# The Empirical Relationship Acoustic Impedance and Thermal Conductivity

by

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Dissertation submitted in partial fulfilment of the requirements for the Bachelor of Engineering (Hons) (Petroleum Engineering)

### **JAN 2011**

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Final Year Project II

### **CERTIFICATION OF APPROVAL**

# THE EMPIRICAL RELATIONSHIP BETWEEN ACOUSTIC IMPEDANCE AND THERMAL CONDUCTIVITY

by

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A project dissertation submitted to the Petroleum Engineering Programme Universiti Teknologi PETRONAS in partial fulfilment of the requirement for the Bachelor of Engineering (Hons) (Petroleum Engineering)

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**July 2010** 

## **CERTIFICATION OF ORIGINALITY**

This is to certify that I am responsible for the work submitted in this project, that the original work is my own except as specified in the references and acknowledgements, and that the original work contained herein have not been undertaken or done by unspecified sources or persons.

MUHAMMAD HAFIZZUDIN BIN ABDUL WAHID

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## ACKNOWLEDGEMENT

I would like to take this opportunity to thank everyone whom has given their support and help throughout the whole period of completing this project.

First and foremost, I would like to acknowledge the endless help, support and guidance received from my supervisor, Assoc. Prof. Wan Ismail bin Wan Yusoff throughout the whole period of completing this final year project despite their many other obligations. His guidance has really been the main source of motivation and has driven me in completing this project successfully.

Appreciation is also extended to FYP coordinator, Pn Mazuin bt Jasamai, for his systematic approach and timely arrangement as well as valuable advices for this project. Genuine gratitude is dedicated to the examiners and evaluators.

Special thanks go to my family and my fellow friends who gave moral support to motivate me in pursue to greater heights in the project.

Thank You.

With Utmost Gratitude,

(Muhammad Hafizzudin bin Abdul Wahid)

Final Year Project II

| LIMPLE OF CONTENTS | TA | BL | Æ | OF | CON | TENTS |
|--------------------|----|----|---|----|-----|-------|
|--------------------|----|----|---|----|-----|-------|

| CERTIFICATION OF APPROVAL                    |
|--|
| CERTIFICATION OF ORIGINALITY                 |
| ACKNOWLEDGEMENT4                             |
| TABLE OF CONTENTS                            |
| LIST OF ILLUSTRATIONS                        |
| LIST OF TABLES                               |
| ABSTRACT                                     |
| CHAPTER 1: INTRODUCTION                      |
| 1.1 Project Background                       |
| 1.2 Problem Statement                        |
| 1.4 Scope of Work11                          |
| CHAPTER 2: LITERATURE REVIEW AND THEORY12    |
| 2.1 Topic 1: Rock Physical Properties12      |
| 2.1.1 Porosity                               |
| 2.1.2 Permeability                           |
| 2.2 Topic 2: Acoustic Impedance15            |
| 2.3 Topic 3: Thermal Conductivity17          |
| 2.3.1 Thermal Conductivity for igneous rocks |
| 2.4 Topic 4: Interpretation of well logs21   |
| CHAPTER 3: METHODOLOGY22                     |

| 3.1 Project Flow Chart   |
|--|
| 3.2 Project Flow Discreption   |
| 3.3 Project Activities and Key Milestone   |
| 3.4 Project Gant Chart:  |
| CHAPTER 4: RESULTS AND DISCUSSION  |
| 4.1 DELTA-1 and HONEY-1 Wells  |
| 4.2 Data Gathering and Data Analysis28   |
| CHAPTER 5: CONCLUSION AN RECOMMENDATION  |
| CHAPTER 6: REFERENCES  |
| CHAPTER 7: APPENDICES  |
| LIST OF ILLUSTRATIONS  |
| Figure 1: Lithology log and example P-wave velocity and gamma density data collected 15          |
| Figure 2: Flow diagram illustrating the major steps in the model-driven inversion of the seismic |
| data to yield acoustic impedance 16  |
| Figure 3: Evaluation of Shale Volume and Types   |
| Figure 4: Mineralogy of igneous rocks and the magmas   |
| Figure 5: Density and thermal conductivity for plagioclase and olivine depend on the anorthite   |
| and fayalite content, respectively   |
| Figure 6: Flow Chart of the Project  |
| Figure 7: Crossplot of Thermal Conductivity versus Acoustic Impedance in DELTA-1 well30          |
| Figure 8: Crossplot of Thermal Conductivity versus Acoustic Impedance in HONEY-1 well34          |

| Figure 9: Crossplot of Thermal Conductivity versus Acoustic Impedance in DELTA-1 well      |
|--|
| without consider facies  |
| Figure 10: Crossplot of Thermal Conductivity versus Acoustic Impedance in HONEY-1 well     |
| without consider facies  |
| Figure 11: Crossplot of Thermal Conductivity versus Acoustic Impedance in DELTA-1 well for |
| sand only  |
| Figure 12: Crossplot of Thermal Conductivity versus Acoustic Impedance in DELTA-1 well and |
| HONEY-1 well without consider facies   |

## LIST OF TABLES

| Table 1: Density and thermal conductivity of certain minerals which dominated the composition | n  |
|---|----|
| in igneous rock types   | 20 |
| Cable 2: Classification of the common wireline log well measurements                          | 21 |
| Table 3: The empirical equation rlating thermal conductivity and log parameter                | 25 |
| Sable 4: Project Timeline   | 26 |
| Table 4: Project Gant Chart       2   | 27 |
| Fable 5: DELTA-1 well data interpretation of the log correlation                              | 29 |
| Cable 6: Summaries of rock properties for DELTA-1 well  | 31 |
| Cable 7: HONEY-1 well data interpretation   | 33 |

## ABSTRACT

Final Year Project (FYP) is an individual research project in connection with a special engineering problem and under the guidance of a faculty member. The project undertaken may fall under one of the following areas; mathematical analysis, experimental tests, computer simulation, hardware and/or software development, device fabrication.

The course outcome:

- Produce an acceptable project proposal.
- Obtain and evaluate the relevance and quality of information and data from related literatures
- Identify and propose various implementation strategies and select the appropriate methodology. (experiment, design, modeling)
- Produce reports on the project and present orally.

The project selected was The Empirical relationship between Acoustic Impedance and Thermal Conductivity.

Rock have different kind of property and as student in Universiti Teknologi PETRONAS, which related in oil and gas industry, the properties of rock that have to be look for is porosity and permeability. With this kind of properties, the field can be describing as good or bad reservoir. The main purpose of the project is to find a relationship between the Acoustic Impedance and Thermal Conductivity. This will provide information on thermal properties of subsurface from the seismic data.

## **CHAPTER 1: INTRODUCTION**

#### **1.1 Project Background**

The interior heat of the earth is transmitted to its surface mainly by three mechanisms: radiation, convection and conduction [1]. In the earth's lithosphere conduction of heat generally dominates among these mechanisms. Reference [2] in evaluating the permanent heat flow form the Earth's interior to its surface, estimated that 17% of the heat flow can be attributed to the earth's cooling, whereas 83% would be attributed to radiogenic heat production.

The basic concept of heat flow defines this property as a temperature difference between two locations resulting in a heat flow q. The magnitude of q depends on the thermal conductivity of the material and the distance between the two locations mentioned earlier. Heat flow studies provide information on the occurrence and nature of geothermal resources, oil source rock maturation, secondary migration of petroleum and subsurface structures [3], [4] and [5]. Heat flow studies in geological systems are paramount interest to the oil and gas industry. The studies give an indication on the thermal maturity of the hydrocarbon reserves and also provide a better enhanced understanding of the reservoir.

Acoustic impedance is the product of density and seismic velocity (in geophysics definition) at which varies among different rock layers, commonly symbolized by Z. The difference in acoustic impedance between rock layers affects the reflection coefficient. Acoustic velocity or seismic velocity is the rate at which a wave travels through a medium (a scalar) or the rate at which a body is displaced in a given direction (a vector), commonly symbolized by v. Unlike the physicist's definition of velocity as a vector, its usage in geophysics is as a property of a medium-distance divided by travel time.

Velocity can be determined from laboratory measurements, acoustic logs and vertical seismic profiles or from velocity analysis of seismic data. Velocity can vary vertically, laterally and azimuthally in anisotropic media such as rocks, and tends to increase with depth in the Earth because compaction reduces porosity.

Velocity also varies as a function of how it is derived from the data. For example, the stacking velocity derived from normal move out measurements of common depth point gathers

differs from the average velocity measured vertically from a check-shot or vertical seismic profile (VSP). Velocity would be the same only in a constant velocity (homogeneous) medium.

The reflection coefficient is the ratio of amplitude of the reflected wave to the incident wave, or how much energy is reflected. If the wave has normal incidence, then its reflection coefficient can be expressed as:

$$\begin{split} R &= (\rho_2 V_2 - \rho_1 V_1) / (\rho_2 V_2 + \rho_1 V_1), \\ \text{where } R &= \text{reflection coefficient, whose values} \\ &= \text{range from } -1 \text{ to } +1 \\ \rho_1 &= \text{ density of medium } 1 \\ \rho_2 &= \text{ density of medium } 2 \\ V_1 &= \text{ velocity of medium } 1 \\ V_2 &= \text{ velocity of medium } 2. \end{split}$$

The reflection coefficient will be affected by the difference in acoustic impedance between rock layers.

### **1.2 Problem Statement**

Several problem statements are identifying which result for this project:

- Lack of information on the reservoir properties and characterization from the Thermal Conductivity data used nowadays. It was a lot of information of the reservoir properties using Acoustic Impedance.
- Difficulties to find the relationship of Thermal Conductivity to Acoustic Impedance.

### 1.3 Objective

The main objectives of this project are:

- to find the empirical relationship between the Acoustic Impedance and Thermal Conductivity
- To interpret the empirical relationship with respect of depositional of environment and facies
- To come out with physical rock properties database with respect to log interpretation for each depositional of environment and facies

#### 1.4 Scope of Work

This project is relevant to the study of Petroleum Geoscience and Reservoir Engineering as well as the field of Formation Evaluation. It concerns us with the evaluation of thermal conductivity and geothermal gradients of the reservoir. It does also give some understanding about the temperature that is as important as pressure to determine reservoir properties. Temperature is also required for calculations of hydrocarbon recovery factors, including pressure-volume-temperature relationships, and gas-oil ratios (S.Prensky, 1992). Another way to get the reservoir properties is by well-log correlations data.

This project focuses on how to interpret the log data such as gamma ray log, density log, and resistivity log. All this logging tools describe the formation of the rock to interpret the reservoir parameters. The data obtain from the log as well as well report, are integrate to get the thermal conductivity and acoustic impedance for each sequence in the reservoir.

As a result, the database obtained for each sequence of the reservoir would be useful for petrophysicist to make a decision according the data.

The scope of studies covers on:

- Interpretation the log data such as gamma ray log, density log, sonic log and neutron log.
- Integration sample data and log interpretation.
- Study of various log parameters with respect to environment of depositional and facies

## **CHAPTER 2: LITERATURE REVIEW AND THEORY**

In order to obtain a good understanding of the study, a lot of literature review had been performed since the beginning of the project. It includes the understanding and knowledge from journals, trusted articles, reference books, research-based websites and other available resources.

The literature review was divided into four topics:

Topic 1: Rock Physical Properties

Topic 2: Acoustic Impedance

Topic 3: Thermal Conductivity

These chapters were divided according to relevant studies in Petroleum Engineering field.

## 2.1 Topic 1: Rock Physical Properties

When we talk about reservoir rock, there were two kinds of physical properties that are related which are porosity for storage capacity and permeability for production capacity.

### 2.1.1 Porosity

Porosity can be defined as:

- A measure of the void spaces in a material and is measured as a fraction between 0 1 or as a percentage between 0 – 100%. (Wikipedia)
- The percentage of pore volume or void space or that volume within rock that can contain fluids. (Schlumberger Oilfield Glossary)

- A measure of the space available for storage of petroleum hydrocarbon.  $(0.1 < \Phi < 0.4)$ Mathematical expression for porosity:

Porosity = 
$$\frac{Pore Volume}{Bulk Volume}$$
  
=  $\frac{Bulk Volume - Grain Volume}{Bulk Volume} = \frac{V_b - V_s}{V_b}$ 

For the type of porosity, according to mode of origin, there were two types which are:

- 1- Primary porosity formed at the time sediment was deposited
- 2- Secondary porosity the porosity created through alteration of rock, commonly by process such as dolomitization, dissolution and fracturing

For type of porosity according to connectivity, there were two types which are:

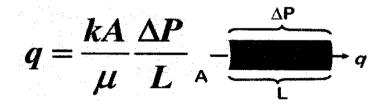
- 1- Absolute porosity -- the ratio of the total void space in a rock to the bulk volume of that rock
- 2- Effective porosity the ratio of the interconnected void space in a rock to bulk volume of that rock. This type of porosity is important for the reservoir engineering standpoint.

The porosity of a reservoir rock may be determined by:

- Core analysis
- Well logging technique
- Well testing

### 2.1.2 Permeability

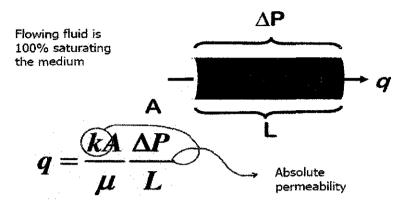
Permeability defines as a measure of the capacity of the porous medium to transmit fluids. This method introduced by Darcy in 1856 while investigating the flow of water through sand filters for water purification. Permeability can be express mathematically:



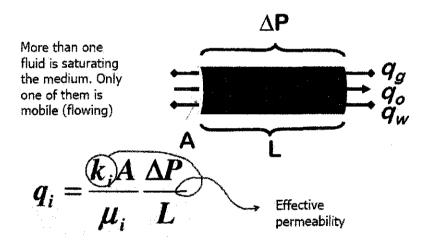
There are 3 types of permeability which are:

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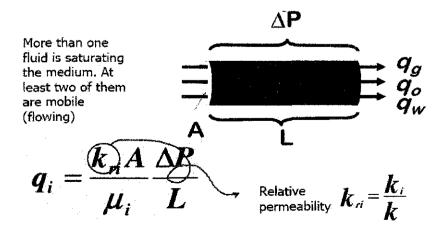
#### 1- Absolute permeability



2- Effective permeability



3- Relative permeability



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#### 2.2 Topic 2: Acoustic Impedance

Acoustic impedance (Z) is the product of rock density and P-wave velocity, both of which can be directly measured by well logging. The determination of such parameter is important for identifying reflectors, detecting lateral variations of lithology, and used for detailed investigation hydrocarbon fields. The variation of Z is highly affected by density and velocity.[1]

The relationships between these two parameters is given by Gardner et al. (1974), which is approximately correct for brine saturated sedimentary rocks, over a wide range of basins, geologic ages and depths. This enables velocity to be computed from acoustic impedance, and vice versa, in most sedimentary rocks: except for salt, anhydrite and hydrocarbon reservoirs.

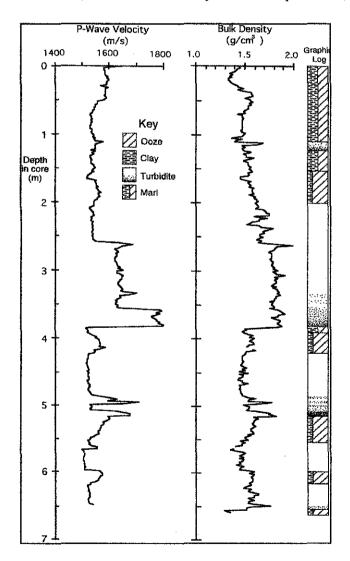


Fig.1. Lithology log and example P-wave velocity and gamma density data collected with SOC's MSCL on a split core from the North Atlantic[2]

Acoustic impedance is the product of rock density and compressional (P-wave) velocity. It is thus a measure of physical properties that are commonly measured in boreholes, such as bulk density and sonic velocity, as well as being qualitatively observed in core and outcrop as the dhardnessT of the rock. Seismic inversion is a method of deriving seismic parameters, such as acoustic impedance, from reflection seismic data constrained by borehole data [2].

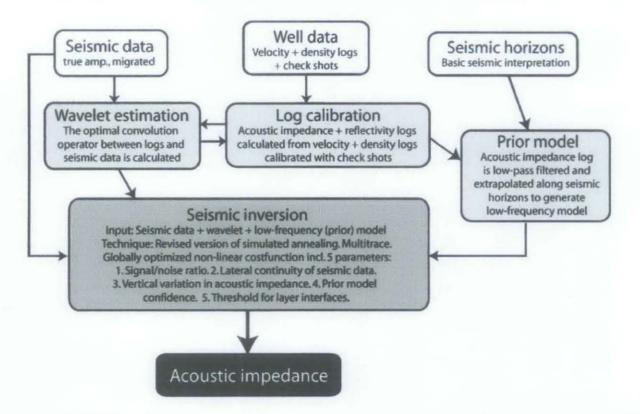


Fig. 2 Flow diagram illustrating the major steps in the model-driven inversion of the seismic data to yield acoustic impedance[3]

The minimum, maximum and average values of acoustic impedance determined with the Eq. (I-15) are in a good agreement.[1]

$$Z = \frac{1}{\Delta_{\rm t}} \left[ \left\{ V_{\rm sh} \left( \frac{\rho_{\rm sh} - \rho_{\rm ma}}{\rho_{\rm f} - \rho_{\rm ma}} - \frac{\Delta_{\rm tsh} - \Delta_{\rm tma}}{\Delta_{\rm tf} - \Delta_{\rm tma}} \right) + \frac{\Delta_{\rm t} - \Delta_{\rm tma}}{\Delta_{\rm tf} - \Delta_{\rm tma}} \right\} (\rho_{\rm f} - \rho_{\rm ma}) + \rho_{\rm ma} \right]$$
(I-15)

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| Table 1<br>Evaluation of sl  | tale volume and types                                    |  |              |  |            |  |  |      |         |
|--|--|--|--------------|--|------------|--|--|------|---------|
| Shale volume d   | etermination   |  |              |  |            |  |  |      |         |
| V <sub>sh</sub> =(GR – GR <sub>n</sub><br>(Schlumberger,<br>Shale volume o               |  |  |              |  |            |  |  |      |         |
| Clavier et al. (1791)<br>$V_{\rm sh} = 1.7 - \sqrt[3]{3.38} - (X+0.7)^2$                 |  | Steiber (1973)         Dresser Atlas (1979) $V_{sh} = 0.5 \mathcal{N} (1.5 - \mathcal{X})$ $V_{sh} = 0.33 [2^{(2.0)} - 1]$ |              |  |            |  |  |      |         |
| CEC calculation  | 1  |  |              |  |            |  |  |      |         |
| Waxman and Si<br>CEC – 10(1.983<br>Shale types<br>Clay type                              | nits (1968)<br>$2 \times V_{sh} = 2.4473$ )<br>Clay name | Formula  |              | Density (g/cm3)                          | CEC (meq/g |  |  |      |         |
| Effective  | Montmorillonite  | (1/2Ca,Na)0.7(A1,Mg,Fe)4(Si,Al8O20)(OH)4   |              | (1/2Ca,Na)0,7(A1,Mg,Fe)4(Si,AlgO20)(OH)4 |            | (1/2Ca,Na)0,7(Al,Mg,Fe)4(Si,AlgO20)(OH)4 |  | 2.12 | 0.8-1.5 |
|  | Illite   | $K_{1-1.5}Al_4(Si_{6.5-7.0}Al_{1.0-}$  | 1.5O20)(OH)4 | 2.52                                     | 0.1 - 0.4  |  |  |      |         |
| neffective Kaolinite Al <sub>4</sub> (Si <sub>4</sub> O <sub>10</sub> )(OH) <sub>8</sub> |  |  |              | 2.41                                     | 0.03 - 0.1 |  |  |      |         |
|  | Chlorite   | (Mg,AI,Fe) <sub>12</sub> (Si,Al) <sub>8</sub> O <sub>20</sub> (O)  | Dis          | 2.77                                     | 0.0        |  |  |      |         |

Fig. 3 Evaluation of Shale Volume and Types[3]

#### 2.3 Topic 3: Thermal Conductivity

The transfer of energy between two adjacent parts of rock mainly depends on its thermal conductivity. Energy transfer arising from the temperature difference between the adjacent parts of the body is called heat conduction. The amount of heat to be transferred through any body depends upon a number of factors, such as the particle shape, porosity, temperature range, solid constituents, moisture content, uniaxial and/or triaxial pressure exerted on the rock, It widely influences the energy transfer between adjacent rocks in underground mines and in insulation of the building by providing an energy efficient solution.[4]

The thermal conductivity is determined by the measurements of temperature gradient in the rock and heat input [6]. In general, the thermal conductivity can be calculated using Fourier's Law as given below:

$$\frac{\mathrm{d}Q}{\mathrm{d}t} = -kA \,\frac{\mathrm{d}T}{\mathrm{d}x}$$

Thermal conductivity can be determined by different methods, e.g.:(1)laboratory measurements,(2) estimation from mineral composition,(3) in situ field measurement sand(4)large- scale field experiments. The various common rock forming minerals have different

thermal conductivities. Knowing the thermal conductivity of the constituent minerals, one can estimate the thermal conductivity for any rock with known mineral composition.[5]

The thermal conductivity of inorganic, solid materials is generally regarded as being proportional to density. This is normally a function of porosity. Increasing porosity gives both lower density and lower thermal conductivity. This is obvious in porous media such as soils and sedimentary rocks. The denser the internal structure, the lower is the resistance to the transfer of heat energy between the different parts of the solid material.

In an anisotropic crystal, the thermal conductivity varies according to crystallographic orientations. The thermal conductivity of a crystalline rock depends largely on mineral composition, density, and the thermal conductivity of the constituent minerals {15}.[5]

#### 2.3.1 Thermal Conductivity for igneous rocks

Rocks can be grouped according to the method of formation (igneous, sedimentary and metamorphic). For a systematization of igneous rocktypes, the SiO2 level is of special significance: felsic >63% SiO2, intermediate 52–63% SiO2, mafic 45–52% SiO2, and ultramafic <45% SiO2. When classifying igneous rock types according to the internationally accepted UGS system, the division is based on the content of three mineral components in the rock: quartz (Q), alkali feldspar (A) and plagioclase (P).[5]

The chemical composition of the different minerals is influenced by the composition of the parent magma, as well as the temperature at which crystallization occurs from the magma. For example, minerals that crystallize at high temperatures (1100–1200 1C) contain high amounts of iron, magnesium and calcium whilst minerals that crystallize at low temperatures (700–800 1C) are richer in potassium ands odium.[5]

Final Year Project II

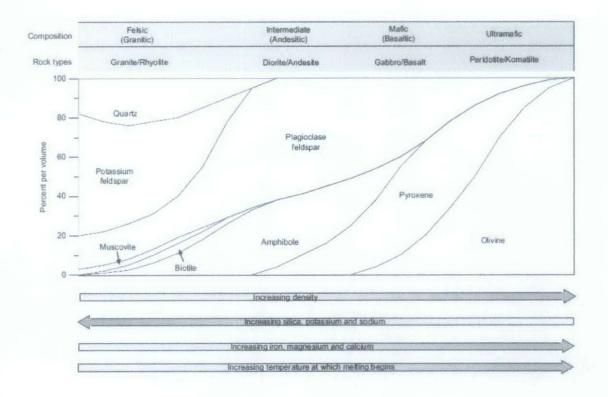


Fig. 4 Mineralogy of igneous rocks and the magmas [5]

The average density of rock types in the earth's crust is 2850 kg/m3. The density of a rock obviously depends on the density of the minerals in the rock. The density of a mineral depends on its chemical composition and crystalline structure. Most common rock-forming minerals have a density of between 2000 and 3000 kg/m3. So-called heavy minerals, with a density greater than 2850 kg/m3, include, for example, oxide and sulphide minerals and the solid metals. For igneous rock, Quartz has highest thermal conductivity of the common rock forming minerals.[5]

19

Final Year Project II

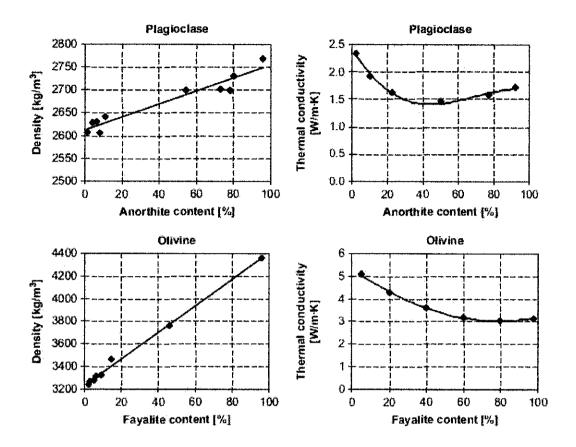


Fig.5 Density and thermal conductivity for plagioclase and olivine depend on the anorthite and fayalite content, respectively. [5]

| Mineral               | Density (kg/m <sup>4</sup> ) | Thermal conductivity (W/(mK)) | Comments   |
|-----------------------|------------------------------|-------------------------------|--|
| Ouartz                | 2674                         | 7.69                          |  |
| Alkali feldspar       | 2571                         | 2.40                          |  |
| Muscovice             | 2852                         | 2.32                          |  |
| Biotite               | 2981                         | 2.02                          |  |
| Plagiociase*          | 26501 (2606-2769)            | 1631 (146-2.34)               | An15-An30 assumed  |
| Amphibole             | 3183                         | 2.81                          | All amphibole assumed to be hornblende                           |
| Pyroxene <sup>2</sup> | 3275                         | 3.82                          | All pyroxene as used to be clinopyrozene with augite composition |
| Olivine <sup>a</sup>  | 3501* (3322-3765)            | 4.572 (3.18-5.1)              | <sup>2</sup> Fa15 assumed  |

 Table 1: Density and thermal conductivity of certain minerals which dominate the composition in igneous rock types

 [5]

Final Year Project II

## 2.4 Topic 4: Interpretation of well logs

Well log is the continuous recording of a geophysical parameter along a borehole. The value of the measurement is plotted continuously against depth in the well. It has often been called an 'electrical log' because historically the first logs were electrical measurement of electrical properties. However, the measurements are no longer simply electrical, and modern methods of data transmission do not necessarily need a wire line. Well logging was first invented by Conrad Schlumberger and Henri Doll. (Rider, 2002)

Well logging is necessary because geological sampling during drilling (cuttings sampling) leaves a very imprecise record of the formations encountered. Entire formation samples can be brought to the surface by mechanical coring, but this is both slow and expensive. The results of coring are unequivocal while logging is precise but equivocal. Logs fill the gap between 'cuttings' and 'cores'. (Rider, 2002)

|  | Log Type               | Formation parameter measured          |
|--|------------------------|---------------------------------------|
| Mechanical measurement<br>Spontaneous<br>measurement | Caliper<br>Temperature | Hole diameter<br>Borehole temperature |
|  | SP (self-potential)    | Spontaneous electrical currents       |
| (vij latni aj klastika da Kantuzev izvalizija)<br>I  | Gamma ray              | Natural radioactivity                 |
| Induced measurement                                  | Resistivity            | Resistance to electrical current      |
| an baran kalendari san santa shikanika sa ku         | Induction              | Conductivity of electrical current    |
|  | Sonic                  | Velocity of sound propagation         |
| alingke montest haar le prosintra skala hoord.<br>T  | Density                | Reaction to gamma ray bombardment     |
|  | Photoelectric          | Reaction to gamma ray bombardment     |
| araan ee arten in daren nemtintu aterren deri<br>N   | Neutron                | Reaction to neutron bombardment.      |

Table 2: Classification of the common wireline log well measurements

#### **CHAPTER 3: METHODOLOGY**

In order to fulfill the objective mentioned, first step is to perform the literature review of the project. The literature review can be the current or relevant materials including journals, books, encyclopedia and articles. The literature review was conducted by referring to the information resources available in Universiti Teknologi PETRONAS such as internet, UTP Information Resource Centre, research officer, lecturer, post-graduate student. The information resources also could be obtained from outsiders such as personnel from industrial. The literature review covered on the understanding of physical rock properties, understanding of the thermal conductivity and acoustic impedance in different type of reservoir, and understanding the calculation and interpretation of the well-log correlation to get the similarities between thermal conductivity and acoustic impedance.

Then, select and get data from the well-log interpretation from the Field Development Planning that significant with the project. Afterward, experiment will be conduct by comparing the data between thermal conductivity and acoustic impedance to the similarity from both of it.

In second semester, after we get the data that are related to the project, the research can be started. There were two kind of research which is:

- 1- Logging interpretation
- 2- Data integration

For logging interpretation, it will covered on how to reading the log data, the log pattern for various kind of log so, the logs that were choose is SP logs, Porosity Log and Gamma Ray Log. Then, the data from well-log interpretation was compiled in the table for calculation of acoustic impedance and thermal conductivity. A graph of acoustic impedance versus thermal conductivity had been plotted to get a clear relationship between both parameters.

Lastly, the result of the research will be combined and integrated according to respective environment of deposition.

Final Year Project II

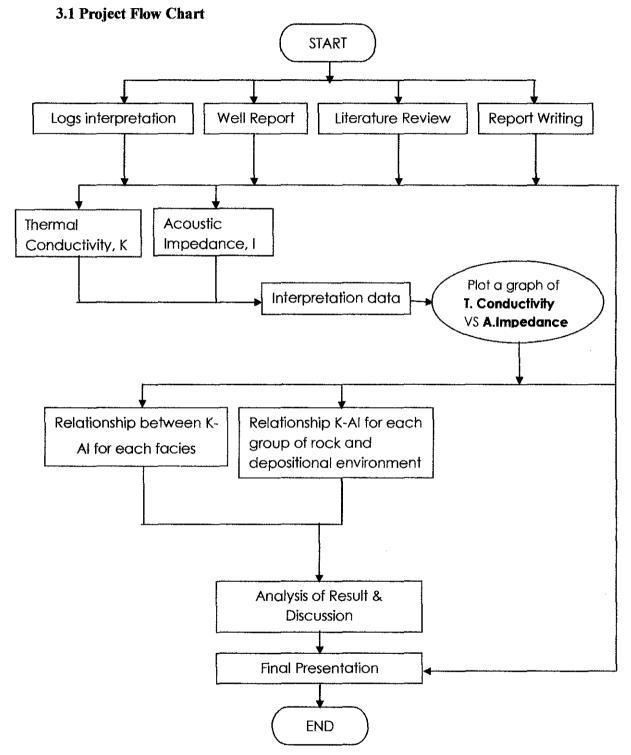


Fig. 6: Flow Chart of the Project

Final Year Project II

#### 3.2 Flow Chart description:

Summary of activities with respect to each item in the flow chart (Figure 6) are as follows:

- 1. Project was proposed to FYP1 committee.
- 2. Doing literature study on this project.
- 3. Collecting the data:
  - o Well log
  - Well report
  - o PVT analysis
  - o Field report
- 4. Interpreting and analyzing the sample data.
- 5. Integrating the data from log interpretation with respect of depositional of environment and facies.
- 6. Calculation
  - A. Volume of Shale, Vsh

$$V_{\rm sh} = (GR - GR_{\rm min})/(GR_{\rm max} - GR_{\rm min})$$
  
(Schlumberger, 1975)

Where:

IGR = gamma ray index GRlog = gamma ray reading of formation GRmin = minimum gamma ray (clean sand or carbonate) GRmax = maximum gamma ray (shale)

### **B.** Acoustic Impedance

#### AI= Velocity x Density

Example:

Depth interval = 5900 m

#### Density, $\rho = 2.47 \text{ gm/cm}^3$

Sonic Transit time,  $\Delta t = 150 \ \mu sec/ft$ 

Velocity =  $1/\Delta t$  (ft/µsec)

=  $1000000 \text{ x} 1/\Delta t$  (ft/sec)

Final Year Project II

 $= 0.3048 \text{ x} (1000000 / \Delta t) \text{ m/sec}$ 

= 0.3048 x (1000000 / 150)

Velocity = 2032 m/sec

 $\therefore$  AI = 2032 m/sec x 2.47 gm/cm<sup>3</sup>

## = <u>5019.04 gm.m/ cm<sup>3</sup>sec</u>

### C. Thermal Conductivity

- Depend on thermal facies (On and Vsh)

| M   | Limit of Log Parameters  | Empirical Equation   |
|-----|--|--|
| кЛ  | ∨f < 20%, Øn < 36%   | $k_{emp} = 6.86 (0.99)^{Vl} (0.98)^{em}$                           |
| kf2 | Vf = or > 20% and < 40%, Øn < 35%<br>>⊃ ≦∀F < 40                         | $k_{emp} = 6.43 \ (0.99)^{Vl} (0.98)^{2m}$                         |
| kf3 | $Vf \ge 40\%$ and < 60%, Øn> 18% < 35%<br>$y_0 \le y_1 \le \omega_0$     | k <sub>emp</sub> ≖ 10.59 (1.00) <sup>Vf</sup> (0.96) <sup>Øn</sup> |
| kf4 | Vf≥60%<85%, Øn>18% < 39%<br>∞≤\:.≤95                                     | $k_{emp} = 5.83 (0.99)^{vf} (1.00)^{cm}$                           |
| kf5 | Vf >13%<30% Øn = or > 33%<60%<br>∴∠(\1 < % <sup>2</sup>                  | $k_{emp} = 13.14 (1.09)^{Vf} (0.91)^{\Theta_0}$                    |
| kf6 | $Vf \ge 30\%$ and < 40%, $On \ge 35\% < 49\%$<br>$_{30} \le 35\% < 40\%$ | $k_{emp} = 12.95(1.03)^{Vf}(0.98)^{Om}$                            |
| kf7 | $Vf = or \ge 40\% < 85\%$ , $@n = or \ge 35\% < 61\%$                    | $k_{emp} = 15.24 (1.01)^{V'} (0.94)^{On}$                          |

Table 3: The empirical equation rlating thermal conductivity and log parameter (Thermal facies) [8] Example:

Depth interval =5900 m

Neutron porosity,  $\Phi n = 24\%$ ; Vsh= 31.74 %; formation temp= 322°C

Thermal facies = kf2

Kemp= 6.43(0.99^31.74)\*(0.98^0.24)

Kemp= 3.98

Corrected:

K corrected= (372\*(3.98-1.84)\*(1/(322+273)-0.00068))+1.84

= <u>2.80</u>

Final Year Project II

7. Compile the data. - The data were compiled into the tables prepared which indicate the

type of thermal facies and the rock properties.

| depth<br>interval<br>(m) | gamma<br>ray<br>(gr) | neutron<br>porosity<br>(Фn) | density<br>ρ,gm/cm<br>3 | sonic<br>transit<br>time(ms/ft) | velocity<br>(m/sec) | Vsh | formation<br>temp<br>(°C) | Acoustic<br>Impedance<br>(x10 <sup>2</sup> ) | Thermal<br>Conductivity | Thermal<br>Facies |
|--------------------------|----------------------|-----------------------------|-------------------------|---------------------------------|---------------------|-----|---------------------------|--|-------------------------|-------------------|
|                          |                      |                             |                         |                                 |                     |     |                           |  |                         |                   |

#### 8. Project Timeline

| Subject            | First Semester   | Second Semester   |
|--------------------|--|---|
| Project Proposal   | an 1990 an 1990<br>I | ang pennengyap 17.000 da sa lama sa peng pa <sup>04</sup> 00 ki 1000 a maan ay ay ang |
| Literature Review  | /  | an a  |
| Collecting Data    |  |   |
| Log interpretation |  | /   |
| Data integration   |  | /   |
| Compile database   |  |   |

9. Raw Materials:

- Logging data

- Well report

- FDP report

10. Softwares Use:

- Microsoft Office 2007 Excel

#### 3.3 Project Activities and Key Milestone

The student plays an important role as an investigator/researcher with the assist and supervision from the supervisor and collaborators. This project requires a precise monitoring from them, and this could be done through a good communication medium such as weekly meeting, progress report and consultations. The student also might want to visit certain the real problem in the industry by having a sharing session from industry personnel which related to the project. Progress report shall be submitted according to the schedule to get to find if there is any corrective action. This is done so that both student and supervisor will have a good and up-to-date communication.

Final Year Project II

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## 3.4 Project Gant Chart:

| WEEK                            | 1 1 | 2 | 3 | 4 | 5     | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13       | 14 | 15 |
|---------------------------------|-----|---|---|---|-------|---|---|---|---|----|----|----|----------|----|----|
| ACTIVITES                       | +   |   |   |   | -     |   |   |   |   |    |    |    |          |    |    |
| Progress Report                 |     |   |   |   | · · · |   |   |   |   |    |    |    |          |    |    |
| Submission the Progress Report  |     |   |   |   |       |   |   |   |   |    |    |    |          |    |    |
| Design the Poster               |     |   |   |   |       |   |   |   |   |    |    |    | <u>}</u> |    |    |
| Poster Presentation             | -   |   |   |   |       |   |   |   |   |    |    |    |          |    |    |
| Technical Report                | 1   |   |   |   |       |   |   |   |   |    |    |    |          |    |    |
| Submission the Technical Report | -   |   |   |   |       |   |   |   |   |    |    |    |          |    |    |
| Dissertation                    |     | İ |   |   | [     |   |   |   |   |    |    |    |          |    |    |
| Submision the Dissertation      |     |   |   |   | 1     |   |   |   |   |    |    |    |          |    |    |
| Submission the Hardbound Copy   |     |   |   |   |       |   |   |   |   |    |    |    |          |    |    |
| Oral Presentation.              |     |   |   |   |       |   |   |   |   |    |    |    |          |    |    |

4

### **CHAPTER 4: RESULTS AND DISCUSSION**

#### 4.1 DELTA-1 and HONEY-1 Well

#### 4.1.1 DELTA-1 Well Background

DELTA-1 well was been drilled in one field in offshore in the block PM315 that call Duyong field. This field located in the Malay Basin that can be divided into 6 regions namely; Northeast, Southeast, North, West, Central and South based on their respective play types and geological location. Duyong field was in the Southeast Region of the Malay Basin. Figure below shows the location of Duyong field on the Malay Basin. [9]

The reservoir is dominated by sand, and intercalated with shale. The sand which is located in this field shows small variation in grain size and sorting. This field produces gas. The Southeast Region contains 62% of entire Peninsular Malaysia gas reserves. 86%ad all associated gas and 15% of all non-associated gas in the Malay Basin occurs in the Southeast Region. [9]

#### 4.1.2 HONEY-1 Well Background

HONEY-1 well was drilled in the Baram Delta that located in the Miri Field. The Baram Delta province is roughly triangular in shape, with its apex occurring onshore and centred in Brunei and the northeastern coastal area of Sarawak. The province expands offshore to cover the whole width of Brunei waters, and encroaches southeast into Sarawak (where it is known as West Baram Delta) and northeast into offshore NW Sabah (Where it is named the East Baram Delta). [9]

The western margin of the Baram Delta is marked by the West Baram Line, system of large, northest-hading, down-to-the-basin faults that separate the delta from the older Balingian and Central Luconia provinces to the west. The eastern margin of the Baram Delta is defined by the Morris Fault-Jerudong Line which separates the delta from the older, intensely tectonised Inboard Belt of offshore NW Sabah. [9]

#### 4.2 Data Gathering and Data Analysis

The data in table below was from the data interpretation of the log correlation for DELTA-1 well in Duyung field. This data use for calculate the Acoustic Impedance and Thermal Conductivity to find the similarity.

| depth interval(m) |        | gamm<br>a ray | neutron<br>porosity (Φn) |       | density<br>p,gm/cm3 | sonic<br>transit | velocity<br>(m/sec) | Vsh       |             | formation<br>temp | Acoustic<br>Impedance | Thermal<br>Conductivity |      | Therm al            |          |           |        |
|-------------------|--------|---------------|--------------------------|-------|---------------------|------------------|---------------------|-----------|-------------|-------------------|-----------------------|-------------------------|------|---------------------|----------|-----------|--------|
| top               | bottom | mid           | (gr)                     | (gr)  | (gr)                | value            | %                   | p,gimento | time(ms/ft) | (imaco)           | value                 | %                       | (°C) | (x10 <sup>2</sup> ) | original | corrected | Facies |
| 5200              | 5235   | 5218          | 75                       | 0.26  | 26                  | 2.43             | 150                 | 2032      | 0.4491      | 44.91             | 288                   | 49.38                   | 3.66 | 2.59                | kt3      |           |        |
| 5235              | 5264   | 5250          | 90                       | 0.3   | 30                  | 2.45             | 180                 | 1693      | 0.6287      | 62.87             | 289                   | 41.49                   | 3.10 | 3.10                | kf4      |           |        |
| 5264              | 5297   | 5281          | 83                       | 0.26  | 26                  | 2.38             | 186                 | 1639      | 0.5449      | 54.49             | 291                   | 39.00                   | 3.66 | 2.58                | kf3      |           |        |
| 5297              | 5320   | 5309          | 98                       | 0.41  | 41                  | 2.36             | 204                 | 1494      | 0.7246      | 72.46             | 292                   | 35.26                   | 2.48 | 2.48                | kt7      |           |        |
| 5320              | 5355   | 5338          | 103                      | 0.36  | 36                  | 2.46             | 165                 | 1847      | 0.7844      | 78.44             | 294                   | 45.44                   | 3.59 | 3.59                | kt7      |           |        |
| 5395              | 5428   | 5412          | 97.5                     | 0.365 | 36.5                | 2.41             | 189                 | 1613      | 0.7186      | 71.86             | 298                   | 38.87                   | 3.26 | 3.26                | k!7      |           |        |
| 5428              | 5450   | 5439          | 100                      | 0.38  | 38                  | 2.45             | 188                 | 1621      | 0.7485      | 74.85             | 299                   | 39.72                   | 2.75 | 2.75                | kf4      |           |        |
| 5450              | 5467   | 5459          | 85                       | 0.375 | 37.5                | 2.44             | 195                 | 1563      | 0.5689      | 56.89             | 300                   | 38.14                   | 2.64 | 2.64                | k17      |           |        |
| 5467              | 5500   | 5484          | 85                       | 0.38  | 38                  | 2.51             | 176                 | 1732      | 0.5689      | 56.89             | 301                   | 43.47                   | 2.56 | 2.56                | k17      |           |        |
| 5500              | 5510   | 5505          | 105                      | 0.38  | 38                  | 2.47             | 181                 | 1684      | 0.8084      | 80.84             | 302                   | 41.59                   | 3.24 | 3.24                | kt7      |           |        |
| 5522              | 5550   | 5536          | 90                       | 0.309 | 30.9                | 2.4              | 162                 | 1881      | 0.6287      | 62.87             | 304                   | 45.16                   | 3.10 | 3.10                | kf4      |           |        |
| 5600              | 5630   | 5615          | 95                       | 0.365 | 36.5                | 2.41             | 190                 | 1604      | 0.6886      | 68.86             | 308                   | 38.66                   | 2.92 | 2.92                | kf4      |           |        |
| 5630              | 5660   | 5645          | 84                       | 0.35  | 35                  | 2.47             | 186                 | 1639      | 0.5569      | 55.69             | 309                   | 40.48                   | 3.04 | 3.04                | k17      |           |        |
| 5660              | 5680   | 5670          | 95                       | 0.345 | 34.5                | 2.4              | 190                 | 1604      | 0.6886      | 68.86             | 311                   | 38.50                   | 2.92 | 2.92                | kf4      |           |        |
| 5680              | 5710   | 5695          | 93                       | 0.37  | 37                  | 2.45             | 194                 | 1571      | 0.6647      | 66.47             | 312                   | 38.49                   | 2.99 | 2.99                | kl4      |           |        |
| 5710              | 5760   | 5735          | 85                       | 0.35  | 35                  | 2.42             | 193                 | 1579      | 0.5689      | 56.89             | 314                   | 38.22                   | 2.54 | 2.11                | kf3      |           |        |
| 5770              | 5790   | 5780          | 40                       | 0.195 | 19.5                | 2.31             | 190                 | 1604      | 0.0299      | 2.99              | 316                   | 37.06                   | 4.78 | 2.95                | kf1      |           |        |
| 5798              | 5812   | 5805          | 45                       | 0.204 | 20.4                | 2.32             | 165                 | 1847      | 0.0898      | 8.98              | 317                   | 42.86                   | 4.60 | 2.88                | kf1      |           |        |
| 5821              | 5846   | 5834          | 55                       | 0.26  | 26                  | 2.43             | 165                 | 1847      | 0.2096      | 20.96             | 319                   | 44.89                   | 3.66 | 2.53                | k/2      |           |        |
| 5855              | 5885   | 5870          | 45                       | 0.215 | 21.5                | 2.28             | 182                 | 1675      | 0.0898      | 8.98              | 321                   | 38.18                   | 4.40 | 2.80                | kf1      |           |        |
| 5885              | 5915   | 5900          | 64                       | 0.24  | 24                  | 2.47             | 157                 | 1941      | 0.3174      | 31.74             | 322                   | 47.95                   | 3.98 | 2.63                | kf2      |           |        |
| 5915              | 5945   | 5930          | 54                       | 0.19  | 19                  | 2.43             | 143                 | 2131      | 0.1976      | 19.76             | 324                   | 51.79                   | 4.88 | 2.97                | kf2      |           |        |
| 5945              | 5960   | 5953          | 69                       | 0.24  | 24                  | 2.48             | 150                 | 2032      | 0.3772      | 37.72             | 325                   | 50.39                   | 3.98 | 2.63                | kt2      |           |        |
| 5960              | 5990   | 5975          | 80                       | 0.29  | 29                  | 2.52             | 173                 | 1762      | 0.5090      | 50.90             | 326                   | 44.40                   | 3.24 | 2.36                | kf3      |           |        |
| 6007              | 6040   | 6024          | 58                       | 0.24  | 24                  | 2.45             | 148                 | 2059      | 0.2455      | 24.55             | 328                   | 50.46                   | 3.98 | 2.62                | kf2      |           |        |
| 6040              | 6072   | 6056          | 88                       | 0.24  | 24                  | 2.48             | 148                 | 2059      | 0.6048      | 60.48             | 330                   | 51.07                   | 3.17 | 3.17                | kf4      |           |        |
| 6072              | 6092   | 6082          | 119                      | 0.35  | 35                  | 2.56             | 155                 | 1966      | 0.9760      | 97.60             | 331                   | 50.34                   | 4.62 | 4.62                | kf7      |           |        |

Table 6: DELTA-1 well data interpretation of the log correlation

#### Final Year Project II

From the data in the table, a graph of thermal conductivity versus acoustic impedance had been made. In the graph below, the real relationship between acoustic impedance and thermal conductivity can be obtained and the distribution of different thermal facies in the DELTA-1 well.

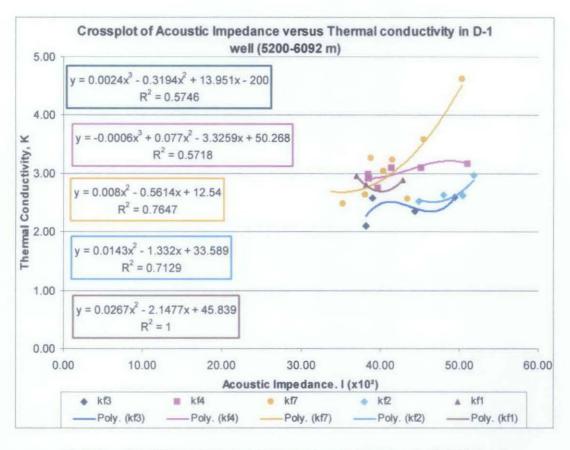


Fig.7 Crossplot of Thermal Conductivity versus Acoustic Impedance in DELTA-1 well

All the points that have their own thermal facies are plotted in the graph in figure 8 above. The points in the graph had been interpreted from the depth of 5200m to 6092m in the DELTA-1 well. It is about 5 types of thermal facies, kf1, kf2, kf3, kf4 and kf7. The range of the acoustic impedance value for this analysis is in between 2.48 to 4.88. On the other hand, the thermal conductivity is in between 20.84 to 27.34. From the table in the figure 7, each depth interval that had been interpreted has different thermal facies. Meaning that, each depth interval has different type of rock properties.

From the well log correlation, there are 4 types of rock in this reservoir in the range of 892 m from top and base. The rocks are sandstone (40%), siltstone (30%), shale (26%) and claystone (4%). Each of this rock has different thermal facies and different value of acoustic impedance and thermal conductivity because of different value of porosity and permeability. Table below shows the summary in DELTA-1 well for each facies and rock property.

| Facies | Type of<br>rock | Neutron<br>porosity,<br><b>D</b> n | Volume of<br>shale, Vsh | Rock Properties   |  |  |
|--------|-----------------|------------------------------------|-------------------------|---|--|--|
| Kfl    | Sandstone       | 19-22%                             | 3-9%                    | <ul> <li>light grey to green</li> <li>fine grain to very fine grain</li> <li>moderate to poor visual porosity and silty matrix</li> </ul>                               |  |  |
| Kf2    | Sandstone       | 19-26%                             | 19-31%                  | <ul> <li>light grey to off white</li> <li>fine grain to very fine grain</li> <li>moderate to poor visual porosity,<br/>silty matrix, calcareous argillaceous</li> </ul> |  |  |
|        | Siltstone       | 24%                                | 37%                     | <ul> <li>Light grey to green grey</li> <li>Firm to moderate hard</li> <li>Non calcareous with micro pyretic</li> </ul>  |  |  |
| Kf3    | Siltstone 26%   |                                    | 44-54%                  | <ul> <li>Light grey to brownish grey</li> <li>Hard and quartzite carbonaceous, calcareous</li> </ul>  |  |  |
|        | Shale           | 35%                                | 56%                     | - Medium grey<br>- Hard fissile splintery   |  |  |

31

Final Year Project II

| Kf4 | Shale     | 30-36% | 62-68%  | <ul> <li>Light greenish grey to medium grey</li> <li>Fissile moderate hard to hard fissile splintery</li> <li>Occasionally slity</li> </ul>                |  |  |  |  |
|-----|-----------|--------|---------|--|--|--|--|--|
|     | Siltstone | 37-38% | 66-74%  | <ul> <li>Light grey to brownish grey</li> <li>Hard and quartzite carbonaceous, calcareous</li> </ul>   |  |  |  |  |
|     | Sandstone | 24-30% | 60-62%  | <ul> <li>Light grey</li> <li>Fine grain friable and slightly glauconitic</li> <li>Low porosity visual and faint crush cut</li> </ul>                       |  |  |  |  |
|     | Claystone | 34.5%  | 68%     | - Cream to light grey swell  |  |  |  |  |
| Kf7 | Shale     | 35-41% | 55-80%  | <ul> <li>Light greenish grey to medium grey</li> <li>Fissile moderate hard to hard fissile splintery</li> <li>Occasionally slity</li> </ul>                |  |  |  |  |
|     | Sandstone | 36-38% | 56%/78% | <ul> <li>Light grey</li> <li>very fine grain and slity at the base</li> <li>fairly good visual porosity(5338n and blocky(5484m)</li> </ul>                 |  |  |  |  |
|     | Siltstone | 35-38% | 56-79%  | <ul> <li>Light grey to brownish grey/light<br/>brow</li> <li>Hard and quartzite carbonaceous,<br/>calcareous</li> <li>Very fine grain sandstone</li> </ul> |  |  |  |  |

Table 7: Summaries of rock properties for DELTA-1 well

#### Final Year Project II

Further studies had been done in the different region which is in HONEY-1 well in Baram Delta at Miri Field. The data had been compiled in a table that shows below and a graph of thermal conductivity versus acoustic impedance had been made.

| Depth<br>interval(m) | gamma<br>ray(gr) | neutron<br>porosity<br>(Φn) | density<br>ρ,gm/cm3 | Vsh | Acoustic<br>Impedance(x10 <sup>2</sup> ) | Thermal<br>Conductivity | Thermal<br>Facies          |
|----------------------|------------------|-----------------------------|---------------------|-----|--|-------------------------|----------------------------|
| 2675                 | 40               | 25                          | 2.4                 | 41  | 91.2                                     | 3.22                    | 2                          |
| 2681                 | 59               | 26                          | 2.4                 | 71  | 96.7                                     | 2.54                    | 1                          |
| 2688                 | 62               | 24                          | 2.5                 | 76  | 98.8                                     | 2.47                    | 1                          |
| 2696                 | 43               | 22                          | 2.5                 | 45  | 102.5                                    | 3.68                    | 2                          |
| 2703                 | 65               | 24                          | 2.5                 | 81  | 100.4                                    | 2.37                    | 1                          |
| 2710                 | 60               | 24                          | 2.4                 | 73  | 97.3                                     | 2.51                    | 1                          |
| 2718                 | 36               | 23                          | 2.4                 | 34  | 98.9                                     | 2.95                    | 2                          |
| 2732                 | 54               | 30                          | 2.4                 | 64  | 97.3                                     | 2.67                    | 1                          |
| 2747                 | 61               | 25                          | 2.5                 | 75  | 100.6                                    | 2.47                    | 1                          |
| 2754                 | 43               | 20                          | 2.4                 | 45  | 99.3                                     | 3.92                    | 2                          |
| 2769                 | 62               | 23                          | 2.4                 | 76  | 89.2                                     | 2.46                    | 1                          |
| 2776                 | 71               | 26                          | 2.4                 | 91  | 92.5                                     | 2.21                    | 1                          |
| 2783                 | 31               | 19                          | 2.4                 | 26  | 95.1                                     | 3.27                    | 2                          |
| 2791                 | 23               | 21                          | 2.5                 | 13  | 100.7                                    | 3.50                    | 3                          |
| 2798                 | 22               | 22                          | 2.5                 | 12  | 96.5                                     | 3.43                    | 3                          |
| 2805                 | 56               | 25                          | 2.4                 | 66  | 85.8                                     | 2.64                    | 1.00                       |
| 2812                 | 35               | 23                          | 2.5                 | 32  | 96.7                                     | 2.98                    | 2                          |
| 2820                 | 31               | 26                          | 2.5                 | 27  | 98.5                                     | 2.94                    | 2                          |
| 2827                 | 44               | 20                          | 2.4                 | 47  | 97.8                                     | 3.94                    | 2                          |
| 2834                 | 48               | 19                          | 2.5                 | 53  | 101.6                                    | 4.17                    | 3                          |
| 2849                 | 24               | 20                          | 2.5                 | 15  | 105.8                                    | 3.53                    | 3                          |
| 2856                 | 35               | 21                          | 2.5                 | 32  | 100.5                                    | 3.06                    | 2<br>2<br>2<br>3<br>3<br>2 |
| 2864                 | 31               | 19                          | 2.5                 | 27  | 107.2                                    | 3.26                    | 2                          |
| 2871                 | 43               | 21                          | 2.5                 | 45  | 108.3                                    | 3.80                    | 2<br>2                     |
| 2878                 | 57               | 24                          | 2.5                 | 68  | 102.0                                    | 2.60                    | 1                          |
| 2885                 | 18               | 24                          | 2.5                 | 5   | 105.1                                    | 3.44                    | 5                          |
| 2893                 | 16               | 24                          | 2.5                 | 0   | 102.0                                    | 3.51                    | 5                          |
| 2900                 | 37               | 18                          | 2.5                 | 35  | 103.8                                    | 3.12                    | 2                          |
| 2907                 | 19               | 24                          | 2.5                 | 4   | 99.9                                     | 3.45                    | 4                          |
| 2915                 | 30               | 21                          | 2.5                 | 23  | 95.6                                     | 3.18                    | 2                          |
| 2929                 | 63               | 22                          | 2.4                 | 78  | 86.4                                     | 2.42                    | 1                          |
| 2944                 | 37               | 20                          | 2.4                 | 36  | 89.7                                     | 3.05                    | 2                          |
| 2951                 | 31               | 17                          | 2.5                 | 25  | 95.8                                     | 3.35                    | 2<br>2                     |
| 2958                 | 64               | 16                          | 2.5                 | 79  | 99.6                                     | 2.41                    | 1 1                        |

Table 8: HONEY-1 well data interpretation



#### Final Year Project II

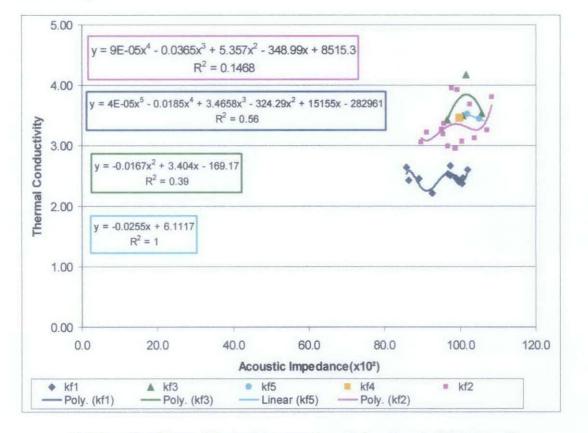


Fig.8 Crossplot of Thermal Conductivity versus Acoustic Impedance in HONEY-1 well

From the result above in HONEY-1 well, all the data are different form the DELTA-1 well data. The value of acoustic impedance in HONEY-1 well is different than the value acoustic impedance in DELTA-1 well. The value is about 2 times higher than the value acoustic impedance in DELTA-1 well. This is because of the different of location of field and type of the field that had been explained in the background of the wells. Moreover, the acoustic impedance and thermal conductivity in HONEY-1 well shows that it is difficult to make a relationship by facies compare to DELTA-1 well.

For the facies in this well, all the point at each depth interval was sandstone and a few of shale. Therefore, the thermal facies in this well is kf1, kf2, k3 and a few of kf4 and kf5.

Final Year Project II

#### **CHAPTER 5: CONCLUSION**

The quantitative database was developed through the analysis of crossplots between thermal conductivity and acoustic impedance derived essentially, from well logs. Although this project uses only two wells, the database that has been developed will be useful for showing the empirical relationship between the acoustic impedance and thermal conductivity.

The database was compiled based on the type of thermal facies, the rock properties such as neutron porosity, gamma ray, density, and volume of shale, formation temperature; velocity and the depth intervals. From these factors, we can see the  $R^2$  value indicate a good trend or not. Hence, the empirical relationships of thermal conductivity in well DELTA have better trends than those of well HONEY. From the equations developed, we can identify the thermal properties of other wells from seismic impedance data. This project shows that the database could be developed from the crossplots method applied in developing empirical equations relating thermal conductivity to acoustic impedance.

The outcome of this project could be the database and the equation developed from the crossplot. The techniques has been developed which use to identify the reservoir characteristic according to environment of deposition and thermal facies. We can predict the thermal conductivity by knowing the seismic data or acoustic impedance. In order to increase the efficiency and the accuracy of the result, this project could be further studied using different wells from different basins.

Final Year Project II

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## **CHAPTER 7: APPENDICES**

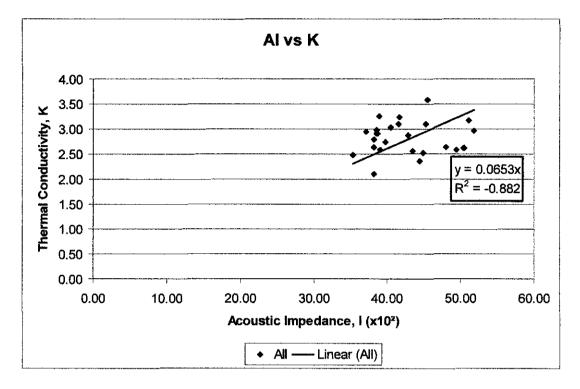


Fig 9: Crossplot of Thermal Conductivity versus Acoustic Impedance in DELTA-1 well without consider facies

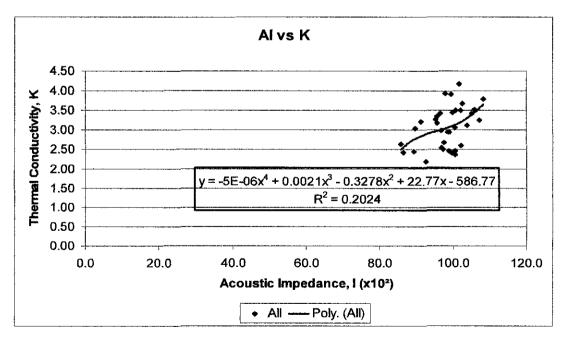


Fig 10: Crossplot of Thermal Conductivity versus Acoustic Impedance in HONEY-1 well without consider facies

Final Year Project II

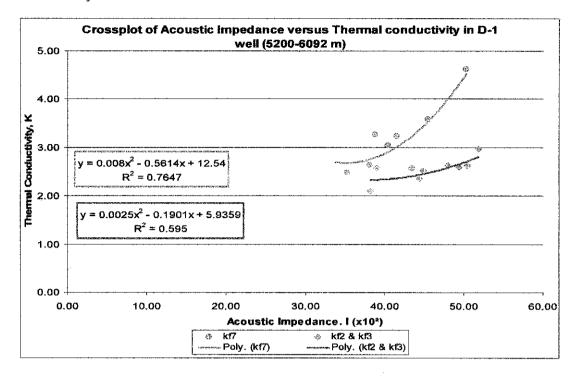


Fig 11: Crossplot of Thermal Conductivity versus Acoustic Impedance in DELTA-1 well for sand only

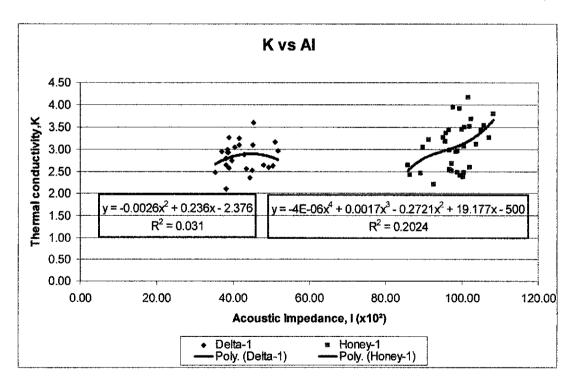


Fig 12: Crossplot of Thermal Conductivity versus Acoustic Impedance in DELTA-1 well and HONEY-1 well without consider facies