2235.9639
729353	2208.2638	729353	2224.6439	729353	2234.5139
738699	2207.6638	738699	2224.2439	738699	2234.2439
748046	2196.6637	748046	2213.2838	748046	2223.2839
757391	2196.0637	757391	2212.8838	757391	2223.0139
766737	2190.8337	766737	2207.7938	766737	2217.9938
776083	2183.3036	776083	2200.3637	776083	2210.6038
785429	2182.7036	785429	2199.9737	785429	2210.3338
504555	2182.1036	794775	2199.5737	794775	2210.0738
794775	2181.4936	804173	2199.1837	804173	2209.8038
804173	2160 2125	813520	2187.0536	813520	2197.6637
804173 813520	2169.3435		2186.6636	822865	2197.3937
804173 813520 822865	2168.7435	822865			
804173 813520 822865 832211	2168.7435 2168.1435	822865 832211	2186.2636	832211	2197.1237
804173 813520 822865 832211 841556	2168.7435 2168.1435 2167.5435	822865 832211 841556	2186.2636 2185.8736	832211 841556	2197.1237 2196.8537
804173 813520 822865 832211 841556 850903	2168.7435 2168.1435 2167.5435 2176.1936	822865 832211 841556 850903	2186.2636 2185.8736 2194.8737	832211 841556 850903	2197.1237 2196.8537 2206.1038
804173 813520 822865 832211 841556 850903 860249	2168.7435 2168.1435 2167.5435 2176.1936 2175.5936	822865 832211 841556 850903 860249	2186.2636 2185.8736 2194.8737 2194.4837	832211 841556 850903 860249	2197.1237 2196.8537 2206.1038 2205.8438
804173 813520 822865 832211 841556 850903 860249 869596	2168.7435 2168.1435 2167.5435 2176.1936 2175.5936 2188.9337	822865 832211 841556 850903 860249 869596	2186.2636 2185.8736 2194.8737 2194.4837 2208.2438	832211 841556 850903 860249 869596	2197.1237 2196.8537 2206.1038 2205.8438 2219.9038
804173 813520 822865 832211 841556 850903 860249 869596 878955	2168.7435 2168.1435 2167.5435 2176.1936 2175.5936 2188.9337 2153.5534	822865 832211 841556 850903 860249 869596 878955	2186.2636 2185.8736 2194.8737 2194.4837 2208.2438 2172.5135	832211 841556 850903 860249 869596 878955	2197.1237 2196.8537 2206.1038 2205.8438 2219.9038 2183.8636
804173 813520 822865 832211 841556 850903 860249 869596 878955 888313	2168.7435 2168.1435 2167.5435 2176.1936 2175.5936 2188.9337 2153.5534 2118.4532	822865 832211 841556 850903 860249 869596 878955 888313	2186.2636 2185.8736 2194.8737 2194.4837 2208.2438 2172.5135 2137.0433	832211 841556 850903 860249 869596 878955 888313	2197.1237 2196.8537 2206.1038 2205.8438 2219.9038 2183.8636 2148.0834
804173 813520 822865 832211 841556 850903 860249 869596 878955 888313 897675	2168.7435 2168.1435 2167.5435 2176.1936 2175.5936 2188.9337 2153.5534 2118.4532 2079.523	822865 832211 841556 850903 860249 869596 878955 888313 897675	2186.2636 2185.8736 2194.8737 2194.4837 2208.2438 2172.5135 2137.0433 2097.6831	832211 841556 850903 860249 869596 878955 888313 897675	2197.1237 2196.8537 2206.1038 2205.8438 2219.9038 2183.8636 2148.0834 2108.3631
804173 813520 822865 832211 841556 850903 860249 869596 878955 888313 897675	2168.7435 2168.1435 2167.5435 2176.1936 2175.5936 2188.9337 2153.5534 2118.4532 2079.523 2070.6229	822865 832211 841556 850903 860249 869596 878955 888313 897675 907022	2186.2636 2185.8736 2194.8737 2194.4837 2208.2438 2172.5135 2137.0433 2097.6831 2088.863	832211 841556 850903 860249 869596 878955 888313 897675 907022	2197.1237 2196.8537 2206.1038 2205.8438 2219.9038 2183.8636 2148.0834 2108.3631 2099.5731
804173 813520 822865 832211 841556 850903 860249 869596 878955 888313 897675 907022 916420	2168.7435 2168.1435 2167.5435 2177.5435 2175.5936 2188.9337 2153.5534 2118.4532 2079.523 2070.6229 2074.6529	822865 832211 841556 850903 860249 869596 878955 888313 897675 907022 916420	2186.2636 2185.8736 2194.8737 2194.4837 2208.2438 2172.5135 2137.0433 2097.6831 2088.863 2093.1831	832211 841556 850903 860249 869596 878955 888313 897675 907022 916420	2197.1237 2196.8537 2206.1038 2205.8438 2219.9038 2183.8636 2148.0834 2108.3631 2099.5731 2104.0731
804173 813520 822865 832211 841556 850903 860249 869596 878955 888313 897675	2168.7435 2168.1435 2167.5435 2176.1936 2175.5936 2188.9337 2153.5534 2118.4532 2079.523 2070.6229	822865 832211 841556 850903 860249 869596 878955 888313 897675 907022	2186.2636 2185.8736 2194.8737 2194.4837 2208.2438 2172.5135 2137.0433 2097.6831 2088.863	832211 841556 850903 860249 869596 878955 888313 897675 907022	2197.1237 2196.8537 2206.1038 2205.8438 2219.9038 2183.8636 2148.0834 2108.3631 2099.5731

APPENDIX VI Simulation results of various pipeline sizing vs pressure drop

Distance26 (miles)	Pressure27 (psi)	Distance28 (miles)	Pressure29 (psi)	Distance30 (miles)	Pressure31 (psi)
D (inch)	45	D (inch)	48	D (inch)	51
0	2325.0145	0	2325.0145	0	2325.0145
0	2325.0145	0	2325.0145	0	2325.0145
9350.35	2324.7545	9350.35	2324.8245	9350.35	2324.8745
18706 28056.3	2342.0146 2341.7646	18706 28056.3	2342.1846 2342.0046	18706 28056.3	2342.2946 2342.1646
37407.2	2341.5146	37407.2	2341.8146	37407.2	2342.0346
46757.6	2341.2646	46757.6	2341.6446	46757.6	2341.9046
56105.8	2341.0246	56105.8	2341.4646	56105.8	2341.7746
65456.7	2340.7746	65456.7	2341.2846	65456.7	2341.6446
74807.6	2340.5346	74807.6	2341.1146	74807.6	2341.5146
84158.4	2340.2946	84158.4	2340.9446	84158.4	2341.3846
93509.3 102860	2340.0546 2339.8246	93509.3 102860	2340.7746 2340.6046	93509.3 102860	2341.2646 2341.1346
112206	2339.5846	112206	2340.4346	112206	2341.0146
121557	2339.3546	121557	2340.2646	121557	2340.8946
130908	2339.1246	130908	2340.1046	130908	2340.7746
140259	2338.8946	140259	2339.9346	140259	2340.6546
149610	2338.6746	149610	2339.7746	149610	2340.5346
158960	2338.4446	158960	2339.6146	158960	2340.4146
168311 177662	2338.2246 2337.9946	168311 177662	2339.4546 2339.2946	168311 177662	2340.2946 2340.1846
187008	2337.7746	187008	2339.1346	187008	2340.0646
196359	2337.5546	196359	2338.9746	196359	2339.9546
205710	2337.3346	205710	2338.8246	205710	2339.8346
215060	2337.1246	215060	2338.6646	215060	2339.7246
224411	2336.9046	224411	2338.5146	224411	2339.6046
233762	2336.6946	233762	2338.3546	233762	2339.4946
243113 252464	2336.4746 2336.2646	243113 252464	2338.2046 2338.0546	243113 252464	2339.3846 2339.2746
261810	2336.2646	261810	2337.9046	261810	2339.1646
271160	2335.8446	271160	2337.7546	271160	2339.0546
280511	2335.6346	280511	2337.6046	280511	2338.9446
289862	2335.4246	289862	2337.4546	289862	2338.8346
299213	2335.2246	299213	2337.3046	299213	2338.7346
308564	2335.0146	308564	2337.1646 2337.0146	308564	2338.6246
317915 327266	2334.8046 2334.6046	317915 327266	2337.0146 2336.8646	317915 327266	2338.5146 2338.4046
336622	2334.4046	336622	2336.7246	336622	2338.3046
345973	2334.1946	345973	2336.5746	345973	2338.1946
355324	2333.9946	355324	2336.4346	355324	2338.0946
364669	2333.7946	364669	2336.2846	364669	2337.9846
374020	2333.5946	374020	2336.1446	374020	2337.8846
383371	2333.3946	383371	2336.0046	383371	2337.7746
392722 402073	2333.1946 2332.9945	392722 402073	2335.8646 2335.7246	392722 402073	2337.6746 2337.5746
411424	2332.8045	411424	2335.5746	411424	2337.4646
420774	2332.6045	420774	2335.4346	420774	2337.3646
430125	2332.4045	430125	2335.2946	430125	2337.2646
439476	2332.2145	439476	2335.1546	439476	2337.1646
448827	2332.0145	448827	2335.0146	448827	2337.0546
458173	2331.8245	458173	2334.8746	458173	2336.9546
467524 476874	2331.6245 2331.4345	467524 476874	2334.7446 2334.6046	467524 476874	2336.8546 2336.7546
486225	2331.2445	486225	2334.4646	486225	2336.6546
495576	2331.0545	495576	2334.3246	495576	2336.5546
504927	2330.8545	504927	2334.1946	504927	2336.4546
514278	2330.6645	514278	2334.0546	514278	2336.3546
523629	2330.4745	523629	2333.9146	523629	2336.2546
532969	2330.2845	532969	2333.7846	532969	2336.1546
542315 551660	2330.0945 2329.9045	542315 551660	2333.6446 2333.5046	542315 551660	2336.0546 2335.9546
561006	2329.7145	561006	2333.3746	561006	2335.8546
570352	2329.5245	570352	2333.2346	570352	2335.7546
579697	2329.3445	579697	2333.1046	579697	2335.6546
589043	2329.1545	589043	2332.9645	589043	2335.5546
598441	2328.9645	598441	2332.8345	598441	2335.4646
607787 617132	2328.7745 2328.5845	607787 617132	2332.7045 2332.5645	607787 617132	2335.3646 2335.2646
626478	2328.5845	626478	2332.4345	626478	2335.1646
635824	2328.2145	635824	2332.2945	635824	2335.0646
645169	2328.0345	645169	2332.1645	645169	2334.9746
654515	2327.8445	654515	2332.0345	654515	2334.8746
663860	2327.6545	663860	2331.9045	663860	2334.7746
673212 682559	2303.2144	673212 682559	2307.3044	673212	2310.0444
691904	2290.9343 2289.5343	691904	2294.9743 2293.6243	682559 691904	2297.6643 2296.3443
701315	2254.4041	701315	2258.2641	701315	2260.7841
710660	2254.2241	710660	2258.1341	710660	2260.6841
720008	2242.034	720008	2245.904	720008	2248.404
729353	2240.644	729353	2244.564	729353	2247.084
738699	2240.454	738699	2244.424	738699	2246.994
748046	2229.4839	748046	2233.4039 2233.2739	748046	2235.9339
757391 766737	2229.2939 2224.3039	757391 766737	2228.3039	757391 766737	2235.8339 2230.8639
776083	2216.9338	776083	2220.9139	776083	2223.4639
785429	2216.7438	785429	2220.7839	785429	2223.3639
794775	2216.5538	794775	2220.6438	794775	2223.2639
804173	2216.3638	804173	2220.5138	804173	2223.1639
813520	2204.1937	813520	2208.2938	813520	2210.9138
822865 832211	2204.0037 2203.8137	822865	2208.1638 2208.0238	822865 832211	2210.8138
832211 841556	2203.8137	832211 841556	2208.0238	832211 841556	2210.7138 2210.6138
850903	2213.0538	850903	2217.4338	850903	2220.2538
860249	2212.8638	860249	2217.3038	860249	2220.1538
869596	2227.1439	869596	2231.7439	869596	2234.7139
878955	2190.8437	878955	2195.2437	878955	2198.0437
888313	2154.8234	888313	2159.0135	888313	2161.6635
897675	2114.8332	897675	2118.8032	897675	2121.2732
907022 916420	2106.0531 2110.6732	907022 916420	2110.0232 2114.7332	907022 916420	2112.4832 2117.2532
925767	2101.9031	925767	2114.7332	925767	2117.2532
935112	2106.5231	935112	2110.6632	935112	2113.2432
935112	2106.5231	935112	2110.6632	935112	2113.2432

APPENDIX VII

APPENDIX VII Simulation results of various pipeline sizing vs pressure drop

Distance32 (miles)	Pressure33 (psi)	Distance34 (miles)	Pressure35 (psi)
D (inch)	54	D (inch)	56
0	2325.0145 2325.0145	0	2325.0145 2325.0145
9350.35	2324.9145	9350.35	2324.9245
18706	2342.3846	18706	2342.4346
28056.3 37407.2	2342.2846 2342.1846	28056.3 37407.2	2342.3446 2342.2646
46757.6	2342.0846	46757.6	2342.1846
56105.8	2341.9846	56105.8	2342.1046
65456.7 74807.6	2341.8946 2341.7946	65456.7 74807.6	2342.0246 2341.9446
84158.4	2341.7046	84158.4	2341.8646
93509.3 102860	2341.6146 2341.5146	93509.3 102860	2341.7846 2341.7146
112206	2341.3146	112206	2341.7146
121557	2341.3346	121557	2341.5546
130908 140259	2341.2446 2341.1546	130908 140259	2341.4846 2341.4046
149610	2341.0646	149610	2341.3346
158960	2340.9746	158960	2341.2646
168311 177662	2340.8946 2340.8046	168311 177662	2341.1946 2341.1146
187008	2340.7146	187008	2341.0446
196359	2340.6346	196359	2340.9746
205710 215060	2340.5446 2340.4646	205710 215060	2340.9046 2340.8346
224411	2340.3746	224411	2340.7646
233762	2340.2946	233762	2340.6946
243113 252464	2340.2146 2340.1346	243113 252464	2340.6246 2340.5646
261810	2340.0446	261810	2340.3646
271160	2339.9646	271160	2340.4246
280511 289862	2339.8846 2339.8046	280511 289862	2340.3546 2340.2946
299213	2339.8046	299213	2340.2946
308564	2339.6446	308564	2340.1546
317915 327266	2339.5646 2339.4846	317915 327266	2340.0946 2340.0246
336622	2339.4046	336622	2339.9646
345973	2339.3246	345973	2339.8946
355324 364669	2339.2446 2339.1746	355324 364669	2339.8246 2339.7646
374020	2339.0946	374020	2339.7046
383371	2339.0146	383371	2339.6346
392722 402073	2338.9346 2338.8646	392722 402073	2339.5746 2339.5046
411424	2338.7846	411424	2339.4446
420774	2338.7046	420774	2339.3846
430125 439476	2338.6346 2338.5546	430125 439476	2339.3146 2339.2546
448827	2338.4846	448827	2339.1946
458173	2338.4046	458173	2339.1246
467524 476874	2338.3246 2338.2546	467524 476874	2339.0646 2339.0046
486225	2338.1746	486225	2338.9446
495576	2338.1046	495576	2338.8746
504927 514278	2338.0246 2337.9546	504927 514278	2338.8146 2338.7546
523629	2337.8846	523629	2338.6946
532969 542315	2337.8046 2337.7346	532969 542315	2338.6346 2338.5746
551660	2337.6546	551660	2338.5146
561006	2337.5846	561006	2338.4446
570352 579697	2337.5146 2337.4346	570352 579697	2338.3846 2338.3246
589043	2337.3646	589043	2338.2646
598441	2337.2946	598441	2338.2046
607787 617132	2337.2146 2337.1446	607787 617132	2338.1446 2338.0846
626478	2337.0746	626478	2338.0246
635824 645169	2336.9946	635824	2337.9646
654515	2336.9246 2336.8546	645169 654515	2337.9046 2337.8446
663860	2336.7746	663860	2337.7846
673212 682559	2311.9244 2299.5043	673212 682559	2312.8544 2300.4043
691904	2298.1943	691904	2299.1043
701315	2262.4441	701315	2263.2141
710660 720008	2262.3641 2250.034	710660 720008	2263.1541 2250.794
729353	2248.734	729353	2249.504
738699	2248.664	738699	2249.434
748046 757391	2237.564 2237.484	748046 757391	2238.314 2238.254
766737	2232.5139	766737	2233.2739
776083	2225.1039 2225.0339	776083	2225.8539
785429 794775	2225.0339	785429 794775	2225.7939 2225.7239
804173	2224.8839	804173	2225.6639
813520 822865	2212.5838	813520 822865	2213.3538
822865 832211	2212.5138 2212.4438	822865 832211	2213.2838 2213.2238
841556	2212.3638	841556	2213.1638
850903 860249	2222.0739 2222.0039	850903 860249	2222.9139
860249 869596	2236.6539	869596	2222.8539 2237.544
878955	2199.8437	878955	2200.6637
888313 897675	2163.3335 2122.8132	888313 897675	2164.0835 2123.4732
907022	2122.8132	907022	2123.4732
916420	2118.8232	916420	2119.5132
925767 935112	2110.0332 2114.8532	925767 935112	2110.7132 2115.5532
935112	2114.8532	935112	2115.5532

APPENDIX VIII Simulation results of various pipeline roughness value vs pressure drop

Distance (miles)	Pressure 🔻	Distance2 (miles)	Pressure3 🕶	Distance4 (miles)	Pressure! •
Roughness (inch)	(psi) 0.000005	Roughness (inch)	(psi) 0.00026	Roughness (inch)	(psi) 0.00046
0	2325.0145	0	2325.0145	0	2325.0145
О	2325.0145	0	2325.0145	О	2325.0145
1.7709 3.5428	2320.3045 2332.9845	1.7709 3.5428	2319.6145	1.7709 3.5428	2319.2645
5.3137	2328.3345	5.3137	2326,2645	5.3137	2325.2045
7.0847	2323.7045	7.0847	2320.9545	7.0847	2319.5445
8.8556	2319.0945	8.8556	2315.6544	8.8556	2313.9044
10.6261	2314.4944	10.6261	2310.3844	10.6261	2308.2844
12.3971 14.1681	2309.9144	12.3971 14.1681	2305.1244	12.3971 14.1681	2302.6744
15.9391	2300.8143	15.9391	2294.6643	15.9391	2291.5143
17.7101	2296.2743	17.7101	2289.4543	17.7101	2285.9643
19.4811	2291.7643	19.4811	2284.2642	19.4811	2280.4242
21.2511	2287.2643	21.2511	2279.0842	21.2511	2274.9042
23.0222	2282.7742	23.0222	2273.9242	23.0222	2269.3842
26.5642	2273.8342	26.5642	2263.6241	26.5642	2258.4041
28.3352	2269.3742	28.3352	2258.5041	28.3352	2252.9241
30.1061	2264.9441	30.1061	2253.3841	30.1061	2247.474
31.8771	2260.5141	31.8771	2248.294	31.8771	2242.024
33.6481	2256.1041	33.6481	2243.204	33.6481	2236.6039
35.4182 37.1892	2251.714 2247.324	35.4182 37.1892	2238.144	35.4182 37.1892	2231.1939 2225.7839
38.9602	2242.954	38.9602	2228.0439	38.9602	2220.4038
40.7311	2238.594	40.7311	2223.0139	40.7311	2215.0238
42.5021	2234.2439	42.5021	2217.9938	42.5021	2209.6638
44.2731	2229.9039	44.2731	2212.9838	44.2731	2204.3037
46.0441 47.8152	2225.5739 2221.2639	46.0441 47.8152	2207.9838 2203.0037	46.0441 47.8152	2198.9637 2193.6237
49.5852	2216.9538	49.5852	2198.0237	49.5852	2188.3036
51.3561	2212.6538	51.3561	2193.0537	51.3561	2182.9936
53.1271	2208.3638	53.1271	2188.0936	53.1271	2177.6836
54.8981	2204.0837	54.8981	2183.1436	54.8981	2172.3835
56.6691 58.4402	2199.8137 2195.5437	56.6691 58.4402	2178.1936 2173.2636	56.6691 58.4402	2167.0935 2161.8135
60.2112	2191.2937	60.2112	2168.3335	60.2112	2156.5334
61.9822	2187.0336	61.9822	2163.4135	61.9822	2151.2634
63.7542	2182.7936	63.7542	2158.4935	63.7542	2146.0034
65.5252	2178.5636	65.5252	2153.5934	65.5252	2140.7534
67.2962 69.0661	2174.3436	67.2962 69.0661	2148.6934	67.2962 69.0661	2135.5033
70.8371	2165.9235	70.8371	2138.9333	70.8371	2125.0533
72.6081	2161.7235	72.6081	2134.0633	72.6081	2119.8332
74.3792	2157.5335	74.3792	2129.2033	74.3792	2114.6232
76.1502	2153.3534	76.1502	2124.3432	76.1502	2109.4132
77.9212	2149.1734	77.9212	2119.4932	77.9212	2104.2131
79.692 81.4631	2145.0034 2140.8434	79.692 81.4631	2114.6532 2109.8232	79.692 81.4631	2099.0231 2093.8431
83.2341	2136.6833	83.2341	2104.9931	83.2341	2088.653
85.0051	2132.5333	85.0051	2100.1631	85.0051	2083.483
86.7752 88.5462	2128.3933	86.7752 88.5462	2095.3431	86.7752 88.5462	2078.313
90.317	2120.1232	90.317	2085.713	90.317	2067.9729
92.0881	2115.9932	92.0881	2080.913	92.0881	2062.8129
93.8591	2111.8632	93.8591	2076.1029	93.8591	2057.6528
95.6301 97.4011	2107.7431 2103.6231	95.6301 97.4011	2071.3029 2066.5029	95.6301 97.4011	2052.4928
99.1722	2099.5131	99.1722	2061.7129	99.1722	2042.1827
100.9411	2095.4131	100.9411	2056.9228	100.9411	2037.0427
102.7112	2091.303	102.7112	2052.1328	102.7112	2031.8927
104.4811 106.2511	2087.213 2083.113	104.4811	2047.3528	104.4811 106.2511	2026.7526 2021.6026
108.0212	2079.013	108.0212	2037.7827	108.0212	2016.4626
109.7911	2074.9229	109.7911	2033.0027	109.7911	2011.3125
111.5612	2070.8329	111.5612	2028.2226	111.5612	2006.1725
113.3411 115.1112	2066.7229 2062.6429	113.3411 115.1112	2023.4126 2018.6326	113.3411 115.1112	2000.9925 1995.8524
116.8811	2058.5628	116.8811	2013.8526	116.8811	1990.7124
118.6511	2054.4828	118.6511	2009.0825	118.6511	1985.5724
120.4212 122.1911	2050.4028 2046.3328	120.4212 122.1911	2004.3125 1999.5325	120.4212 122.1911	1980.4224
123.9612	2046.3328	123.9612	1994.7624	122.1911	1975.2823 1970.1423
125.7311	2038.1927	125.7311	1989.9924	125.7311	1965.0023
127.5023	2014.2926	127.5023	1965.8123	127.5023	1940.6721
129.2725 131.0424	2000.3325 1995.2524	129.2725 131.0424	1951.3522 1945.5721	129.2725 131.0424	1925.942 1919.802
131.0424	1962.6622	131.0424	1912.8919	131.0424	1887.0718
134.5947	1958.5322	134.5947	1908.0419	134.5947	1881.8317
136.3652	1944.6421	136.3652	1893.6518	136.3652	1867.1716
138.135 139.9051	1939.5321 1935.3921	138.135 139.9051	1887.8218 1882.9417	138.135 139.9051	1860.9616 1855.6916
141.6754	1935.3921	141.6754	1869.5217	139.9051	1855.6916
143.4453	1918.352	143.4453	1864.6316	143.4453	1836.7015
145.2153	1910.3119	145.2153	1855.9416	145.2153	1827.6714
146.9854 148.7555	1900.3519 1896.1818	146.9854 148.7555	1845.3815 1840.4515	146.9854 148.7555	1816.7813
150.5256	1896.1818	150.5256	1835.5214	150.5256	1811.4613
152.3055	1887.8218	152.3055	1830.5714	152.3055	1800.7612
154.0758	1874.0217	154.0758	1816.2613	154.0758	1786.1911
155.8456 157.6157	1869.8317 1865.6516	155.8456 157.6157	1811.3013 1806.3413	155.8456 157.6157	1780.8211 1775.4411
159.3856	1861.4616	159.3856	1806.3413	157.6157	1770.061
161.1559	1864.9516	161.1559	1803.8612	161.1559	1772.0111
162.9259	1860.7616	162.9259	1798.8912	162.9259	1766.621
164.6962	1868.1217	164.6962	1805.1013	164.6962	1772.2311
166.4687 168.2411	1835.1814 1802.5012	166.4687 168.2411	1772.2611 1739.6708	166.4687 168.2411	1739.4408 1706.8906
170.0142	1766.711	170.0142	1704.0606	170.0142	1671.4004
171.7845	1755.6209	171.7845	1692.3606	171.7845	1659.3703
173.5644	1755.0909	173.5644	1690.8605	173.5644	1657.3503
175.3347 177.1045	1744.0009 1743.4609	175.3347 177.1045	1679.1705 1677.6505	175.3347 177.1045	1645.3303 1643.3002
177.1045	1743.4609	177.1045	1677.6505	177.1045	1643.3002

 $\label{eq:APPENDIX} \mbox{ APPENDIX IX}$ APPENDIX IX Simulation results of various pipeline roughness value vs pressure drop

Distance6 🔻	Pressure7 🔻	Distance8 🔻	Pressure! -	Distance10 🔻	Pressure11 -
(miles)	(psi)	(miles)	(psi)	(miles)	(psi)
Roughness (inch) 0	0.00066 2325.0145	Roughness (inch) 0	0.00086 2325.0145	Roughness (inch)	0.001 2325.0145
o	2325.0145	0	2325.0145	o	2325.0145
1.7709	2318.9845	1.7709	2318.7545	1.7709	2318.6145
3.5428	2330.3345	3.5428	2329.8645	3.5428	2329.5745
5.3137 7.0847	2324.3745 2318.4345	5.3137 7.0847	2323.6745 2317.5045	5.3137 7.0847	2323.2445
8.8556	2312.5144	8.8556	2311.3544	8.8556	2310.6444
10.6261	2306.6244	10.6261	2305.2344	10.6261	2304.3744
12.3971	2300.7443	12.3971	2299.1243	12.3971	2298.1143
14.1681 15.9391	2294.8743 2289.0343	14.1681 15.9391	2293.0243 2286.9543	14.1681 15.9391	2291.8843 2285.6643
17.7101	2283.2042	17.7101	2280.8942	17.7101	2279.4642
19.4811	2277.3842	19.4811	2274.8442	19.4811	2273.2742
21.2511 23.0222	2271.5842	21.2511 23.0222	2268.8241 2262.8041	21.2511 23.0222	2267.1041
24.7932	2260.0241	24.7932	2256.7941	24.7932	2254.7941
26.5642	2254.2641	26.5642	2250.804	26.5642	2248.664
28.3352	2248.514	28.3352	2244.824	28.3352	2242.544
30.1061 31.8771	2242.784 2237.064	30.1061 31.8771	2238.864	30.1061 31.8771	2236.4439 2230.3539
33.6481	2231.3639	33.6481	2226.9839	33.6481	2224.2739
35.4182	2225.6839	35.4182	2221.0739	35.4182	2218.2138
37.1892	2220.0038	37.1892	2215.1638	37.1892	2212.1738
38.9602 40.7311	2214.3438 2208.6938	38.9602 40.7311	2209.2738 2203.3937	38.9602 40.7311	2206.1338 2200.1137
42.5021	2203.0537	42.5021	2197.5237	42.5021	2194.0937
44.2731	2197.4237	44.2731	2191.6637	44.2731	2188.0936
46.0441	2191.8037	46.0441	2185.8136	46.0441	2182.1036
47.8152 49.5852	2186.2036 2180.6036	47.8152 49.5852	2179.9736 2174.1536	47.8152 49.5852	2176.1236 2170.1535
51.3561	2175.0136	51.3561	2168.3235	51.3561	2164.1835
53.1271	2169.4335	53.1271	2162.5135	53.1271	2158.2235
54.8981	2163.8635 2158.2935	54.8981 56.6691	2156.7035 2150.9034	54.8981	2152.2734 2146.3334
56.6691 58.4402	2158.2935 2152.7334	56.6691 58.4402	2150.9034	56.6691 58.4402	2146.3334
60.2112	2147.1734	60.2112	2139.3233	60.2112	2134.4633
61.9822	2141.6334	61.9822	2133.5433	61.9822	2128.5333
63.7542 65.5252	2136.0933 2130.5633	63.7542 65.5252	2127.7733 2122.0032	63.7542 65.5252	2122.6132 2116.7032
67.2962	2125.0433	67.2962	2116.2532	67.2962	2110.7032
69.0661	2119.5332	69.0661	2110.5132	69.0661	2104.9231
70.8371	2114.0332	70.8371	2104.7731	70.8371	2099.0331
72.6081 74.3792	2108.5332 2103.0431	72.6081 74.3792	2099.0431 2093.3131	72.6081 74.3792	2093.1531 2087.283
76.1502	2097.5631	76.1502	2087.593	76.1502	2081.423
77.9212	2092.083	77.9212	2081.883	77.9212	2075.5529
79.692	2086.613	79.692	2076.1729	79.692	2069.7029
81.4631 83.2341	2081.143	81.4631 83.2341	2070.4729	81.4631 83.2341	2063.8529
85.0051	2070.2229	85.0051	2059.0728	85.0051	2052.1528
86.7752	2064.7729	86.7752	2053.3828	86.7752	2046.3128
88.5462 90.317	2059.3128 2053.8728	88.5462 90.317	2047.6928 2042.0027	88.5462 90.317	2040.4727 2034.6327
92.0881	2048.4228	92.0881	2036.3127	92.0881	2028.8027
93.8591	2042.9727	93.8591	2030.6327	93.8591	2022.9626
95.6301 97.4011	2037.5327 2032.0927	95.6301 97.4011	2024.9426	95.6301 97.4011	2017.1326 2011.2925
99.1722	2026.6526	99.1722	2013.5826	99.1722	2005.4625
100.9411	2021.2226	100.9411	2007.9025	100.9411	1999.6325
102.7112 104.4811	2015.7826 2010.3525	102.7112 104.4811	2002.2225 1996.5425	102.7112 104.4811	1993.8024 1987.9724
106.2511	2004.9225	106.2511	1990.8624	106.2511	1982.1324
108.0212	1999.4825	108.0212	1985.1824	108.0212	1976.3023
109.7911 111.5612	1994.0424 1988.6124	109.7911 111.5612	1979.5023 1973.8123	109.7911 111.5612	1970.4623 1964.6223
113.3411	1983.1424	113.3411	1968.0923	113.3411	1958.7422
115.1112	1977.7023	115.1112	1962.4122	115.1112	1952.9022
116.8811 118.6511	1972.2723 1966.8323	116.8811 118.6511	1956.7222 1951.0422	116.8811 118.6511	1947.0621 1941.2221
120.4212	1961.3922	120.4212	1945.3521	120.4212	1935.3721
122.1911	1955.9622	122.1911	1939.6621	122.1911	1929.522
123.9612 125.7311	1950.5222 1945.0821	123.9612 125.7311	1933.9721 1928.272	123.9612 125.7311	1923.672 1917.822
127.5023	1920.622	127.5023	1903.7019	127.5023	1893.1818
129.2725	1905.6819	129.2725	1888.5818	129.2725 131.0424	1877.9417
131.0424 132.8248	1899.2418 1866.4616	131.0424 132.8248	1881.8917 1849.0715	131.0424	1871.0917 1838.2515
134.5947	1860.9116	134.5947	1843.2615	134.5947	1832.2714
136.3652	1846.0315	136.3652	1828.1914	136.3652	1817.0913
138.135 139.9051	1839.5315 1833.9414	138.135 139.9051	1821.4214 1815.5713	138.135 139.9051	1810.1613 1804.1313
141.6754	1820.0114	141.6754	1801.4512	141.6754	1789.8912
143.4453	1814.4013 1805.0913	143.4453	1795.5612	143.4453	1783.8311
145.2153 146.9854	1805.0913	145.2153 146.9854	1786.0111 1774.6411	145.2153 146.9854	1774.1311 1762.621
148.7555	1788.2912	148.7555	1768.711	148.7555	1756.511
150.5256	1782.6311	150.5256	1762.771	150.5256	1750.4009
152.3055 154.0758	1776.9411 1762.141	152.3055 154.0758	1756.791 1741.8109	152.3055 154.0758	1744.2409 1729.1308
155.8456	1756.441	155.8456	1735.8208	155.8456	1722.9707
157.6157	1750.7309	157.6157	1729.8208	157.6157	1716.7807
159.3856 161.1559	1745.0109 1746.5209	159.3856 161.1559	1723.8108 1724.9408	159.3856 161.1559	1710.5907 1711.4907
162.9259	1740.7909	162.9259	1718.9207	162.9259	1705.2806
164.6962	1745.9009	164.6962	1723.6107	164.6962	1709.7107
166.4687 168.2411	1713.1507 1680.6405	166.4687 168.2411	1690.8805 1658.4103	166.4687 168.2411	1677.0005 1644.5303
170.0142	1645.2303	170.0142	1623.0601	170.0142	1609.23
171.7845	1632.9402	171.7845	1610.53	171.7845	1596.55
173.5644 175.3347	1630.5002 1618.2001	173.5644 175.3347	1607.73 1595.1999	173.5644 175.3347	1593.5199 1580.8399
177.1045	1615.7401	177.1045	1592.3799	177.1045	1577.7798
177.1045	1615.7401	177.1045	1592.3799	177.1045	1577.7798

APPENDIX X Simulation results of compressor outlet temp vs pressure drop

Distance (miles)	Pressure (psi)	Distance (miles)	Pressure (psi)	Distance (miles)	Pressure (psi)	Distance (miles)	Pressure (psi)
Temperature (F)	180	Temperature (F)	190	Temperature (F)	200	Temperature (F)	210
0	2325.0145	0	2325.0145	0	2325.0145	0	2325.0145
0	2325.0145	0	2325.0145	0	2325.0145	0	2325.0145
1.7709 3.5428	2319.1045 2331.9845	1.7709 3.5428	2318.9545 2331.2245	1.7709 3.5428	2318.8045 2330.4845	1.7709 3.5428	2318.6445 2329.7245
5.3137	2326.1345	5.3137	2325.2245	5.3137	2324.3345	5.3137	2323.4245
7.0847	2320.2945	7.0847	2319.2345	7.0847	2318.2045	7.0847	2317.1445
8.8556	2314.4744	8.8556	2313.2644	8.8556	2312.0944	8.8556	2310.8844
10.6261	2308.6644	10.6261	2307.3044	10.6261	2305.9944	10.6261	2304.6444
12.3971	2302.8644	12.3971	2301.3544	12.3971	2299.9043	12.3971	2298.4143
14.1681 15.9391	2297.0843 2291.3143	14.1681 15.9391	2295.4243 2289.5043	14.1681 15.9391	2293.8343 2287.7843	14.1681 15.9391	2292.2143 2286.0243
17.7101	2285.5543	17.7101	2283.6042	17.7101	2281.7342	17.7101	2279.8442
19.4811	2279.8042	19.4811	2277.7142	19.4811	2275.7042	19.4811	2273.6842
21.2511	2274.0742	21.2511	2271.8442	21.2511	2269.6942	21.2511	2267.5341
23.0222	2268.3441	23.0222	2265.9841	23.0222	2263.6941	23.0222	2261.4041
24.7932	2262.6241	24.7932	2260.1341	24.7932	2257.7041	24.7932	2255.2841
26.5642	2256.9141	26.5642	2254.2941	26.5642	2251.734	26.5642	2249.174
28.3352	2251.204	28.3352	2248.464	28.3352	2245.774	28.3352	2243.074
30.1061 31.8771	2245.514 2239.824	30.1061 31.8771	2242.644 2236.844	30.1061 31.8771	2239.824 2233.8939	30.1061 31.8771	2237.004 2230.9339
33.6481	2234.1439	33.6481	2230.844	33.6481	2227.9739	33.6481	2230.933
35,4182	2228.4739	35.4182	2225,2539	35.4182	2222,0639	35,4182	2218.8538
37.1892	2222.8139	37.1892	2219.4638	37.1892	2216.1638	37.1892	2212.8338
38.9602	2217.1538	38.9602	2213.6938	38.9602	2210.2738	38.9602	2206.8238
40.7311	2211.5038	40.7311	2207.9238	40.7311	2204.3937	40.7311	2200.8237
42.5021	2205.8738	42.5021	2202.1637	42.5021	2198.5137	42.5021	2194.8337
44.2731	2200.2437	44.2731	2196.4037	44.2731	2192.6537	44.2731	2188.8537
46.0441 47.8152	2194.6237	46.0441	2190.6537	46.0441 47.8152	2186.7936	46.0441	2182.8836 2176.9236
47.8152 49.5852	2189.0037 2183.4036	47.8152 49.5852	2184.9236 2179.1936	47.8152 49.5852	2180.9436 2175.1036	47.8152 49.5852	2176.9236
51.3561	2177.8036	51.3561	2173.4736	51.3561	2169.2635	51.3561	2165.0335
53.1271	2172.2035	53.1271	2167.7635	53.1271	2163.4335	53.1271	2159.0935
54.8981	2166.6135	54.8981	2162.0635	54.8981	2157.6035	54.8981	2153.1634
56.6691	2161.0335	56.6691	2156.3634	56.6691	2151.7934	56.6691	2147.2334
58.4402	2155.4534	58.4402	2150.6734	58.4402	2145.9934	58.4402	2141.3234
60.2112	2149.8734	60.2112	2144.9834	60.2112	2140.1933	60.2112	2135.4033
61.9822	2144.3034	61.9822	2139.3033	61.9822	2134.4033	61.9822	2129.5033
63.7542 65.5252	2138.7333 2133.1633	63.7542 65.5252	2133.6333 2127.9633	63.7542 65.5252	2128.6233 2122.8432	63.7542 65.5252	2123.6132 2117.7232
67.2962	2127.6033	67.2962	2122.2932	67.2962	2117.0732	67.2962	2111.8432
69.0661	2122.0432	69.0661	2116.6332	69.0661	2111.3132	69.0661	2105.9831
70.8371	2116.4832	70.8371	2110.9832	70.8371	2105.5531	70.8371	2100.1131
72.6081	2110.9332	72.6081	2105.3231	72.6081	2099.7931	72.6081	2094.2631
74.3792	2105.3731	74.3792	2099.6731	74.3792	2094.0431	74.3792	2088.403
76.1502	2099.8131	76.1502	2094.0231	76.1502	2088.303	76.1502	2082.563
77.9212	2094.2631	77.9212	2088.373	77.9212	2082.553	77.9212	2076.723
79.692 81.4631	2088.713 2083.153	79.692 81.4631	2082.733 2077.083	79.692 81.4631	2076.813 2071.0729	79.692 81.4631	2070.8829 2065.0529
83.2341	2077.603	83.2341	2071.4429	83.2341	2065.3429	83.2341	2059.2228
85.0051	2072.0429	85.0051	2065.7929	85.0051	2059.6028	85.0051	2053.3928
86.7752	2066.4929	86.7752	2060.1528	86.7752	2053.8728	86.7752	2047.5728
88.5462	2060.9329	88.5462	2054.5128	88.5462	2048.1428	88.5462	2041.7527
90.317	2055.3828	90.317	2048.8628	90.317	2042.4127	90.317	2035.9327
92.0881 93.8591	2049.8228 2044.2727	92.0881 93.8591	2043.2227 2037.5727	92.0881 93.8591	2036.6827 2030.9527	92.0881 93.8591	2030.1127
95.6301	2038.7127	95.6301	2031.9227	95.6301	2025.2226	95.6301	2018.4726
97.4011	2033.1627	97.4011	2026.2726	97.4011	2019.4826	97.4011	2012.6626
99.1722	2027.6026	99.1722	2020.6326	99.1722	2013.7526	99.1722	2006.8425
100.9411	2022.0526	100.9411	2014.9926	100.9411	2008.0225	100.9411	2001.0325
102.7112	2016.4926	102.7112	2009.3425	102.7112	2002.2925	102.7112	1995.2124
104.4811	2010.9425	104.4811	2003.7025	104.4811	1996.5525	104.4811	1989.4024
106.2511	2005.3825	106.2511	1998.0525	106.2511	1990.8224	106.2511	1983.5824
108.0212 109.7911	1999.8125 1994.2524	108.0212 109.7911	1992.4024 1986.7524	108.0212 109.7911	1985.0824 1979.3523	108.0212 109.7911	1977.7623 1971.9323
111.5612	1988.6824	111.5612	1981.1024	111.5612	1973.6123	111.5612	1966.1123
113.3411	1983.0824	113.3411	1975.4223	113.3411	1967.8423	113.3411	1960.2522
115.1112	1977.5123	115.1112	1969.7623	115.1112	1962.1022	115.1112	1954.4322
116.8811	1971.9323	116.8811	1964.1022	116.8811	1956.3622	116.8811	1948.6122
118.6511	1966.3523	118.6511	1958.4422	118.6511	1950.6222	118.6511	1942.7821
120.4212	1960.7622	120.4212	1952.7722	120.4212	1944.8721	120.4212	1936.9521
122.1911 123.9612	1955.1722 1949.5822	122.1911 123.9612	1947.1021 1941.4321	122.1911 123.9612	1939.1221 1933.3721	122.1911 123.9612	1931.122 1925.282
125.7311	1943.9821		1935.7521		1933.3721		1925.282
127.5023	1918.742		1910.7119		1902.7519		1894.7718
129.2725	1903.3419		1895.3618	129.2725	1887.4618		1879.5217
131.0424	1896.7018	131.0424	1888.6518	131.0424	1880.6917	131.0424	1872.6917
132.8248	1862.9316		1855.1816	132.8248	1847.5115	132.8248	1839.7915
134.5947	1857.2016		1849.3715		1841.6215	134.5947	1833.8214
136.3652 138.135	1841.8615 1835.1414	136.3652 138.135	1834.0914 1827.3014	136.3652 138.135	1826.3814 1819.5313		1818.6313 1811.7213
138.135	1835.1414 1829.3614	138.135	1827.3014 1821.4514	138.135	1819.5313 1813.6013	138.135	1811.7213
141.6754	1815.0113	141.6754	1807.1313		1799.3112		1791.4512
143.4453	1809.1913		1801.2412	143.4453	1793.3512		1785.4111
145.2153	1799.5812	145.2153	1791.6012	145.2153	1783.6811	145.2153	1775.7211
146.9854	1788.0812	146.9854	1780.1011		1772.1811	146.9854	1764.211
148.7555	1782.2111		1774.1611		1766.161	148.7555	1758.121
150.5256	1776.3311	150.5256	1768.211	150.5256	1760.141	150.5256	1752.0209
152.3055	1770.411	152.3055	1762.211	152.3055	1754.0609	152.3055	1745.8709
154.0758 155.8456	1755.1809 1749.2509	154.0758 155.8456	1747.0209 1741.0109	154.0758 155.8456	1738.9208 1732.8408	154.0758 155.8456	1730.7608 1724.6108
157.6157	1743.3009	157.6157	1734.9908		1732.8408		1718.4407
159.3856	1737.3308		1728.9608		1720.7408		1712.2607
161.1559	1738.7408		1730.2008		1721.7207		1713.1907
162.9259	1732.7608	162.9259	1724.1508	162.9259	1715.6007	162.9259	1707.0006
164.6962	1737.8208		1729.0208	164.6962	1720.2707	164.6962	1711.4707
166.4687	1704.3306	166.4687	1695.7706	166.4687	1687.2705	166.4687	1678.7105
168.2411	1671.0504	168.2411	1662.7804	168.2411	1654.5303	168.2411	1646.2003
170.0142	1634.7802	170.0142	1626.8201	170.0142	1618.8701	170.0142	1610.84
171.7845	1622.1001	171.7845	1614.1401		1606.2	171.7845	1598.16
173.5644 175.3347	1619.4801 1606.8		1611.39 1598.72		1603.32 1590.6499	173.5644 175.3347	1595.1599 1582.4799
1,0.0047	1604.14		1595.93		1587.7399	177.1045	1579.4399
177.1045							

APPENDIX XI APPENDIX XI Simulation results of compressor outlet temp vs pressure drop

Distance (miles)	Pressure (psi)	Distance (miles)	Pressure (psi)	Distance (miles)	Pressure (psi)	Distance (miles)	Pressure (psi)
emperature (F)		Temperature (F)		Temperature (F)		Temperature (F)	(621)
0	2325.0145	O	2325.0145	O	2325.0145	0	2325.0
0	2325.0145	0	2325.0145	0	2325.0145	0	2325.0
1.7709	2318.4945	1.7709	2318.3545	1.7709	2318.1945	1.7709	2318.0
3.5428	2329.0445	3.5428	2328.3845	3.5428	2327.7045	3.5428	2327.0
5.3137	2322.5945	5.3137	2321.7945	5.3137	2320.9745	5.3137	2320.2
7.0847 8.8556	2316.1644 2309.7544	7.0847 8.8556	2315.2244 2308.6744	7.0847 8.8556	2314.2544 2307.5744	7.0847 8.8556	2313.3 2306.5
10.6261	2303.3644	10.6261	2302.1444	10.6261	2300.9043	10.6261	2299.7
12.3971	2296.9943	12.3971	2295.6343	12.3971	2294.2643	12.3971	2292.9
14.1681	2290.6443	14.1681	2289.1443	14.1681	2287.6343	14.1681	2286.1
15.9391	2284.3142	15.9391	2282.6642	15.9391	2281.0342	15.9391	2279.4
17.7101	2277.9942	17.7101	2276.2142	17.7101	2274.4442	17.7101	2272.7
19.4811	2271.7042	19.4811	2269.7842	19.4811	2267.8741	19.4811	2266.0
21.2511	2265.4241	21.2511	2263.3741	21.2511	2261.3241	21.2511	2259.3
23.0222	2259.1641	23.0222	2256.9741	23.0222	2254.7941	23.0222	2252.
24.7932	2252.9241	24.7932 26.5642	2250.604	24.7932 26.5642	2248.284	24.7932	2246
26.5642 28.3352	2246.684 2240.464	28.3352	2244.244 2237.904	28.3352	2241.794 2235.3239	26.5642 28.3352	2239 2232.8
30.1061	2234.2639	30.1061	2231.5739	30.1061	2228.8739	30.1061	2226.2
31.8771	2228.0739	31.8771	2225.2639	31.8771	2222.4339	31.8771	2219.7
33.6481	2221.8939	33.6481	2218.9638	33.6481	2216.0238	33.6481	2213.1
35.4182	2215.7238	35.4182	2212.6838	35.4182	2209.6238	35.4182	2206.6
37.1892	2209.5738	37.1892	2206.4138	37.1892	2203.2337	37.1892	2200.1
38.9602	2203.4437	38.9602	2200.1537	38.9602	2196.8537	38.9602	2193.0
40.7311	2197.3237	40.7311	2193.9037	40.7311	2190.5037	40.7311	2187.1
42.5021	2191.2137	42.5021	2187.6736	42.5021	2184.1536	42.5021	2180.7
44.2731	2185.1136	44.2731	2181.4536	44.2731	2177.8136	44.2731	2174.2
46.0441	2179.0336	46.0441	2175.2536	46.0441	2171.4935	46.0441	2167.8
47.8152	2172.9636	47.8152	2169.0635	47.8152	2165.1835	47.8152	2161.4
49.5852	2166.9035	49.5852	2162.8935	49.5852	2158.8935	49.5852	2155.
51.3561	2160.8435	51.3561	2156.7335	51.3561	2152.6134	51.3561	2148.
53.1271	2154.8034	53.1271	2150.5734	53.1271	2146.3534	53.1271	2142.
54.8981 56.6691	2148.7734 2142.7434	54.8981 56.6691	2144.4334 2138.3033	54.8981 56.6691	2140.0933 2133.8533	54.8981 56.6691	2135. 2129.
58.4402	2136.7233	58.4402	2132.1833	58.4402	2127.6233	58.4402	2123.
60.2112	2130.7233	60.2112	2126.0633	60.2112	2121.4032	60.2112	2116.
61.9822	2124.7033	61.9822	2119.9632	61.9822	2115.1932	61.9822	2110.
63.7542	2118.7032	63.7542	2113.8532	63.7542	2108.9932	63.7542	2104.
65.5252	2112.7032	65.5252	2107.7631	65.5252	2102.8031	65.5252	2097.
67.2962	2106.7131	67.2962	2101.6831	67.2962	2096.6231	67.2962	2091
69.0661	2100.7431	69.0661	2095.6031	69.0661	2090.443	69.0661	2085
70.8371	2094.7731	70.8371	2089.533	70.8371	2084.283	70.8371	2079
72.6081	2088.813	72.6081	2083.463	72.6081	2078.113	72.6081	2072.
74.3792	2082.853	74.3792	2077.403	74.3792	2071.9629	74.3792	2066.
76.1502	2076.903	76.1502	2071.3529	76.1502	2065.8029	76.1502	2060.
77.9212	2070.9629	77.9212	2065.3029	77.9212	2059.6628	77.9212	2054.
79.692	2065.0329	79.692	2059.2728	79.692	2053.5228	79.692	2047.
81.4631 83.2341	2059.1028 2053.1728	81.4631 83.2341	2053.2428 2047.2128	81.4631 83.2341	2047.3928 2041.2727	81.4631 83.2341	2041. 2035.
85.0051	2047.2528	85.0051	2041.2027	85.0051	2035.1527	85.0051	2029.
86.7752	2041.3427	86.7752	2035.1927	86.7752	2029.0427	86.7752	2023.
88.5462	2035.4227	88.5462	2029.1827	88.5462	2022.9426	88.5462	2016.
90.317	2029.5127	90.317	2023.1826	90.317	2016.8426	90.317	2010.
92.0881	2023.6026	92.0881	2017.1826	92.0881	2010.7525	92.0881	2004.
93.8591	2017.7026	93.8591	2011.1925	93.8591	2004.6725	93.8591	1998.
95.6301	2011.7925	95.6301	2005.1925	95.6301	1998.5825	95.6301	1992.
97.4011	2005.8925	97.4011	1999.2025	97.4011	1992.5024	97.4011	1985.
99.1722	1999.9925	99.1722	1993.2124	99.1722	1986.4324	99.1722	1979.
100.9411	1994.0924	100.9411	1987.2324	100.9411	1980.3624	100.9411	1973.
102.7112 104.4811	1988.2024 1982.3024	102.7112 104.4811	1981.2524 1975.2723	102.7112 104.4811	1974.2923 1968.2323	102.7112 104.4811	1967. 1961.
104.4811	1982.3024	104.4811	1969.2923	104.4811	1968.2323	104.4811	1951.
108.0212	1970.5023	108.0212	1963.3122	108.0212	1956.1022	108.0212	1949.
109.7911	1964,6023	109.7911	1957.3322	109.7911	1950.1022	109.7911	1942.
111.5612	1958.6922	111.5612	1951.3422	111.5612	1943.9721	111.5612	1936.
113.3411	1952.7522	113.3411	1945.3221	113.3411	1937.8721	113.3411	1930
115.1112	1946.8421	115.1112	1939.3421	115.1112	1931.802	115.1112	1924
116.8811	1940.9321	116.8811	1933.3521	116.8811	1925.742	116.8811	1918
118.6511	1935.0221	118.6511	1927.362	118.6511	1919.672	118.6511	1912.
120.4212	1929.112	120.4212	1921.362	120.4212	1913.6019	120.4212	1905.
122.1911	1923.202	122.1911	1915.3719	122.1911	1907.5219	122.1911	1899.
123.9612	1917.282	123.9612	1909.3719	123.9612	1901.4519	123.9612	1893.
125.7311	1911.3619	125.7311	1903.3719	125.7311	1895.3718	125.7311	1887.
127.5023	1886.8618	127.5023	1879.0417	127.5023	1871.2117	127.5023	1863.
129.2725	1871.6617	129.2725	1863.8816	129.2725	1856.0916	129.2725	1848.
131.0424 132.8248	1864.7616 1832.1414	131.0424 132.8248	1856.9116 1824.5614	131.0424 132.8248	1849.0515 1816.9613	131.0424 132.8248	1841. 1809.
134.5947	1826.0914	134.5947	1818.4413	134.5947	1810.7613	134.5947	1803.
136.3652	1810.9413	136.3652	1803.3312	136.3652	1795.6812	136.3652	1788.
138.135	1803.9613	138.135	1796.2812	138.135	1788.5612	138.135	1780.
139.9051	1797.8712	139.9051	1790.1112	139.9051	1782.3211	139.9051	1774.
141.6754	1783.6511	141.6754	1775.9111	141.6754	1768.141	141.6754	1760
143.4453	1777.5311	143.4453	1769.721	143.4453	1761.871	143.4453	1754.
145.2153	1767.811	145.2153	1759.961	145.2153	1752.0809	145.2153	1744.
146.9854	1756.291	146.9854	1748.4309	146.9854	1740.5409	146.9854	1732.
148.7555	1750.1209	148.7555	1742.1909	148.7555	1734.2208	148.7555	1726.
150.5256	1743.9509	150.5256	1735.9408	150.5256	1727.9008	150.5256	1719.
152.3055	1737.7208	152.3055	1729.6408	152.3055	1721.5207	152.3055	1713.
154.0758	1722.6507	154.0758	1714.6007	154.0758	1706.5106	154.0758	1698.
155.8456	1716.4207	155.8456	1708.2907	155.8456	1700.1306	155.8456	1692.
157.6157	1710.1807	157.6157	1701.9806	157.6157	1693.7406	157.6157	1685.
159.3856	1703.9306	159.3856	1695.6506	159.3856	1687.3405	159.3856	1679.
161.1559 162.9259	1704.7006 1698.4306	161.1559 162.9259	1696.2606	161.1559 162.9259	1687.8005 1681.3805	161.1559	1679. 1672.
164.6962	1702.7006	164.6962	1689.9205 1693.9906	164.6962	1681.3805	162.9259 164.6962	1676.
166.4687	1670.1804	166.4687	1661.7004	166.4687	1653.1903	166.4687	1644.
168.2411	1637.9002	168.2411	1629.6502	168.2411	1621.3501	168.2411	1613.
170.0142	1602.81	170.0142	1594.8099	170.0142	1586.7599	170.0142	1578.
171.7845	1590.1299	171.7845	1582.1199	171.7845	1574.0698	171.7845	1566.
173.5644	1586.9899	173.5644	1578.8598	173.5644	1570.6998	173.5644	1562.
	1574.3098	175.3347	1566.1798	175.3347	1557.9997	175.3347	1549.
175.3347							
175.3347 177.1045	1571.1498	177.1045	1562.8797	177.1045	1554.5897	177.1045	1546

APPENDIX XII Simulation results of compressor outlet temp vs pressure drop

(miles)	Pressure (psi)	Distance (miles)	Pressure (psi)	Distance (miles)	Pressure (psi)	Distance (miles)	Pressure (psi)	Distance (miles)	Pressur (psi)
erature (F)		Temperature (F)		emperature (F)		emperature (F)		emperature (F)	(65.)
0	2325.0145	0	2325.0145	0	2325.0145	0	2325.0145	0	2325.0
0	2325.0145	0	2325.0145	0	2325.0145	0	2325.0145	0	2325.0
1.7709	2317.9145	1.7709	2317.7645	1.7709	2317.6245	1.7709	2317.4845	1.7709	2317.3
3.5428	2326.4945	3.5428	2325.8845	3.5428	2325.3145	3.5428	2324.7645	3.5428	2324.2
5.3137	2319.4745	5.3137	2318.7245	5.3137	2318.0045	5.3137	2317.3245	5.3137	2316.6
7.0847	2312.4844	7.0847	2311.5944	7.0847	2310.7344	7.0847	2309.9244	7.0847	2309.0
8.8556	2305.5144	8.8556	2304.4944	8.8556	2303.4944	8.8556	2302.5444	8.8556	2301.5
10.6261	2298.5743	10.6261	2297.4243	10.6261	2296.2843	10.6261	2295.1943	10.6261	2294.1
12.3971 14.1681	2291.6543 2284.7542	12.3971 14.1681	2290.3643 2283.3442	12.3971 14.1681	2289.0943 2281.9442	12.3971 14.1681	2287.8743 2280.5842	12.3971	2286.6
15.9391	2277.8842	15.9391	2276.3342	15.9391	2274.8142	15.9391	2273.3142	14.1681 15.9391	2271.8
17.7101	2271.0442	17.7101	2269.3542	17.7101	2267.7041	17.7101	2266.0841	17.7101	2264.4
19.4811	2264.2141	19.4811	2262.4041	19.4811	2260.6241	19.4811	2258.8741	19.4811	2257.1
21.2511	2257.4241	21.2511	2255.4741	21.2511	2253.5641	21.2511	2251.694	21.2511	2249
23.0222	2250.644	23.0222	2248.564	23.0222	2246.524	23.0222	2244.534	23.0222	2242
24.7932	2243.884	24.7932	2241.684	24.7932	2239.514	24.7932	2237.404	24.7932	2235.2
26.5642	2237.144	26.5642	2234.8239	26.5642	2232.5239	26.5642	2230.2839	26.5642	2228.0
28.3352	2230.4239	28.3352	2227.9839	28.3352	2225.5639	28.3352	2223.1939	28.3352	2220.
30.1061	2223.7139	30.1061	2221.1639	30.1061	2218.6238	30.1061	2216.1338	30.1061	2213.
31.8771	2217.0338	31.8771	2214.3638	31.8771	2211.7038	31.8771	2209.0938	31.8771	2206.
33.6481	2210.3638	33.6481	2207.5838	33.6481	2204.8038	33.6481	2202.0837	33.6481	2199.
35.4182	2203.7237	35.4182	2200.8137	35.4182	2197.9337	35.4182	2195.0937	35.4182	2192.
37.1892	2197.0937	37.1892	2194.0637	37.1892	2191.0737	37.1892	2188.1136	37.1892	2185.
38.9602	2190.4937	38.9602	2187.3436	38.9602	2184.2236	38.9602	2181.1636	38.9602	2178.0
40.7311	2183.9036	40.7311	2180.6336	40.7311	2177.4036	40.7311	2174.2236	40.7311	2171.
42.5021	2177.3336	42.5021	2173.9436	42.5021	2170.5935	42.5021	2167.3135	42.5021 44.2731	2164. 2157.
44.2731 46.0441	2170.7735 2164.2335	44.2731 46.0441	2167.2735 2160.6235	44.2731 46.0441	2163.8035 2157.0435	44.2731 46.0441	2160.4135 2153.5234	46.0441	2157.
47.8152	2157.7135	47.8152	2153.9934	47.8152	2150.2934	47.8152	2146.6634	47.8152	2143.
49.5852	2151.2034	49.5852	2147.3734	49.5852	2143.5634	49.5852	2139.8233	49.5852	2145.
51.3561	2144.7034	51.3561	2140.7734	51.3561	2136.8533	51.3561	2133.0033	51.3561	2129.
53.1271	2138.2233	53.1271	2134.1833	53.1271	2130.1533	53.1271	2126.1933	53.1271	2122.
54.8981	2131.7433	54.8981	2127.6033	54.8981	2123.4732	54.8981	2119.4032	54.8981	2115.
56.6691	2125.2833	56.6691	2121.0432	56.6691	2116.8132	56.6691	2112.6332	56.6691	2108.
58.4402	2118.8332	58.4402	2114.4932	58.4402	2110.1532	58.4402	2105.8831	58.4402	2101.
60.2112	2112.4032	60.2112	2107.9531	60.2112	2103.5131	60.2112	2099.1431	60.2112	2094.
61.9822	2105.9831	61.9822	2101.4231	61.9822	2096.8931	61.9822	2092.413	61.9822	208
63.7542	2099.5731	63.7542	2094.9031	63.7542	2090.273	63.7542	2085.693	63.7542	208:
65.5252	2093.1731	65.5252	2088.403	65.5252	2083.663	65.5252	2078.993	65.5252	2074.
67.2962	2086.793	67.2962	2081.913	67.2962	2077.073	67.2962	2072.3029	67.2962	2067.
69.0661	2080.423	69.0661	2075.4529	69.0661	2070.4929	69.0661	2065.6329	69.0661	2060.
70.8371	2074.0629 2067.7129	70.8371 72.6081	2068.9829	70.8371 72.6081	2063.9329	70.8371 72.6081	2058.9628	70.8371 72.6081	2053.
72.6081 74.3792				72.6081	2057.3828	74.3792			2047.
76.1502	2061.3629 2055.0328	74.3792 76.1502	2056.0928 2049.6628	76.1502	2050.8428 2044.3127	76.1502	2045.6628	74.3792 76.1502	2040. 2033.
77.9212	2048.7028	77.9212	2043.2427	77.9212	2037.8027	77.9212	2032.4227	77.9212	2027
79.692	2042.3827	79.692	2036.8327	79.692	2031.2927	79.692	2025.8226	79.692	2020
81.4631	2036.0727	81.4631	2030.4327	81.4631	2024.7926	81.4631	2019.2326	81.4631	2013
83.2341	2029.7627	83.2341	2024.0326	83.2341	2018.3026	83.2341	2012.6526	83.2341	2006
85.0051	2023.4526	85.0051	2017.6426	85.0051	2011.8225	85.0051	2006.0725	85.0051	2000
86.7752	2017.1626	86.7752	2011.2525	86.7752	2005.3525	86.7752	1999.5125	86.7752	1993.
88.5462	2010.8625	88.5462	2004.8725	88.5462	1998.8825	88.5462	1992.9624	88.5462	1987
90.317	2004.5825	90.317	1998.5025	90.317	1992.4224	90.317	1986.4124	90.317	1980
92.0881	1998.3025	92.0881	1992.1324	92.0881	1985.9624	92.0881	1979.8623	92.0881	1973
93.8591	1992.0224	93.8591	1985.7624	93.8591	1979.5123	93.8591	1973.3323	93.8591	1967
95.6301	1985.7624	95.6301	1979.4023	95.6301	1973.0623	95.6301	1966.7923	95.6301	1960.
97.4011	1979.5023	97.4011	1973.0523	97.4011	1966.6223	97.4011	1960.2722	97.4011	1953
99.1722	1973.2423	99.1722 100.9411	1966.7023	99.1722	1960.1822 1953.7522	99.1722	1953.7422	99.1722	1947
100.9411	1967.0023		1960.3722	100.9411 102.7112		100.9411 102.7112	1947.2321	100.9411	1940.
102.7112	1960.7622	102.7112 104.4811	1954.0422		1947.3321 1940.9221		1940.7221	102.7112	1934
104.4811 106.2511	1954.5222 1948.2922	106.2511	1947.7121 1941.3921	104.4811 106.2511	1934.5121	104.4811 106.2511	1934.2121 1927.712	104.4811 106.2511	192
108.0212	1942.0621	108.0212	1935.0721	108.0212	1928.102	108.0212	1921.222	108.0212	1914
109.7911	1935.8321	109.7911	1928.762	109.7911	1921.702	109.7911	1914.7319	109.7911	1907
111.5612	1929.602	111.5612	1922.452	111.5612	1915.3019	111.5612	1908.2419	111.5612	1901
113.3411	1923.342	113.3411	1916.1019	113.3411	1908.8819	113.3411	1901.7319	113.3411	1894
115.1112	1917.112	115.1112	1909.7919	115.1112	1902.4819	115.1112	1895.2518	115.1112	1888
116.8811	1910.8919	116.8811	1903.4919	116.8811	1896.1018	116.8811	1888.7818	116.8811	1881
118.6511		118.6511	1897.1818	118.6511	1889.7118	118.6511	1882.3117	118.6511	1874
120.4212		120.4212	1890.8818	120.4212	1883.3217	120.4212	1875.8417	120.4212	1868
122.1911		122.1911	1884.5718	122.1911	1876.9417	122.1911	1869.3817	122.1911	1861
123.9612	1885.9818	123.9612	1878.2717	123.9612	1870.5517	123.9612	1862.9116	123.9612	1855.
125.7311	1879.7517	125.7311	1871.9617	125.7311	1864.1716	125.7311	1856.4516	125.7311	1848
127.5023	1855.8816	127.5023	1848.2215	127.5023	1840.5615	127.5023	1832.9714	127.5023	1825
129.2725	1840.8315	129.2725	1833.2014	129.2725	1825.5714	129.2725	1818.0013	129.2725	1810
131.0424	1833.6514	131.0424	1825.9614	131.0424	1818.2613	131.0424	1810.6313	131.0424 132.8248	1802
132.8248 134.5947	1802.0612 1795.7012	132.8248 134.5947	1794.5912 1788.1512	132.8248 134.5947	1787.1111 1780.5911	132.8248 134.5947	1779.6911 1773.1011	132.8248	1772 176
136.3652	1780.6811	136.3652	1773.1611	136.3652	1765.631	136.3652	1758.151	134.3947	1750
138.135	1773.4311	138.135	1765.841	138.135	1758.241	138.135	1750.7009	138.135	1743
139.9051	1767.031	139.9051	1759.371	139.9051	1751.6909	139.9051	1744.0709	139.9051	1736
141.6754		141.6754	1745.2409	141.6754	1737.5708	141.6754	1729.9708	141.6754	1722
143.4453		143.4453	1738.7408	143.4453	1730.9908	143.4453	1723.3107	143.4453	1715
145.2153	1736.6108	145.2153	1728.8408	145.2153	1721.0607	145.2153	1713.3307	145.2153	1705
146.9854	1725.0408	146.9854	1717.2607	146.9854	1709.4507	146.9854	1701.7106	146.9854	1693
148.7555	1718.5707	148.7555	1710.7107	148.7555	1702.8306	148.7555	1695.0106	148.7555	1687
150.5256		150.5256	1704.1606	150.5256	1696.2006	150.5256	1688.3005	150.5256	1680
152.3055		152.3055	1697.5606	152.3055	1689.5205	152.3055	1681.5405	152.3055	1673
154.0758	1690.6005	154.0758	1682.6205	154.0758	1674.6004	154.0758	1666.6404	154.0758	1658
155.8456		155.8456	1676.0105	155.8456	1667.9204	155.8456	1659.8804	155.8456	1651
157.6157		157.6157	1669.4004	157.6157	1661.2304	157.6157	1653.1103	157.6157	1644
159.3856	1670.9904	159.3856	1662.7704	159.3856	1654.5303	159.3856	1646.3303	159.3856	1638
161.1559	1671.1404	161.1559	1662.7804	161.1559	1654.3803	161.1559	1646.0303	161.1559	1637
162.9259	1664.5804	162.9259	1656.1403	162.9259	1647.6703	162.9259	1639.2402	162.9259	1630.
164.6962	1668.0804	164.6962	1659.4503	164.6962	1650.7903	164.6962	1642.1802	164.6962	1633.
166.4687	1636.4402	166.4687	1628.0202	166.4687	1619.5601	166.4687	1611.15	166.4687	160
168.2411	1605.02	168.2411	1596.8	168.2411	1588.5399	168.2411	1580.3199	168.2411	1572.
170.0142	1570.8898	170.0142	1562.8997	170.0142	1554.8597	170.0142	1546.8596	170.0142	1538.
171.7845	1558.1797	171.7845	1550.1797	171.7845	1542.1296	171.7845	1534.1196	171.7845	1526.
173.5644	1554.5897	173.5644	1546.4696	173.5644	1538.3096	173.5644	1530.1795	173.5644	1522.
	1541.8696	175.3347	1533.7396	175.3347	1525.5695	175.3347	1517.4295	175.3347	1509.
175.3347 177.1045	1538.2396	177.1045	1529.9995	177.1045	1521.7095	177.1045	1513.4494	177.1045	1505.