

**ESTIMATION & COMPARISON OF HEAT TRANSFER COEFFICIENT OF
CRUDE OIL USING VARIOUS CORRELATIONS**

by

Noor Zaheera Binti Noorizam

A project dissertation submitted to the

Chemical Engineering Programme

Universiti Teknologi PETRONAS

In partial fulfillment of the requirement for the

BACHELOR OF ENGINEERING (Hons)

(CHEMICAL ENGINEERING)

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Universiti Teknologi PETRONAS

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CERTIFICATION OF APPROVAL

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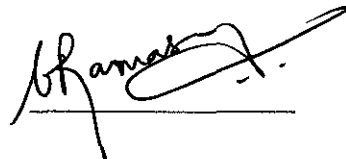
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Approved by,

A handwritten signature in black ink, appearing to read 'M. Ramasamy', is written over a horizontal line.

(AP Dr. M. Ramasamy)

UNIVERSITI TEKNOLOGI PETRONAS

TRONOH, PERAK

September 2011

CERTIFICATION OF ORIGINALITY

This is to certify that I am responsible for the work submitted in this project, that the original work is my own except as specified in the references and acknowledgements, and that the original work contained herein have not been undertaken or done by unspecified sources or persons.



NOOR ZAHEERA BINTI NOORIZAM

ABSTRACT

Heat transfer may occur by any one or more of the three basic mechanisms of heat transfer; conduction, convection and radiation but in process industries, the transfer of heat between two fluids is generally done via convective heat transfer.

For example, in oil refinery plant, the most common heat transfer phenomenon is the crude oil/water interchange via heat exchanger.

Calculating and estimating the heat transfer coefficients, h of crude oil using various correlations will able us to see the variations of its value and we can compare to the reference value that is being used in the industry to see which one of the correlations is suitable to be used for the crude oil system.

By having the knowledge of heat transfer coefficient of crude oil, the design of any heat exchangers will be simplified. It also help in developing better flow process control that will then help to reduce and conserve energy.

NOMENCLATURE

| | |
|-----------------|---|
| ρ_1 | final density (kg/m^3) |
| ρ_0 | initial density (kg/m^3) |
| β | volumetric temperature expansion coefficient ($\text{m}^3/\text{m}^3\text{ }^\circ\text{C}$) |
| t_1 | final temperature ($^\circ\text{C}$) |
| μ | viscosity of liquid at t degree Celsius in poise |
| μ_0 | viscosity of the fluid at 0° Celsius in poise |
| a, b, c, d (Cp) | coefficients from Perry's Chemical Engineers' Handbook |
| a, b (k) | empirical constant |

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CHAPTER 1

INTRODUCTION

1.1 Background of Study

Crude oil or commonly known as petroleum, a liquid found within the Earth is consist of hydrocarbons, organic compounds and small amount of metal. Hydrocarbons are the primary component of crude oil with the composition that can vary from 50% to 97%, depending on the type of crude oil and how it is extracted. Organic compound like nitrogen, oxygen and sulfur make-up between 6% to 10% of crude oil while metals such as copper, nickel, vanadium and iron account for less than 1% of the total composition.

Malaysian oilfield has the lightest and the sweetest of the main types of crude oil with the physical properties as shown below, [10];

Table 1: Crude Oil Properties

| CRUDE OIL | |
|--------------------------------------|--------|
| Density at 15°C (g/cm ³) | 0.8036 |
| Viscosity at 40°C (cSt) | 3.831 |
| API Gravity | 44.5 |

Heat transfer may occur by any one or more of the three basic mechanism of heat transfer: conduction, convection and radiation [1].

Convection heat transfer takes place whenever a fluid is in contact with a solid surface that is at a different temperature than the fluid. If the fluid is moving past the solid surface because of an external driving force, like pump or blower, then it is called forced convection. If a fluid motion is due to density differences caused by temperature variation in the fluid, then it is called natural or free convection.

k is the thermal conductivity of the fluid (W/m.K)

D is characteristic length parameter such as diameter for flow through a pipe (m)

V is characteristic velocity (m/s)

ρ is the density of the fluids (kg/m³)

μ is the viscosity of the fluid (N-s/m²)

C_p is heat capacity of the fluid (kJ/kg.K)

1.2 Problem Statement

In an oil refinery plant, the transfer of heat between two fluids is generally done in heat exchangers via convective heat transfer. For example, heat exchangers are used for crude oil/water interchange. The knowledge on heat transfer coefficient of crude oil will help in designing and calculations for heat exchanger design. It also help in developing better flow process control that will then help to reduce and conserve energy.

1.3 Objectives

- To estimate & calculate the properties of crude oil (density, heat capacity, viscosity and thermal conductivity) in function of temperature.
- To estimate & calculate heat transfer coefficients of crude oil using various correlations collected and compares the result between the different correlations used and data from experiment.

1.4 Scope of Study

The scope for this project has been scrutinized to estimate the heat transfer coefficient of crude oil via forced convection in turbulent flows inside a pipe. The physical properties of crude oil that vary with temperature and will effect the calculation of heat transfer coefficients that has been identified are thermal conductivity (k), density (ρ), viscosity (μ) and specific heat capacity (C_p).

1.5 Relevancy of Project

With the continued increased in design complexity and modernization of oil refinery plant, the knowledge of heat transfer coefficient is necessary for heat transfer design and calculation. Heat transfer coefficient is also critical for designing and developing better flow process control in resulting in reduced energy consumption and enhanced energy conservation.

1.6 Feasibility of Project

This project is fully computer based. In the time given, the project could be done. This project can be done within 4 months given that everything goes fine. The objective can be achieved if the procedures are closely followed.

CHAPTER 2

LITERATURE REVIEW

2.1 Physical Properties of Crude Oil

One of the factors that will effect the calculation of heat transfer coefficients is the physical properties of the fluid itself. The physical properties of crude oil that will vary with temperature are density, viscosity, specific heat capacity and thermal conductivity. Different temperature will give different value of these physical properties that will then effect the calculation of heat transfer coefficients through Reynolds and Prandtl numbers.

2.1.1. Density

The density changes with temperature as the molecules moves around faster. That pushes them slightly farther apart, making the density go down.

When temperature is changed, the density of a fluid can be expressed as [3],

$$\rho_1 = \rho_0 / (1 + \beta (t_1 - t_0)) \quad (5)$$

2.1.2 Viscosity

Viscosity is the property of the fluid that resists the flow of the fluids. The viscosity behavior of most crude oil is very sensitive to temperature changes. As temperature increases, the viscosity of crude oil decreases [10].

When the temperature of fluid is changed, the viscosity of the fluid can be expressed [3];

$$\mu = \mu_0 / (1 + \alpha t + \beta t) \quad (6)$$

2.1.3 Specific Heat Capacity

Heat capacity is physical properties that may be expressed in any units of energy per unit amount per unit temperature interval. Heat capacity is a function of temperature and frequently expressed in polynomial form [4],

$$C_p = a + bT + cT^2 + dT^3 \quad (7)$$

2.1.4 Thermal Conductivity

Thermal conductivity of liquids varies moderately with temperature and often can be expressed as a linear variation [1],

$$k = a + bT \quad (8)$$

2.2 Heat Transfer Coefficients Correlation

There are several correlations available for calculation of the convective heat transfer coefficient for turbulent flow inside a circular tube.

2.2.1 Classic Correlation – Dittus – Boelter Equation (1930) [2]

The exponent on the Prandtl number depends on the service (either heating or cooling). Different values are needed because of the variation of viscosity with temperature [5].

$$\begin{aligned} \text{Nu} &= 0.0243 \text{Re}^{0.8} \text{Pr}^{0.4}, \text{ heating of fluid } (T_{\text{wall}} > T_{\text{fluid}}) \\ \text{Nu} &= 0.0265 \text{Re}^{0.8} \text{Pr}^{0.3}, \text{ cooling of fluid } (T_{\text{wall}} < T_{\text{fluid}}) \end{aligned} \quad (9)$$

This equation is recommended only for rather small temperature differences between bulk fluid and pipe wall. It is valid for smooth pipe and for,

$$0.6 \leq \text{Pr} \leq 160$$

$$\text{Re} \geq 10000$$

$$L/D \geq 10$$

2.2.2. Sieder - Tate (1936) [2]

This equation can accommodate larger temperature differences,

$$Nu = 0.023 Re^{0.8} Pr^{1/3} (\mu_b/\mu_w)^{0.14} \quad (10)$$

This equation is valid for smooth pipes and for,

$$0.7 \leq Pr \leq 16700$$

$$Re \geq 10000$$

$$L/D \geq 10$$

2.2.3 Pethukov, Gnielinski

This correlation has been based on extensive experimental data and on a better understanding of turbulent flow [6].

$$Nu_0 = \frac{\frac{\xi}{8}}{1 + 12.7 \sqrt{\frac{\xi}{8}} (Pr^{2/3})} (Re - 1000) Pr \times \left[1 + \left(\frac{D}{L} \right)^{2/3} \right]$$
$$\xi = \frac{1}{(1.82 \log Re - 1.64)^2} \quad (11)$$

This correlation is valid for both smooth and rough tubes with

$$0.5 \leq Pr \leq 2000$$

$$2300 < Re < 5 \times 10^6$$

2.2.4 Colburn Equation

After simplified from Chilton-Colburn equation, the final equation is [7],

$$Nu = 0.023 Re^{0.8} Pr^{1/3}$$

CHAPTER 3 METHODOLOGY

3.1 Research Methodology

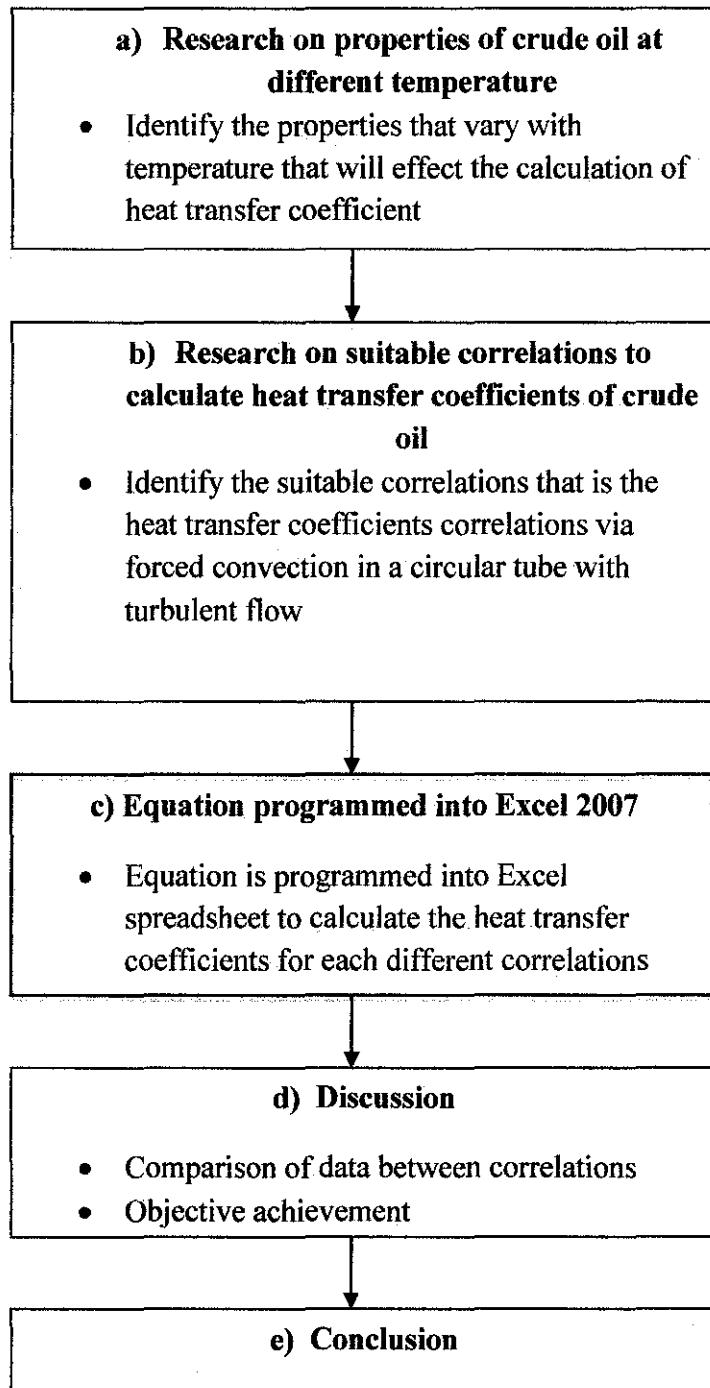


Figure 1: Flow Chart for FYP Methodology

3.2 Project Activities

For this project, the main activities that will be done are:

- Literature review – gathering information, reading journals and finding references.
- Correlations – gathering relevant correlations for this project
 - The correlations chosen must not be specially for certain fluid only
- Estimation & Calculations
 - Find the relationship for properties of crude oil (thermal conductivity, density, viscosity, and specific heat capacity) with respect to temperature through simulation of PETROSIM with temperature range from 0°C to 300°C.
 - Then, graph is plotted (ex; Temperature vs Density) to find the related equation between the physical properties and temperature.
 - Heat transfer coefficients for crude oil is calculated based on the correlations gathered (Dittus-Boelter, Sieder-Tate, Pethukov, Gnielinski & Colburn) at reference heat transfer coefficient data.

Table 2: Reference Heat Transfer Coefficient Data

| Heat Exchanger | Temperature (°C) | Velocity (m/s) | Heat Transfer Coefficient (W/m ² .K) |
|----------------|------------------|----------------|---|
| E-01 | 58 | 1.79 | 1506 |
| E-02 | 86 | 1.62 | 1567 |
| E-03 | 108 | 1.06 | 1194 |
| E-05 | 138.5 | 0.78 | 996 |
| E-06 | 149 | 2.12 | 2241 |
| E-07 | 154 | 1.7 | 1903 |
| E-09 | 185.5 | 1.35 | 1769 |
| E-10 | 204 | 2.89 | 3442 |

- Analysis of Data
 - The value of transfer coefficients calculated using the four correlations gathered is compared with the reference data.

- Graph heat transfer coefficient, h_{calc} vs. h_{ref} is plotted and one linear line is plotted to see the nearness of value of every data of heat transfer coefficient of crude oil (calculated h_{calc}) to the heat transfer coefficient of crude oil (reference, h_{ref})

3.3 Gantt Chart

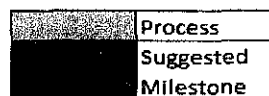
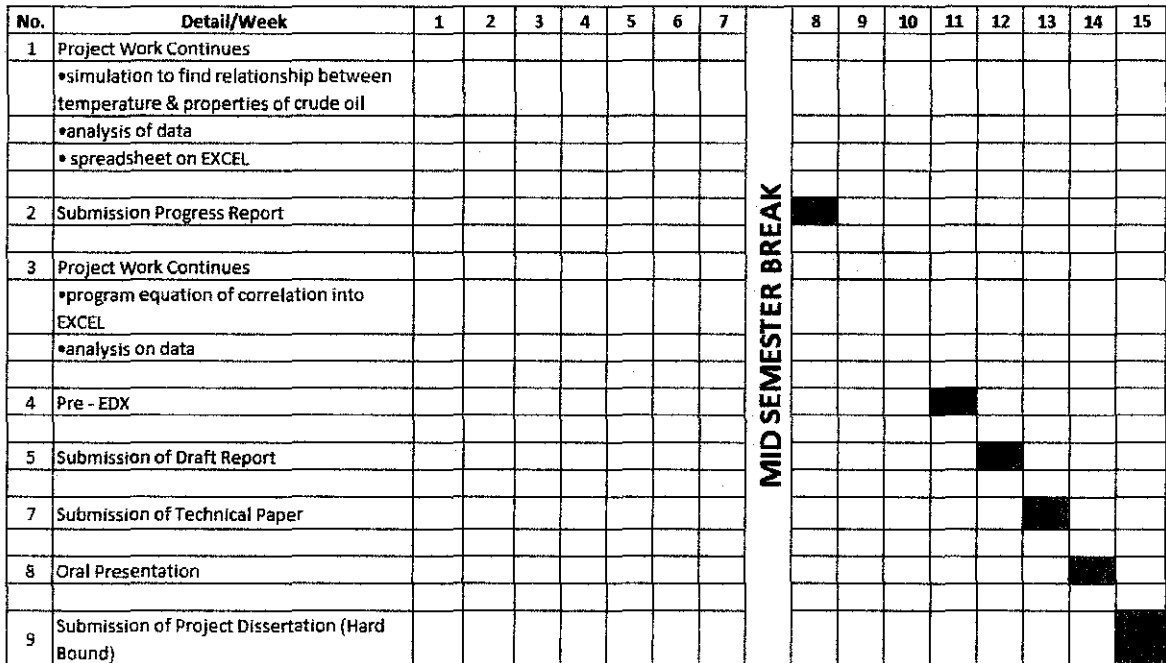


Figure 2: Gantt chart for FYP II

3.4 Tools & Equipment

In this project, computers are the major tool used. Simulation is done by PETROSIM software and calculations are done using Microsoft Excel.

CHAPTER 4 RESULT & DISCUSSION

4.1 Estimation & Calculation of Properties of Crude Oil with respect to Temperature

INSTRUCTION: insert value in blue box, spreadsheet calculate in yellow box

| | |
|--|--|
| <p><u>Calculation of Density</u></p> $y = -0.00118x^2 - 0.618x + 811.3$ <p>y = density x = temperature</p> <p>Enter Temperature 200</p> <p>Density 636.1211 kg/m³</p> <p><u>Calculation of Thermal Conductivity</u></p> $y = 2.19E-08x^2 - 1.16E-05x^2 + 1.30E-03x^2 - 2.91E-01x + 137$ <p>y = thermal conductivity x = temperature</p> <p>Enter Temperature 200</p> <p>Thermal Conductivity 0.071185 W/m.K</p> | <p><u>Calculation of Viscosity</u></p> $y = -8.85E-12x^5 + 8.12E-09x^4 - 2.90E-06x^3 + 5.16E-04x^2 - 4.98E-02x + 2.60$ <p>y = viscosity x = temperature</p> <p>Enter Temperature 200</p> <p>Viscosity 0.000231 Pa.s</p> <p><u>Calculation of Specific Heat Capacity</u></p> $y = -2.02E-06x^2 + 0.00444x + 1.94$ <p>y = specific heat capacity x = temperature</p> <p>Enter Temperature 200</p> <p>Specific Heat Capacity 2.761696 kJ/Kg.K</p> |
|--|--|

Figure 3: Spreadsheet to calculate the properties of crude oil

Figure 3 above is the spreadsheet that calculates every physical properties of crude oil (thermal conductivity, density, viscosity & specific heat capacity) with respect to temperature. The relationship between properties of crude oil to temperature is determined through the simulation of crude oil through PETROSIM software. The value obtained from the PETROSIM simulation is attached in Appendices section.

The graph is plotted between temperature and each properties of crude oil for range of temperature between 0°C to 300°C, based on the result from PETROSIM simulation to find the equation that relates them and simplified the general correlation shown, to an equation that represents the actual result.

4.1 Density

In the PETROSIM simulation, the relationship between temperature and density is shown in the graph below.

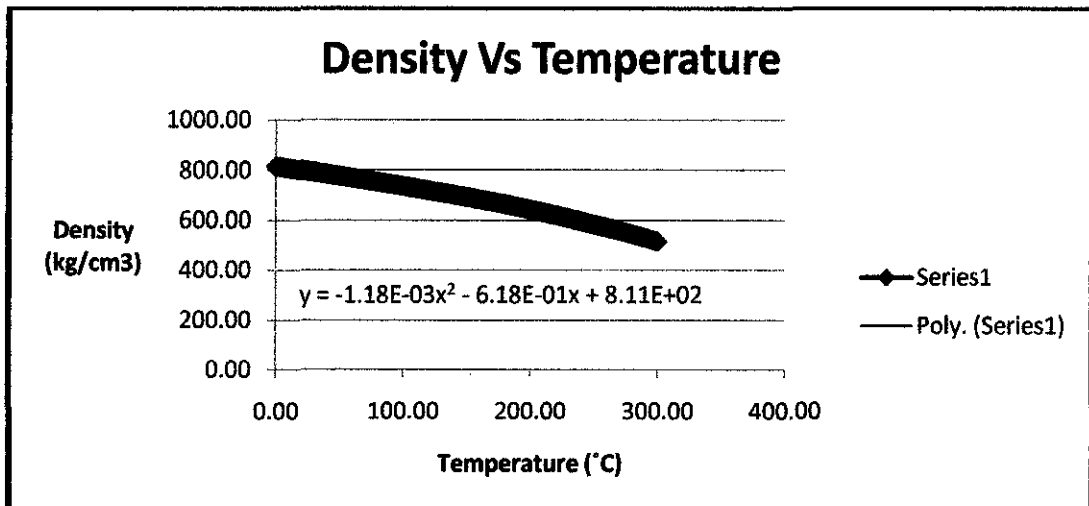


Figure 4: Graph of Density vs. Temperature from PETROSIM simulation

Based on the graph, the density of crude oil show a linear relationship to temperature that is with the increase of temperature, the density of crude oil decrease thus proving the statement above and the general correlation has been simplified to the equation below,

$$\rho = -1.18 \times 10^{-3} T^2 - 0.618T + 811 \quad (13)$$

4.2 Viscosity

In the PETROSIM simulation, the relationship between temperature and viscosity is shown in the graph below.

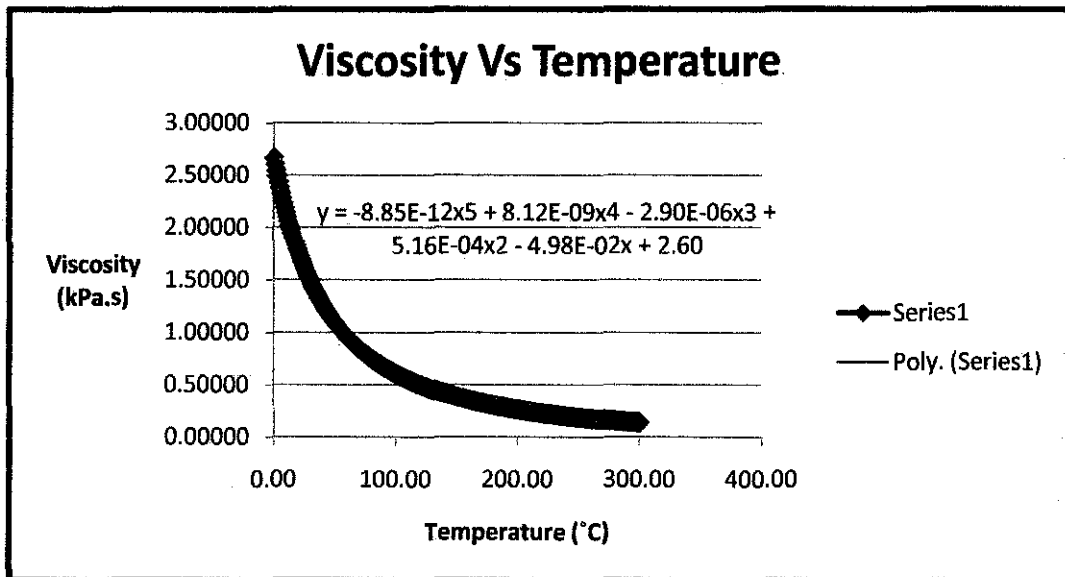


Figure 5: Graph of Viscosity Vs Temperature from PETROSIM simulation

Based on the graph, with the increase of temperature, the viscosity of crude oil will decrease and the general correlation has been simplified to the equation below,

$$\mu = -8.85 \times 10^{-12}T^5 + 8.12 \times 10^{-9}T^4 - 2.9 \times 10^{-6}T^3 + 5.16 \times 10^{-4}T^2 - 0.0498T + 2.6 \quad (14)$$

4.3 Specific Heat Capacity

In the PETROSIM simulation, the relationship between temperature and specific heat capacity is shown in the graph below.

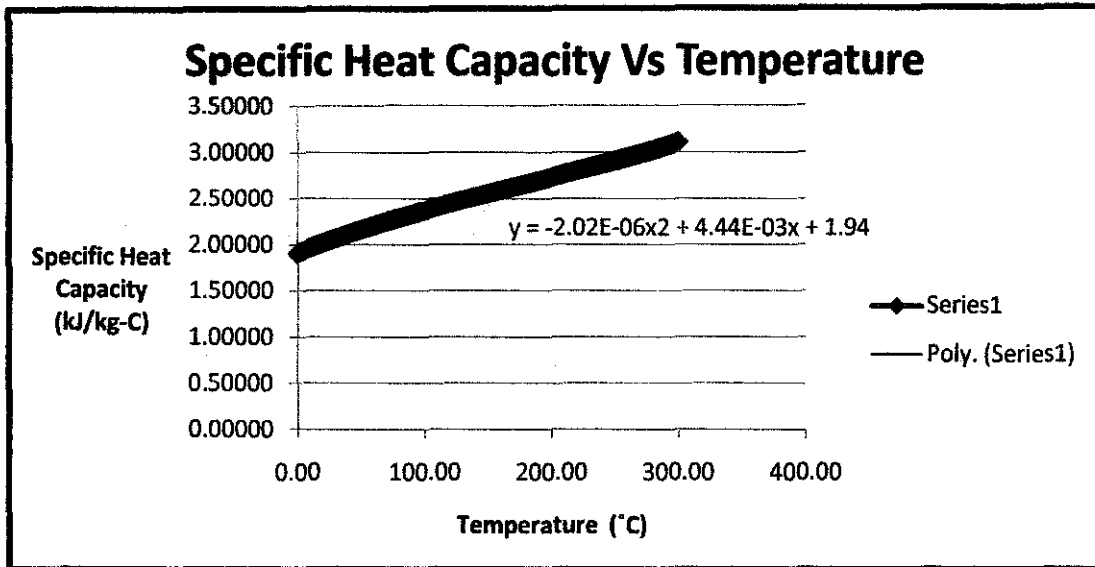


Figure 6: Graph of Specific Heat Capacity Vs Temperature from PETROSIM simulation

Based on the graph, with the increase of temperature, the specific heat capacity of crude oil will decrease and the general correlation has been simplified to the equation below,

$$C_p = -2.02 \times 10^{-6}T^2 + 0.00444T + 1.94 \quad (15)$$

4.3 Thermal Conductivity

In the PETROSIM simulation, the relationship between temperature and thermal conductivity is shown in the graph below.

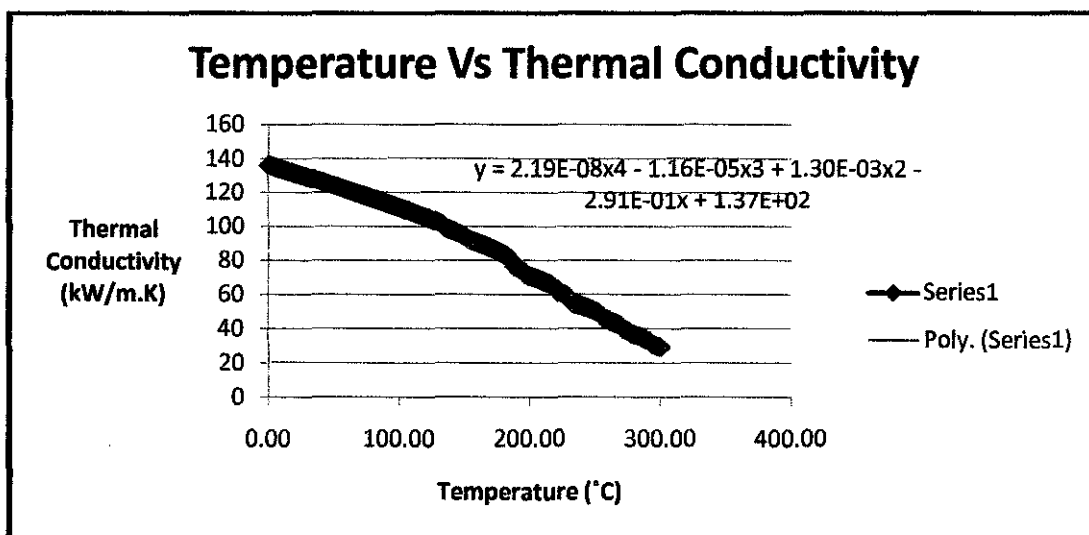


Figure 7: Graph of Thermal Conductivity Vs Temperature from PETROSIM simulation

Based on the graph, thermal conductivity of crude oil show a linear relationship to temperature that is with the increase of temperature, the thermal conductivity of crude oil decrease and the general correlation has been simplified to the equation below,

$$k = 2.19 \times 10^{-8}T^4 - 1.16 \times 10^{-5}T^3 + 0.013T^2 - 0.291T + 137 \quad (16)$$

4.2 Estimation & Calculation of Heat Transfer Coefficient

INSTRUCTION: Insert value in blue box, spreadsheet calculate in yellow box

| Inputs | | Calculations | |
|-------------------------------|---|--|---|
| Fluid Temp., T_b | <input type="text"/> °C | Reynolds No., Re | <input type="text"/> Moody Factor, f <input type="text"/> |
| Pipe diam., D | <input type="text"/> inch <input type="text"/> m | Prandtl No., Pr | <input type="text"/> |
| Average Vel., V | <input type="text"/> m/s | | |
| Fluid Density, ρ | <input type="text"/> kg/m ³ | Correlation #1: Dittus-Boelter (Classic) | |
| Fluid Viscosity, μ | <input type="text"/> Pa.s | $T_{wall} > T_{fluid}$ Nu = <input type="text"/> | Correlation #2: Sieder-Tate |
| Fluid Sp. Heat, Cp | <input type="text"/> J/kg.K | h = <input type="text"/> | Nu = <input type="text"/> |
| Fluid Thermal Conductivity, k | <input type="text"/> W/m.K | $T_{wall} < T_{fluid}$ Nu = <input type="text"/> | Correlation #3: Pethukov & Geilinski |
| Pipe Length, L | <input type="text"/> m | h = <input type="text"/> | Nu = <input type="text"/> |
| Wall Temp., T_w | <input type="text"/> °C | | h = <input type="text"/> |
| | | | Correlation #4: Colburn |
| | | | Nu = <input type="text"/> |
| | | | h = <input type="text"/> |

Figure 8: Spreadsheet to calculate heat transfer coefficients for each correlation

The value of heat transfer coefficient of crude oil based on different correlations is calculated by Microsoft Excel in a spreadsheet shown above.

In the correlations of the heat transfer coefficients, there are few properties that need to be specified which is, the length of tubes (L) and diameter of tube (D). The typical length of tube being used is 20 feet (6.1m) [8] with diameter of 3/4" [9].

The calculation is done by setting the constant temperature and velocity for both reference data and calculated data. The values obtained from these correlations are then being compared to the reference data and the result is shown in the table below;

Table 3: Values of Heat Transfer Coefficient (h_{ref} and h_{calc})

| Temperature (°C) | Velocity (m/s) | Reference Heat Transfer Coefficient, $h_{ref}(W/m^2.K)$ | Calculated Heat Transfer Coefficient, $h_{calc}(W/m^2.K)$ | | | |
|------------------|----------------|---|---|-----------------------------|--------------------------------------|-------------------------|
| | | | Correlation 1 (Dittus-Boelter) | Correlation 2 (Sieder-Tate) | Correlation 3 (Pethukov, Gnielinski) | Correlation 4 (Colburn) |
| 58 | 1.79 | 1506 | 1698.601 | 1356.509 | 6402.686 | 1327.225 |
| 86 | 1.62 | 1567 | 1725.015 | 1372.152 | 5993.127 | 1368.083 |
| 108 | 1.06 | 1194 | 1283.272 | 1035.419 | 4239.345 | 1025.386 |
| 138.5 | 0.78 | 996 | 1036.632 | 832.006 | 3267.409 | 834.406 |
| 149 | 2.12 | 2241 | 2322.192 | 1873.307 | 7343.314 | 1873.478 |
| 154 | 1.7 | 1903 | 1951.268 | 1576.080 | 6109.059 | 1575.955 |
| 185.5 | 1.35 | 1769 | 1632.853 | 1322.834 | 4891.746 | 1327.745 |
| 204 | 2.89 | 3442 | 2968.540 | 2417.560 | 8857.137 | 2420.726 |

The value of the reference heat transfer coefficient of crude oil is plotted against the value of calculated heat transfer coefficient of crude oil for each correlation. A linear line is also plotted to see the deviation between the reference heat transfer coefficient and the calculated heat transfer coefficient.

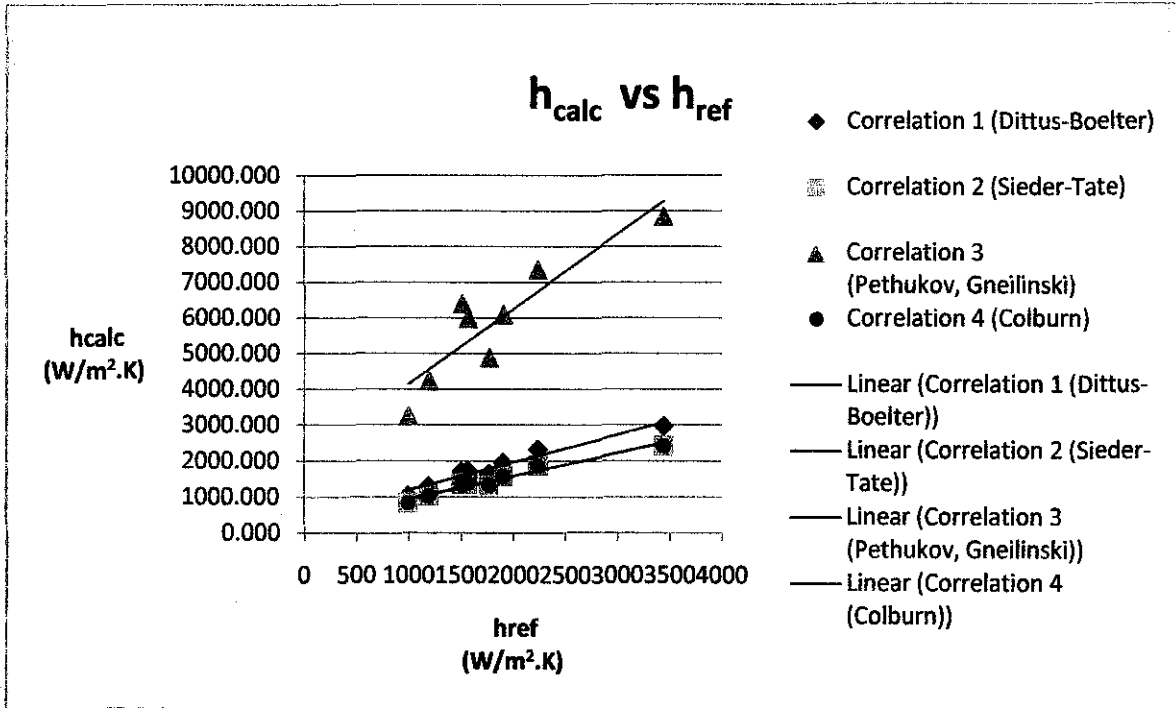


Figure 9: Graph h_{calc} Vs h_{ref}

For Correlation 1 (Dittus-Boelter), each value of calculated heat transfer coefficient does not deviate too much from the reference heat transfer coefficient. Each data falls on the linear line, showing that the calculated heat transfer coefficient gives almost the same value as the reference heat transfer coefficient value. The same goes for Correlation 2 (Sieder-Tate) and Correlation 4 (Colburn). However, for Correlation 3 (Pethukov, Gneilinski), the value deviates too much, almost all data did not falls on the linear line, proving the calculated heat transfer coefficient gives totally different value from reference heat transfer coefficient.

The table below shows the deviation between the reference heat transfer coefficients and the value from the calculated correlations.

Table 4: Deviation Percentage between h_{ref} and h_{cal}

| Deviation (%) | | | | |
|---------------|---------------------------------------|------------------------------------|---|----------------------------|
| | Correlation 1 (Dittus- Boelter) | Correlation 2 (Sieder- Tate) | Correlation 3 (Pethukov, Gnielinski) | Correlation 4 (Colburn) |
| | 12.789 | 9.926 | 325.145 | 11.871 |
| | 10.084 | 12.434 | 282.459 | 12.694 |
| | 7.477 | 13.281 | 255.054 | 14.122 |
| | 4.080 | 16.465 | 228.053 | 16.224 |
| | 3.623 | 16.408 | 227.680 | 16.400 |
| | 2.536 | 17.179 | 221.023 | 17.186 |
| | 7.696 | 25.221 | 176.526 | 24.944 |
| | 13.755 | 29.763 | 157.325 | 29.671 |
| MAD = | 7.755 | 17.585 | 234.158 | 17.889 |

Based on the table above, the calculated heat transfer coefficient for Correlation 1 (Dittus-Boelter) deviated from the reference data by a mean of 7.755%. This overall mean average deviation of 7.755% represents an excellent match between the calculated and reference heat transfer coefficient of crude oil and is well within an acceptable limit of reference error of 10%.

However, for Correlation 2 (Sieder-Tate), Correlation 3 (Pethukov, Gnielinski) and Correlation 4 (Colburn), the calculated heat transfer coefficient deviated from the reference data by a mean of 17.585%, 234.158%, and 17.889% each which is not within the acceptable limit of reference error of 10%.

This proved that Correlation 1 (Dittus-Boelter) is suitable to be used for heat transfer coefficient calculation for TAPIS crude oil system.

CHAPTER 5

CONCLUSION

The project is to calculate the heat transfer coefficient of crude oil of various correlations but in order to calculate this; few factors must be taken into consideration. Between the factors that will affect the calculation of heat transfer coefficients are the type and velocity of the flow, temperature difference, geometry of the system and also the physical properties of crude oil. As the physical properties of crude oil are changing with temperature, it is required to find its relationship before proceeding in calculating heat transfer coefficients for crude oil.

It is the first objective of this project to estimate and calculate the properties of crude oil (density, heat capacity, viscosity, and thermal conductivity) with respect to temperature. In order to see this relationship, a simulation oil crude oil is done through software PETROSIM. 400 data is gathered and each graph of these properties is plotted against temperature.

The density, thermal conductivity and viscosity of crude oil are decreasing with the increase of temperature while the specific heat capacity of crude oil is increasing. The result has been shown in Chapter 4.

Heat transfer coefficient is calculated for each correlation and the value calculated is being compared to the reference heat transfer coefficient data. It is shown that Correlation 1 (Dittus-Boelter Equation) can be used as the correlation for heat transfer coefficient calculation for crude oil system as it has the lowest mean average deviation, that is 7.755% from the reference value.

Correlation 2, 3 and 4 is not suitable as the value calculated using these correlations deviates too much from the reference data.

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APPENDICES

Table 1: Specification of crude oil

| Object | Property | LiqVol Fractions | MB/d (*From Data) |
|---------------|------------------|-------------------------|--------------------------|
| Unit | Unit | | |
| Blend | TAPIS_44_8_C_TAP | 1.0000 | 100.00 |
| Blend | MASA03 | 0.0000 | 0.00 |
| Blend | MIRI_LT_06 | 0.0000 | 0.00 |
| Blend | BINTULU_CRUDE | 0.0000 | 0.00 |
| Blend | ARAB_LT_06 | 0.0000 | 0.00 |
| Blend | CENDOR | 0.0000 | 0.00 |
| Blend | BINTUL_COND_59_6 | 0.0000 | 0.00 |
| Blend | MURBAN_39_3 | 0.0000 | 0.00 |
| Blend | COSSACK_47_7 | 0.0000 | 0.00 |
| Blend | BKEKWA | 0.0000 | 0.00 |
| Blend | KIKEH | 0.0000 | 0.00 |
| Blend | ANGSI05 | 0.0000 | 0.00 |
| Blend | DULANG_37_6 | 0.0000 | 0.00 |
| Total | | 1.00 | 100.00 |

Table 2: Data gathered from PETROSIM Simulation

| Temperature | Mass Density | Thermal Conductivity | Viscosity (Dynamic) | Mass Heat Capacity |
|--------------------|-------------------------|-----------------------------|----------------------------|---------------------------|
| | <i>kg/m³</i> | <i>W/m-K</i> | <i>Pa-s</i> | <i>kJ/kg-C</i> |
| 0.00 | 815.47 | 0.13647 | 0.00266982 | 1.90823 |
| 1.00 | 814.70 | 0.13623 | 0.00260867 | 1.91382 |
| 2.00 | 813.93 | 0.13599 | 0.00254965 | 1.91939 |
| 3.00 | 813.15 | 0.13575 | 0.00249267 | 1.92493 |
| 4.00 | 812.38 | 0.13551 | 0.00243765 | 1.93045 |
| 5.00 | 811.61 | 0.13527 | 0.00238448 | 1.93594 |
| 6.00 | 810.84 | 0.13503 | 0.00233310 | 1.94141 |
| 7.00 | 810.06 | 0.13479 | 0.00228342 | 1.94686 |
| 8.00 | 809.29 | 0.13454 | 0.00223538 | 1.95228 |
| 9.00 | 808.52 | 0.13430 | 0.00218890 | 1.95768 |
| 10.00 | 807.74 | 0.13406 | 0.00214391 | 1.96306 |
| 11.00 | 806.97 | 0.13382 | 0.00210037 | 1.96841 |
| 12.00 | 806.19 | 0.13358 | 0.00205820 | 1.97374 |
| 13.00 | 805.42 | 0.13333 | 0.00201734 | 1.97905 |
| 14.00 | 804.64 | 0.13309 | 0.00197776 | 1.98433 |
| 15.00 | 803.86 | 0.13285 | 0.00193939 | 1.98959 |
| 16.00 | 803.09 | 0.13261 | 0.00190219 | 1.99483 |
| 17.00 | 802.31 | 0.13236 | 0.00186611 | 2.00004 |
| 18.00 | 801.53 | 0.13212 | 0.00183111 | 2.00523 |

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|-------|--------|---------|------------|---------|
| 19.00 | 800.76 | 0.13188 | 0.00179715 | 2.01040 |
| 20.00 | 799.98 | 0.13164 | 0.00176418 | 2.01555 |
| 21.00 | 799.20 | 0.13139 | 0.00173217 | 2.02067 |
| 22.00 | 798.42 | 0.13115 | 0.00170108 | 2.02578 |
| 23.00 | 797.64 | 0.13090 | 0.00167088 | 2.03086 |
| 24.00 | 796.86 | 0.13066 | 0.00164153 | 2.03592 |
| 25.00 | 796.08 | 0.13042 | 0.00161301 | 2.04095 |
| 26.00 | 795.30 | 0.13017 | 0.00158528 | 2.04597 |
| 27.00 | 794.52 | 0.12993 | 0.00155785 | 2.05096 |
| 28.00 | 793.74 | 0.12968 | 0.00153154 | 2.05593 |
| 29.00 | 792.96 | 0.12944 | 0.00150594 | 2.06088 |
| 30.00 | 792.17 | 0.12919 | 0.00148102 | 2.06581 |
| 31.00 | 791.39 | 0.12895 | 0.00145675 | 2.07072 |
| 32.00 | 790.61 | 0.12870 | 0.00143311 | 2.07561 |
| 33.00 | 789.82 | 0.12845 | 0.00141008 | 2.08048 |
| 34.00 | 789.04 | 0.12821 | 0.00138764 | 2.08532 |
| 35.00 | 788.26 | 0.12796 | 0.00136576 | 2.09015 |
| 36.00 | 787.47 | 0.12772 | 0.00134443 | 2.09496 |
| 37.00 | 786.68 | 0.12747 | 0.00132362 | 2.09975 |
| 38.00 | 785.90 | 0.12723 | 0.00130333 | 2.10451 |
| 39.00 | 785.11 | 0.12698 | 0.00128353 | 2.10926 |
| 40.00 | 784.32 | 0.12673 | 0.00126420 | 2.11399 |
| 41.00 | 783.53 | 0.12648 | 0.00124534 | 2.11870 |
| 42.00 | 782.75 | 0.12624 | 0.00122692 | 2.12339 |
| 43.00 | 781.96 | 0.12599 | 0.00120893 | 2.12806 |
| 44.00 | 781.17 | 0.12574 | 0.00119135 | 2.13272 |
| 45.00 | 780.38 | 0.12549 | 0.00117419 | 2.13735 |
| 46.00 | 779.58 | 0.12524 | 0.00115741 | 2.14197 |
| 47.00 | 778.79 | 0.12500 | 0.00114101 | 2.14657 |
| 48.00 | 778.00 | 0.12475 | 0.00112497 | 2.15115 |
| 49.00 | 777.21 | 0.12450 | 0.00110929 | 2.15571 |
| 50.00 | 776.41 | 0.12425 | 0.00109387 | 2.16026 |
| 51.00 | 775.62 | 0.12400 | 0.00107896 | 2.16479 |
| 52.00 | 774.82 | 0.12374 | 0.00106428 | 2.16930 |
| 53.00 | 774.03 | 0.12349 | 0.00104991 | 2.17379 |
| 54.00 | 773.23 | 0.12324 | 0.00103585 | 2.17827 |
| 55.00 | 772.44 | 0.12299 | 0.00102209 | 2.18273 |
| 56.00 | 771.64 | 0.12274 | 0.00100861 | 2.18718 |
| 57.00 | 770.84 | 0.12248 | 0.00099541 | 2.19161 |
| 58.00 | 770.04 | 0.12223 | 0.00098248 | 2.19602 |
| 59.00 | 769.24 | 0.12198 | 0.00096981 | 2.20042 |
| 60.00 | 768.44 | 0.12172 | 0.00095740 | 2.20480 |
| 61.00 | 767.64 | 0.12147 | 0.00094523 | 2.20917 |
| 62.00 | 766.84 | 0.12121 | 0.00093331 | 2.21352 |

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|--------|--------|---------|------------|---------|
| 63.00 | 766.04 | 0.12096 | 0.00092162 | 2.21785 |
| 64.00 | 765.23 | 0.12070 | 0.00091016 | 2.22218 |
| 65.00 | 764.43 | 0.12045 | 0.00089891 | 2.22648 |
| 66.00 | 763.62 | 0.12019 | 0.00088789 | 2.23078 |
| 67.00 | 762.82 | 0.11993 | 0.00087707 | 2.23505 |
| 68.00 | 762.01 | 0.11968 | 0.00086646 | 2.23932 |
| 69.00 | 761.21 | 0.11942 | 0.00085604 | 2.24357 |
| 70.00 | 760.40 | 0.11916 | 0.00084582 | 2.24780 |
| 71.00 | 759.59 | 0.11890 | 0.00083579 | 2.25203 |
| 72.00 | 758.78 | 0.11864 | 0.00082594 | 2.25624 |
| 73.00 | 757.97 | 0.11838 | 0.00081627 | 2.26043 |
| 74.00 | 757.16 | 0.11812 | 0.00080677 | 2.26461 |
| 75.00 | 756.35 | 0.11786 | 0.00079744 | 2.26878 |
| 76.00 | 755.53 | 0.11759 | 0.00078828 | 2.27294 |
| 77.00 | 754.72 | 0.11733 | 0.00077928 | 2.27709 |
| 78.00 | 753.90 | 0.11707 | 0.00077043 | 2.28122 |
| 79.00 | 753.09 | 0.11680 | 0.00076174 | 2.28534 |
| 80.00 | 752.27 | 0.11654 | 0.00075320 | 2.28945 |
| 81.00 | 751.45 | 0.11627 | 0.00074480 | 2.29354 |
| 82.00 | 750.64 | 0.11601 | 0.00073655 | 2.29763 |
| 83.00 | 749.82 | 0.11574 | 0.00072844 | 2.30170 |
| 84.00 | 749.00 | 0.11547 | 0.00072046 | 2.30576 |
| 85.00 | 748.18 | 0.11520 | 0.00071261 | 2.30981 |
| 86.00 | 747.35 | 0.11494 | 0.00070489 | 2.31385 |
| 87.00 | 746.53 | 0.11467 | 0.00069730 | 2.31788 |
| 88.00 | 745.71 | 0.11439 | 0.00068983 | 2.32189 |
| 89.00 | 744.88 | 0.11412 | 0.00068249 | 2.32590 |
| 90.00 | 744.05 | 0.11385 | 0.00067526 | 2.32990 |
| 91.00 | 743.23 | 0.11358 | 0.00066814 | 2.33388 |
| 92.00 | 742.40 | 0.11330 | 0.00066114 | 2.33786 |
| 93.00 | 741.57 | 0.11303 | 0.00065425 | 2.34182 |
| 94.00 | 740.74 | 0.11275 | 0.00064747 | 2.34578 |
| 95.00 | 739.91 | 0.11248 | 0.00064079 | 2.34972 |
| 96.00 | 739.08 | 0.11220 | 0.00063421 | 2.35366 |
| 97.00 | 738.24 | 0.11193 | 0.00062774 | 2.35758 |
| 98.00 | 737.41 | 0.11167 | 0.00062136 | 2.36150 |
| 99.00 | 736.57 | 0.11141 | 0.00061508 | 2.36541 |
| 100.00 | 735.73 | 0.11115 | 0.00060891 | 2.36931 |
| 101.00 | 734.89 | 0.11089 | 0.00060280 | 2.37320 |
| 102.00 | 734.06 | 0.11062 | 0.00059680 | 2.37708 |
| 103.00 | 733.21 | 0.11036 | 0.00059088 | 2.38095 |
| 104.00 | 732.37 | 0.11009 | 0.00058506 | 2.38481 |
| 105.00 | 731.53 | 0.10983 | 0.00057931 | 2.38867 |
| 106.00 | 730.68 | 0.10956 | 0.00057365 | 2.39252 |

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|--------|--------|---------|------------|---------|
| 107.00 | 729.84 | 0.10929 | 0.00056807 | 2.39635 |
| 108.00 | 728.99 | 0.10902 | 0.00056258 | 2.40018 |
| 109.00 | 728.14 | 0.10875 | 0.00055716 | 2.40401 |
| 110.00 | 727.29 | 0.10848 | 0.00055181 | 2.40782 |
| 111.00 | 726.44 | 0.10820 | 0.00054654 | 2.41163 |
| 112.00 | 725.59 | 0.10793 | 0.00054135 | 2.41543 |
| 113.00 | 724.74 | 0.10765 | 0.00053623 | 2.41922 |
| 114.00 | 723.88 | 0.10737 | 0.00053117 | 2.42301 |
| 115.00 | 723.03 | 0.10709 | 0.00052619 | 2.42678 |
| 116.00 | 722.17 | 0.10681 | 0.00052128 | 2.43056 |
| 117.00 | 721.31 | 0.10652 | 0.00051643 | 2.43432 |
| 118.00 | 720.45 | 0.10623 | 0.00051165 | 2.43808 |
| 119.00 | 719.59 | 0.10594 | 0.00050693 | 2.44183 |
| 120.00 | 718.73 | 0.10565 | 0.00050227 | 2.44557 |
| 121.00 | 717.86 | 0.10535 | 0.00049768 | 2.44931 |
| 122.00 | 717.00 | 0.10505 | 0.00049315 | 2.45304 |
| 123.00 | 716.13 | 0.10474 | 0.00048868 | 2.45676 |
| 124.00 | 715.26 | 0.10444 | 0.00048426 | 2.46048 |
| 125.00 | 714.39 | 0.10412 | 0.00047991 | 2.46419 |
| 126.00 | 713.52 | 0.10380 | 0.00047561 | 2.46790 |
| 127.00 | 712.64 | 0.10348 | 0.00047136 | 2.47160 |
| 128.00 | 711.77 | 0.10314 | 0.00046717 | 2.47529 |
| 129.00 | 710.89 | 0.10280 | 0.00046304 | 2.47898 |
| 130.00 | 710.01 | 0.10244 | 0.00045895 | 2.48267 |
| 131.00 | 709.13 | 0.10207 | 0.00045492 | 2.48634 |
| 132.00 | 708.25 | 0.10167 | 0.00045094 | 2.49002 |
| 133.00 | 707.37 | 0.10122 | 0.00044701 | 2.49368 |
| 134.00 | 706.48 | 0.10066 | 0.00044313 | 2.49735 |
| 135.00 | 705.59 | 0.09893 | 0.00043929 | 2.50100 |
| 136.00 | 704.70 | 0.09865 | 0.00043550 | 2.50466 |
| 137.00 | 703.81 | 0.09837 | 0.00043176 | 2.50830 |
| 138.00 | 702.92 | 0.09809 | 0.00042807 | 2.51195 |
| 139.00 | 702.03 | 0.09781 | 0.00042442 | 2.51559 |
| 140.00 | 701.13 | 0.09752 | 0.00042081 | 2.51922 |
| 141.00 | 700.23 | 0.09723 | 0.00041725 | 2.52285 |
| 142.00 | 699.33 | 0.09693 | 0.00041373 | 2.52647 |
| 143.00 | 698.43 | 0.09664 | 0.00041025 | 2.53009 |
| 144.00 | 697.52 | 0.09633 | 0.00040681 | 2.53371 |
| 145.00 | 696.61 | 0.09602 | 0.00040342 | 2.53732 |
| 146.00 | 695.71 | 0.09570 | 0.00040006 | 2.54093 |
| 147.00 | 694.79 | 0.09538 | 0.00039675 | 2.54454 |
| 148.00 | 693.88 | 0.09504 | 0.00039347 | 2.54814 |
| 149.00 | 692.97 | 0.09468 | 0.00039023 | 2.55173 |
| 150.00 | 692.05 | 0.09429 | 0.00038702 | 2.55533 |

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|--------|--------|---------|------------|---------|
| 151.00 | 691.13 | 0.09383 | 0.00038386 | 2.55892 |
| 152.00 | 690.20 | 0.09289 | 0.00038073 | 2.56250 |
| 153.00 | 689.28 | 0.09225 | 0.00037764 | 2.56609 |
| 154.00 | 688.35 | 0.09197 | 0.00037458 | 2.56966 |
| 155.00 | 687.42 | 0.09169 | 0.00037155 | 2.57324 |
| 156.00 | 686.49 | 0.09141 | 0.00036857 | 2.57681 |
| 157.00 | 685.56 | 0.09113 | 0.00036561 | 2.58039 |
| 158.00 | 684.62 | 0.09085 | 0.00036269 | 2.58395 |
| 159.00 | 683.68 | 0.09056 | 0.00035980 | 2.58752 |
| 160.00 | 682.74 | 0.09027 | 0.00035694 | 2.59108 |
| 161.00 | 681.79 | 0.08998 | 0.00035411 | 2.59464 |
| 162.00 | 680.84 | 0.08969 | 0.00035132 | 2.59819 |
| 163.00 | 679.89 | 0.08939 | 0.00034855 | 2.60175 |
| 164.00 | 678.94 | 0.08909 | 0.00034582 | 2.60530 |
| 165.00 | 677.98 | 0.08879 | 0.00034311 | 2.60885 |
| 166.00 | 677.02 | 0.08848 | 0.00034043 | 2.61240 |
| 167.00 | 676.06 | 0.08817 | 0.00033779 | 2.61594 |
| 168.00 | 675.10 | 0.08786 | 0.00033517 | 2.61948 |
| 169.00 | 674.13 | 0.08754 | 0.00033258 | 2.62302 |
| 170.00 | 673.15 | 0.08722 | 0.00033001 | 2.62656 |
| 171.00 | 672.18 | 0.08689 | 0.00032748 | 2.63010 |
| 172.00 | 671.20 | 0.08655 | 0.00032497 | 2.63363 |
| 173.00 | 670.22 | 0.08622 | 0.00032249 | 2.63717 |
| 174.00 | 669.23 | 0.08587 | 0.00032003 | 2.64070 |
| 175.00 | 668.25 | 0.08552 | 0.00031760 | 2.64423 |
| 176.00 | 667.25 | 0.08515 | 0.00031519 | 2.64776 |
| 177.00 | 666.26 | 0.08478 | 0.00031281 | 2.65129 |
| 178.00 | 665.26 | 0.08440 | 0.00031046 | 2.65481 |
| 179.00 | 664.25 | 0.08400 | 0.00030813 | 2.65834 |
| 180.00 | 663.25 | 0.08359 | 0.00030582 | 2.66186 |
| 181.00 | 662.24 | 0.08316 | 0.00030353 | 2.66538 |
| 182.00 | 661.22 | 0.08271 | 0.00030127 | 2.66890 |
| 183.00 | 660.20 | 0.08221 | 0.00029904 | 2.67243 |
| 184.00 | 659.18 | 0.08167 | 0.00029682 | 2.67595 |
| 185.00 | 658.15 | 0.08105 | 0.00029463 | 2.67947 |
| 186.00 | 657.12 | 0.08027 | 0.00029246 | 2.68298 |
| 187.00 | 656.08 | 0.07881 | 0.00029031 | 2.68650 |
| 188.00 | 655.04 | 0.07652 | 0.00028818 | 2.69002 |
| 189.00 | 653.99 | 0.07620 | 0.00028607 | 2.69354 |
| 190.00 | 652.98 | 0.07588 | 0.00028399 | 2.69705 |
| 191.00 | 651.96 | 0.07555 | 0.00028192 | 2.70057 |
| 192.00 | 650.93 | 0.07520 | 0.00027988 | 2.70409 |
| 193.00 | 649.90 | 0.07482 | 0.00027785 | 2.70760 |
| 194.00 | 648.87 | 0.07441 | 0.00027584 | 2.71112 |

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|--------|--------|---------|------------|---------|
| 195.00 | 647.84 | 0.07392 | 0.00027386 | 2.71464 |
| 196.00 | 646.80 | 0.07320 | 0.00027189 | 2.71816 |
| 197.00 | 645.75 | 0.07168 | 0.00026994 | 2.72167 |
| 198.00 | 644.70 | 0.07142 | 0.00026802 | 2.72519 |
| 199.00 | 643.65 | 0.07116 | 0.00026611 | 2.72871 |
| 200.00 | 642.60 | 0.07090 | 0.00026421 | 2.73223 |
| 201.00 | 641.53 | 0.07063 | 0.00026234 | 2.73575 |
| 202.00 | 640.47 | 0.07037 | 0.00026048 | 2.73927 |
| 203.00 | 639.40 | 0.07009 | 0.00025865 | 2.74279 |
| 204.00 | 638.33 | 0.06982 | 0.00025682 | 2.74631 |
| 205.00 | 637.25 | 0.06954 | 0.00025502 | 2.74983 |
| 206.00 | 636.16 | 0.06925 | 0.00025323 | 2.75336 |
| 207.00 | 635.07 | 0.06896 | 0.00025146 | 2.75688 |
| 208.00 | 633.98 | 0.06866 | 0.00024971 | 2.76041 |
| 209.00 | 632.88 | 0.06836 | 0.00024797 | 2.76394 |
| 210.00 | 631.78 | 0.06805 | 0.00024625 | 2.76747 |
| 211.00 | 630.67 | 0.06774 | 0.00024454 | 2.77100 |
| 212.00 | 629.55 | 0.06741 | 0.00024285 | 2.77453 |
| 213.00 | 628.43 | 0.06708 | 0.00024118 | 2.77807 |
| 214.00 | 627.30 | 0.06673 | 0.00023952 | 2.78161 |
| 215.00 | 626.17 | 0.06636 | 0.00023787 | 2.78515 |
| 216.00 | 625.03 | 0.06598 | 0.00023624 | 2.78869 |
| 217.00 | 623.89 | 0.06557 | 0.00023463 | 2.79223 |
| 218.00 | 622.74 | 0.06513 | 0.00023303 | 2.79578 |
| 219.00 | 621.58 | 0.06462 | 0.00023144 | 2.79933 |
| 220.00 | 620.41 | 0.06397 | 0.00022987 | 2.80288 |
| 221.00 | 619.24 | 0.06221 | 0.00022832 | 2.80643 |
| 222.00 | 618.06 | 0.06145 | 0.00022677 | 2.80999 |
| 223.00 | 616.88 | 0.06115 | 0.00022524 | 2.81355 |
| 224.00 | 615.68 | 0.06084 | 0.00022373 | 2.81711 |
| 225.00 | 614.48 | 0.06051 | 0.00022222 | 2.82068 |
| 226.00 | 613.27 | 0.06016 | 0.00022073 | 2.82425 |
| 227.00 | 612.06 | 0.05979 | 0.00021926 | 2.82782 |
| 228.00 | 610.83 | 0.05939 | 0.00021779 | 2.83139 |
| 229.00 | 609.60 | 0.05893 | 0.00021634 | 2.83497 |
| 230.00 | 608.36 | 0.05833 | 0.00021490 | 2.83856 |
| 231.00 | 607.10 | 0.05704 | 0.00021348 | 2.84215 |
| 232.00 | 605.84 | 0.05652 | 0.00021207 | 2.84574 |
| 233.00 | 604.57 | 0.05475 | 0.00021066 | 2.84934 |
| 234.00 | 603.29 | 0.05453 | 0.00020928 | 2.85294 |
| 235.00 | 602.03 | 0.05431 | 0.00020790 | 2.85655 |
| 236.00 | 600.77 | 0.05409 | 0.00020653 | 2.86016 |
| 237.00 | 599.50 | 0.05386 | 0.00020518 | 2.86377 |
| 238.00 | 598.22 | 0.05363 | 0.00020384 | 2.86740 |

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|--------|--------|---------|------------|---------|
| 239.00 | 596.93 | 0.05340 | 0.00020251 | 2.87102 |
| 240.00 | 595.63 | 0.05316 | 0.00020119 | 2.87465 |
| 241.00 | 594.31 | 0.05291 | 0.00019988 | 2.87829 |
| 242.00 | 592.99 | 0.05267 | 0.00019858 | 2.88193 |
| 243.00 | 591.75 | 0.05241 | 0.00019729 | 2.88558 |
| 244.00 | 590.58 | 0.05216 | 0.00019602 | 2.88924 |
| 245.00 | 589.40 | 0.05189 | 0.00019475 | 2.89290 |
| 246.00 | 588.22 | 0.05162 | 0.00019350 | 2.89657 |
| 247.00 | 587.03 | 0.05134 | 0.00019225 | 2.90024 |
| 248.00 | 585.83 | 0.05105 | 0.00019102 | 2.90392 |
| 249.00 | 584.64 | 0.05075 | 0.00018979 | 2.90761 |
| 250.00 | 583.43 | 0.05043 | 0.00018858 | 2.91131 |
| 251.00 | 582.23 | 0.05008 | 0.00018738 | 2.91501 |
| 252.00 | 581.02 | 0.04971 | 0.00018618 | 2.91872 |
| 253.00 | 579.80 | 0.04927 | 0.00018500 | 2.92244 |
| 254.00 | 578.57 | 0.04837 | 0.00018382 | 2.92617 |
| 255.00 | 577.35 | 0.04792 | 0.00018266 | 2.92991 |
| 256.00 | 576.11 | 0.04712 | 0.00018150 | 2.93365 |
| 257.00 | 574.87 | 0.04609 | 0.00018035 | 2.93741 |
| 258.00 | 573.63 | 0.04584 | 0.00017922 | 2.94117 |
| 259.00 | 572.38 | 0.04557 | 0.00017809 | 2.94494 |
| 260.00 | 571.12 | 0.04528 | 0.00017697 | 2.94872 |
| 261.00 | 569.86 | 0.04495 | 0.00017586 | 2.95252 |
| 262.00 | 568.59 | 0.04426 | 0.00017476 | 2.95632 |
| 263.00 | 567.32 | 0.04401 | 0.00017366 | 2.96013 |
| 264.00 | 566.04 | 0.04375 | 0.00017258 | 2.96396 |
| 265.00 | 564.76 | 0.04348 | 0.00017150 | 2.96780 |
| 266.00 | 563.46 | 0.04319 | 0.00017044 | 2.97164 |
| 267.00 | 562.16 | 0.04288 | 0.00016938 | 2.97550 |
| 268.00 | 560.86 | 0.04254 | 0.00016833 | 2.97938 |
| 269.00 | 559.55 | 0.04215 | 0.00016729 | 2.98326 |
| 270.00 | 558.23 | 0.04167 | 0.00016625 | 2.98716 |
| 271.00 | 556.90 | 0.04074 | 0.00016523 | 2.99107 |
| 272.00 | 555.57 | 0.03970 | 0.00016421 | 2.99500 |
| 273.00 | 554.23 | 0.03944 | 0.00016320 | 2.99894 |
| 274.00 | 552.88 | 0.03916 | 0.00016220 | 3.00289 |
| 275.00 | 551.53 | 0.03884 | 0.00016120 | 3.00686 |
| 276.00 | 550.17 | 0.03844 | 0.00016021 | 3.01085 |
| 277.00 | 548.80 | 0.03721 | 0.00015923 | 3.01485 |
| 278.00 | 547.42 | 0.03701 | 0.00015826 | 3.01887 |
| 279.00 | 546.03 | 0.03681 | 0.00015730 | 3.02290 |
| 280.00 | 544.64 | 0.03661 | 0.00015634 | 3.02695 |
| 281.00 | 543.23 | 0.03639 | 0.00015539 | 3.03102 |
| 282.00 | 541.82 | 0.03615 | 0.00015445 | 3.03511 |

| | | | | |
|--------|--------|---------|------------|---------|
| 283.00 | 540.40 | 0.03591 | 0.00015351 | 3.03922 |
| 284.00 | 538.97 | 0.03563 | 0.00015258 | 3.04335 |
| 285.00 | 537.54 | 0.03531 | 0.00015166 | 3.04750 |
| 286.00 | 536.09 | 0.03462 | 0.00015075 | 3.05167 |
| 287.00 | 534.63 | 0.03421 | 0.00014984 | 3.05586 |
| 288.00 | 533.17 | 0.03398 | 0.00014894 | 3.06008 |
| 289.00 | 531.69 | 0.03373 | 0.00014804 | 3.06431 |
| 290.00 | 530.20 | 0.03345 | 0.00014716 | 3.06857 |
| 291.00 | 528.71 | 0.03313 | 0.00014627 | 3.07286 |
| 292.00 | 527.20 | 0.03273 | 0.00014540 | 3.07717 |
| 293.00 | 525.68 | 0.03203 | 0.00014453 | 3.08151 |
| 294.00 | 524.15 | 0.03086 | 0.00014367 | 3.08587 |
| 295.00 | 522.61 | 0.03067 | 0.00014281 | 3.09027 |
| 296.00 | 521.06 | 0.03046 | 0.00014196 | 3.09469 |
| 297.00 | 519.49 | 0.03016 | 0.00014112 | 3.09914 |
| 298.00 | 517.92 | 0.02970 | 0.00014029 | 3.10362 |
| 299.00 | 516.33 | 0.02953 | 0.00013945 | 3.10814 |
| 300.00 | 514.73 | 0.02935 | 0.00013863 | 3.11269 |
| 301.00 | 513.11 | 0.02915 | 0.00013781 | 3.11727 |
| 302.00 | 511.48 | 0.02891 | 0.00013700 | 3.12189 |
| 303.00 | 501.71 | | | 3.12509 |
| 304.00 | 489.39 | | | 3.12775 |
| 305.00 | 477.58 | | | 3.13040 |

Table 2: Reference data for Heat Transfer Coefficient

| Heat Exchanger | Temperature (°C) | Velocity (m/s) | Heat Transfer Coefficient (W/m ² .K) |
|----------------|------------------|----------------|---|
| E-1101A/B | 58 | 1.79 | 1506 |
| E-1102A/B | 86 | 1.62 | 1567 |
| E-1103A/B | 108 | 1.06 | 1194 |
| E-1105A-D | 138.5 | 0.78 | 996 |
| E-1106 | 149 | 2.12 | 2241 |
| E-1107 | 154 | 1.7 | 1903 |
| E-1109 | 185.5 | 1.35 | 1769 |
| E-1110 | 204 | 2.89 | 3442 |