

**INTELLIGENT POWER QUALITY ASSESSMENT IN A PLANT
DISTRIBUTION SYSTEM**

By

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FINAL PROJECT REPORT

**Submitted to the Electrical & Electronics Engineering Programme
in Partial Fulfillment of the Requirements
for the Degree
Bachelor of Engineering (Hons)
(Electrical & Electronics Engineering)**

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CERTIFICATION OF APPROVAL

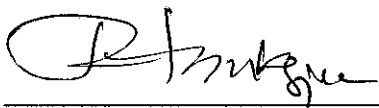
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Approved:



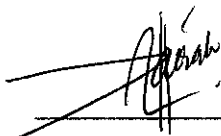
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Project Supervisor

UNIVERSITI TEKNOLOGI PETRONAS
TRONOH, PERAK

December 2007

CERTIFICATION OF ORIGINALITY

This is to certify that I am responsible for the work submitted in this project, that the original work is my own except as specified in the references and acknowledgements, and that the original work contained herein have not been undertaken or done by unspecified sources or persons.



Syairah binti Abdul Ghani

ABSTRACT

The objective of this project is to develop a power quality assessment procedure on a plant distribution system. This project focuses on identifying and differentiating features of two voltage sags waveforms caused by fault and large load starting respectively by using one of the digital signals processing technique, wavelet analysis. Power quality has become an important issue for electricity consumers at all levels of usage. It can be defined as the quality of voltage that results in proper operation of power quality sensitive equipment. It has very wide aspects and elements and will be discussed further in this report. Wavelets analysis is a windowing technique which can determine different frequency component of a signal with different resolutions. Wavelet analysis is very useful in analyzing non-stationary signals whose characteristics change with time. Then by using the Wavelet Toolbox, the two waveforms can be analyzed and differentiated.

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TABLE OF CONTENTS

LIST OF TABLES	ix
LIST OF FIGURES.....	x
CHAPTER 1 INTRODUCTION	1
1.1 Background of Study.....	1
1.2 Problem Statement	1
1.2.1 Problem Identification	1
1.2.2 Significance of the Project.....	1
1.3 Objectives and Scope of the Study	2
CHAPTER 2 LITERATURE REVIEW / THEORY	3
2.1 Power Quality.....	3
2.1.1 Transients.....	3
2.1.2 Sag/Undervoltage.....	4
2.1.3 Swell/Overvoltage	5
2.1.4 Interruptions.....	6
2.1.5 Waveform Distortion	7
2.1.6 Voltage Fluctuations	9
2.1.7 Frequency Variations.....	10
2.2 Wavelet Analysis.....	10
2.2.1 The Drawback of Fourier Analysis.....	11
2.2.2 Wavelet Basics.....	11
2.2.3 The Discrete Wavelet Transform (DWT).....	12
CHAPTER 3 METHODOLOGY / PROJECT WORK	14
3.1 Procedure Identification	14
3.2 Tools.....	15
3.2.1 Fluke 43B Power Quality Analyzer.....	15
3.2.2 Wavelet Toolbox.....	15
CHAPTER 4 RESULTS AND DISCUSSIONS.....	17
4.1 Findings	17
4.1.1 Data Recording at Plant	17
4.1.2 Wavelet Analysis on Actual Data.....	19
4.2 Discussions.....	21

4.2.1 Data Recording at Plant	21
4.2.2 Wavelet Analysis on Actual Data.....	21
CHAPTER 5 CONCLUSIONS AND RECOMMENDATIONS	23
REFERENCES.....	24
APPENDICES.....	26
Appendix A WORK PROCEDURE FOR VOLTAGE SAG RECORDING.....	27
Appendix B JOB SAFETY ANALYSIS	32
Appendix C CALCULATION OF RESULTS.....	33

LIST OF TABLES

Table 1 Duration of Interruptions [2].....	6
Table 2 Result for amplitude ratio analysis for approximations	19
Table 3 Result for amplitude ratio analysis for details	20
Table 4 Result for frequency analysis.....	20

LIST OF FIGURES

Figure 1 Impulsive Transients.....	4
Figure 2 Oscillatory Transients.....	4
Figure 3 Voltage Sags	5
Figure 4 Undervoltage.....	5
Figure 5 Swell	6
Figure 6 Overvoltage.....	6
Figure 7 Interruption	7
Figure 8 DC Offset.....	7
Figure 9 Harmonics [1]	8
Figure 10 Interharmonics	8
Figure 11 Notching [1].....	9
Figure 12 Noise [1]	9
Figure 13 Voltage Fluctuations.....	10
Figure 14 Frequency Variations.....	10
Figure 15 Examples of Mother Wavelet (a)Meyer (b)Morlet (c)Mexican Hat	12
Figure 16 Wavelet Decomposition [4].....	12
Figure 17 Multi-level Decomposition [4]	13
Figure 18 The Procedure Flow Chart.....	14
Figure 19 The Example of Statistic Options in Wavelet Toolbox	16
Figure 20 The Example of Obtaining Frequency using Command Line	16
Figure 21 The Voltage Waveform	18
Figure 22 The Current Waveform.....	18

CHAPTER 1

INTRODUCTION

1.1 Background of Study

Intelligent power quality assessment procedure in a plant distribution system is a project which focuses on characterization of voltage sag waveforms. The characterization of the waveforms is obtained by using wavelet analysis.

1.2 Problem Statement

1.2.1 Problem Identification

Voltage sag is the most common power disturbance in industry. It is actually a brief reduction in voltage on AC power systems between half cycles to a few seconds. Voltage sags can be caused by many reasons such as starting a large load, loose or defective wiring, faults or short circuits. This may result in equipment failure and difficulty in plant operation, which leads to lost production; hence will increase the cost and affect the economical aspects of a company.

1.2.2 Significance of the Project

Since voltage sags may originate from various sources, a complete investigation has to be done in order to identify the cause when an event occurs. This is due to the different ways of overcoming the problem depending on the cause leading to voltage sag. From this project, wavelet analysis is utilized to differentiate the different type of voltage sag waveforms. Hence, the cause of the problem can be identified based on the features identified in the project. Using the features identified in this project, actual cause leading to a voltage dip can be determined online.

1.3 Objectives and Scope of the Study

The objective of the project is to identifying the features which differentiate one cause from the other, leading to voltage sag in order to recognize voltage sag event from its signature from a control room. This study focuses on differentiating the two waveforms of voltage sags that originate from large load starting and fault respectively. The actual data of large load starting event were recorded from Gas Processing Plant B, Petronas Gas Berhad, Paka, Terengganu. The signature for voltage sag due to fault were obtained from Star LRT Sentul Timur.

CHAPTER 2

LITERATURE REVIEW / THEORY

2.1 Power Quality

According to IEEE, the power quality problem can be defined in seven categories based on the waveforms which are:

- Transients
- Sags / Undervoltage
- Swells / Overvoltage
- Interruptions
- Waveform distortions
- Voltage fluctuations
- Frequency variations [2]

2.1.1 Transients

Transient are large, short duration voltage changes resulting from lightning strike or switching operations on the network. It will occur for less than one half cycle of the mains voltage. [1]

Transients can be divided again into two categories; impulsive transients and oscillatory transients. Impulsive transients are characterized by the rate of change of voltage or current magnitude as impulsive transients are generally events where currents and/or voltage are suddenly raising in positive or negative direction in fast, medium and slow speed. [2] Impulsive transients can be caused by lightning, poor grounding, fault clearing by the utility, or switching of inductive loads. People sometimes refer impulsive transients as power surge or spike.

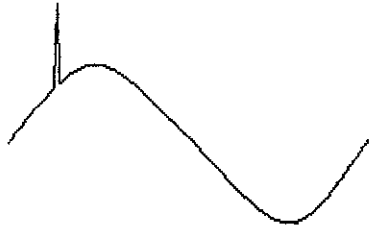


Figure 1 Impulsive Transients

Oscillatory transients on the other hand can be characterized by the frequency content and duration. It is a sudden change in the steady-state condition of a signal's voltage and/or current at both positive and negative signal limits oscillating at the natural system frequency and decay to zero within a cycle. [1] Oscillatory transients can originate from turning off an inductive or capacitive load such as capacitor banks or motors.

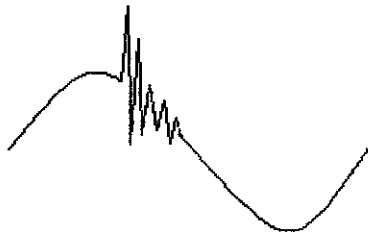


Figure 2 Oscillatory Transients

2.1.2 Sag/Undervoltage

Sags are reduction in the RMS voltage in the range of 10% to 90% of nominal voltage for duration more than half cycle to one minute. The possible causes that can lead to voltage sag are system fault, increase load demand, and translational event such as large motor starting. [3]

Voltage sags are the most common power disturbance and can disturb electronic equipment which lack sufficient internal energy storage. When large motor starts, it can draw up to six times or more its normal running current. This will surely caused the voltage drops within the circuit. Voltage sags may also originate from utility. When the utility attempted to clear the faults, it may cause voltage sag when it cleared

more quickly or when the fault itself is a momentarily one.

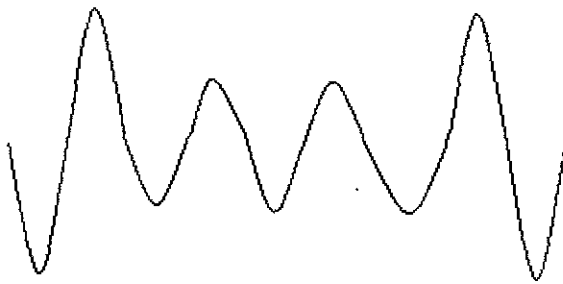


Figure 3 Voltage Sags

Undervoltage is an event resulted from the long term sags. It is a long term variation, which usually more than 1 minute and the voltage are less than 90% of the nominal voltage. Undervoltage maybe caused from the switching off of large loads or energization of large capacitor bank. It can create overheating in motors and lead to the failure of the nonlinear loads such as computer power supplies. [1]

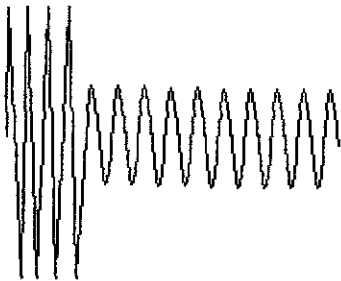


Figure 4 Undervoltage

2.1.3 Swell/Overtoltage

Swell is the reverse of the sags; an increment of RMS voltage more than 110% of nominal voltage for duration more than half main cycle and less than 1 minute. Swell can be originated from system faults, single-phase fault on a three-phase system, load switching, or capacitor switching. Swell can result to data errors, flickering of lights, degradation of electrical contacts, semiconductor damage in electronics and insulation degradation. [1]

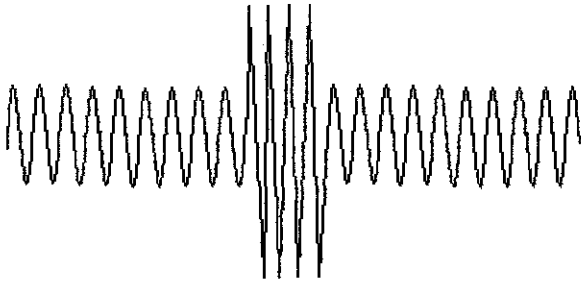


Figure 5 Swell

Just as the undervoltage, overvoltage is the long term version of the swell. The cause of this problem is mainly from the wrong tapping setting of the supply transformer, or the load reduction. This event will cause excess heat to the equipment

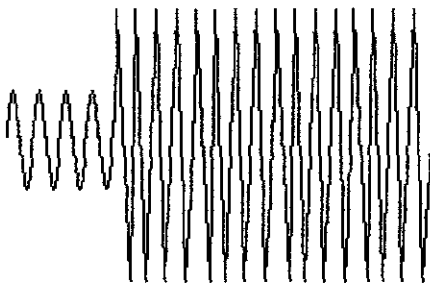


Figure 6 Overvoltage

2.1.4 Interruptions

Interruption is defined as the complete loss of supply voltage or load current depending on its duration. An interruption can be categorized as instantaneous, momentary, temporary, or sustained as described below: [1]

Table 1 Duration of Interruptions [2]

Instantaneous	0.5 to 30 cycles
Momentary	30 cycles to 2 seconds
Temporary	2 seconds to 2 minutes
Sustained	Greater than 2 minutes

There are many causes of interruption to occur and it can vary from place to place. The causes are lightning strikes, animals, trees, vehicle accidents, destructive weather, equipment failure or basic circuit breaker tripping. Interruptions can cause many losses to the industry and business. It will also cause loss of valuable data when information from the computer resulted from the corrupted data when the power suddenly loss.

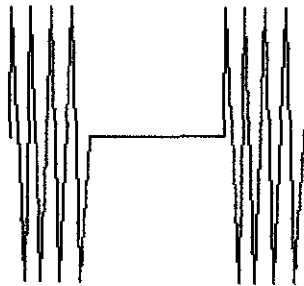


Figure 7 Interruption

2.1.5 *Waveform Distortion*

Waveform distortion can be divided into five types:

- DC Offset

Dc offset is usually due to failures of rectifiers within the many AC to DC conversion technologies. It also may originate from poor grounding. DC can traverse in the AC power system and add unwanted current to devices already operating at their rated level. The circulating DC current may result in overheating and saturation of transformers. The saturated transformers will lead to failure of full power delivery to the load and the instability in electronic load equipment. [1]

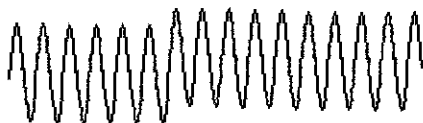


Figure 8 DC Offset

- Harmonics

Harmonics are additional frequencies presents in the mains voltage or current that are integral multiples of the main frequency. [2] As an example, 150 Hz is the third harmonics of a 50 Hz fundamental frequency; $3 \times 50 = 150$ Hz. The main cause for harmonics is nonlinear loads such as power electronic loads. Harmonics can cause many problems such as overheated transformers, neutral conductors and other electrical equipment and the tripping of circuit breakers, and loss of synchronization on timing circuits that are dependent upon a usual clean sine wave. [1]



Figure 9 Harmonics [1]

- Interharmonics

Interharmonics is the distorted voltage or current waveform containing periodic distortions of a sinusoidal nature that are not integer multiples of the fundamental supply frequency. This event originates from the faulty equipment, cycloconverters, induction motors and arcing devices. This event can lead to flicker of displays and incandescent lights and may cause heat to the equipment and communication interference.



Figure 10 Interharmonics

- Notching

Notching is a result from the normal operation of 3-phase electronic switching devices such as AC to DC converters, variable speed drives, and light dimmers. The notching can result to system halts, data loss and data transmission problems. [1]

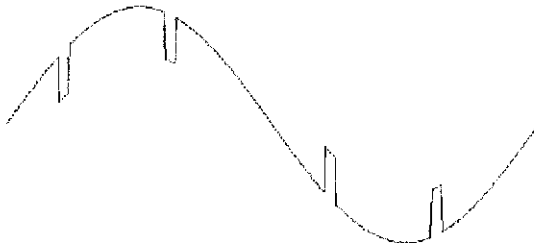


Figure 11 Notching [1]

- Noise

Noise is a disturbance with a broad frequency distribution up to about 200000Hz.[2] It can be generated by the power electronic devices, control circuits, arc welders, switching power supplies and so on. Poor grounding may also lead to noise problem. Noise can cause equipment malfunction, long term component failure and so on. [1]

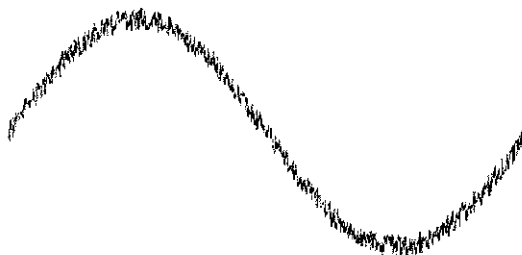


Figure 12 Noise [1]

2.1.6 Voltage Fluctuations

Voltage fluctuations is a systematic variation of the voltage waveform or a series of

random voltage changes of small dimension, from 95% to 105% of nominal voltage at low frequency generally below 25Hz. [1] Voltage fluctuations can be caused from any load that exhibits significant current variations. This event can lead to flickering of incandescent lamps.

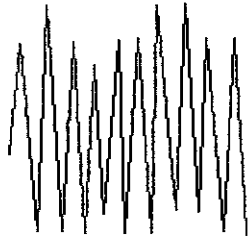


Figure 13 Voltage Fluctuations

2.1.7 Frequency Variations

Frequency variation is more common if the generator is heavily loaded, however it is rarely happening in the utility power systems. This may cause the motor to run faster or slower to match the frequency of the input power as the speed of rotation will depend on the frequency. This will lead the motor to heat and degradation through additional motor speed and current draw.

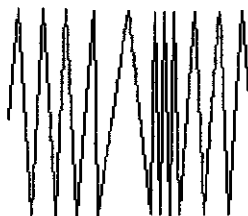


Figure 14 Frequency Variations

2.2 Wavelet Analysis

Wavelet analysis is a useful tool in analyzing non-stationary signals and utilizing a windowing technique with variable-sized regions. Wavelet analysis allows the use of long time intervals if more precise low frequency information would like to be

obtained and shorter regions can be used if high frequency information is desired. [4]

2.2.1 The Drawback of Fourier Analysis

Fourier Transform is also one type of analyzing signals. Fourier Transform will actually break down a signal into constituent sinusoids of different frequencies. However, Fourier Transform has its own disadvantages and limitations where it can only reports the frequency that presents in the portion of the signal that is within the window. It cannot identify the times at which various frequency component occurs within a window. It is impossible to tell when a particular event took place when looking at the Fourier Transform. Fourier Transform can only be useful if the signal has the frequency content that stationary within a window. It fails to analyze non-stationary signal which the frequency content are unpredictable within a window. [5]

2.2.2 Wavelet Basics

Wavelet analysis can overcome the drawback of the Fourier Transform as it can analyze the signal with different resolutions by using the notion of function at different scales. Scales are inversely proportional to the frequency:

$$\text{Scale} = \alpha / \text{Frequency} \quad [5]$$

Wavelet function localized both in frequency and time. There are wavelet families which each family has a characteristic shape and basic scale for each family covers a known and fixed interval of time. A wavelet family contains each component of the wavelet with consist of the father wavelet, mother wavelet and the other wavelet components which scaled and translated from the father or the mother wavelet itself. Father wavelet produces scaling function for the wavelet family whereas the mother wavelet produces the wavelet function. Both the father and mother wavelet has the scale equals to 1. There are many types of wavelet families exist such as Haar, Daubechies-6, Daubechies-16, Symlets, Coiflets and so on. All of the wavelet families are localized in time and they are nonzero only over a finite of time. [5]

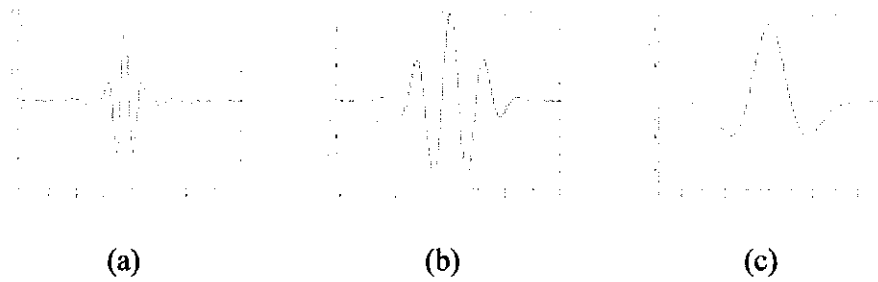


Figure 15 Examples of Mother Wavelet (a)Meyer (b)Morlet (c)Mexican Hat

Wavelet transforms are classified into discrete wavelet transform (DWT) and continuous wavelet transform (CWT). CWT operate over every possible scale and translation whereas DWT use a specific subset of scale and translation values.

2.2.3 The Discrete Wavelet Transform (DWT)

The Discrete Wavelet Transform (DWT) provides the DWT coefficients $c_j[k]$ and $d_j[k]$ for the decomposition of the signal into its scaling function and wavelet function components. The scaling function coefficients $h_0[k]$ and wavelet function coefficient $h_1[k]$ maybe viewed as impulse response of a pair of filters. For all wavelet families, $h_0[k]$ behaves as the low pass filter and $h_1[k]$ behaves as a high pass filter. The filters divide the spectrum into two equal frequency bands. The low pass filter output contains the low frequency elements of the signal while the high pass output contains the high frequency component of the signal. [5]

In MATLAB, the output of the filter can be termed as approximation (A) and details (D). The approximations are the high-scale, low-frequency components of the signal. The details are the low-scale, high-frequency components. [4]

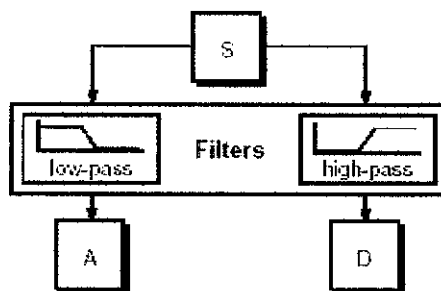


Figure 16 Wavelet Decomposition [4]

In wavelet analysis, the signal to be analyzed is divided into two parts by filtering it through the low pass and high pass filters as mentioned before. The high pass filter will pick up the small details whereas the low pass filter will pick up everything else. This process continues with the low pass portion of signals which in turn filtered by low and high pass filters. Further detail of the signal is uncovered at each step and the process of the subdividing the low frequency bands can continue as long as detail remains. [5] This is called multi-level decomposition. When the filtering only occurs once, then it is only level-1 decomposition and so on.

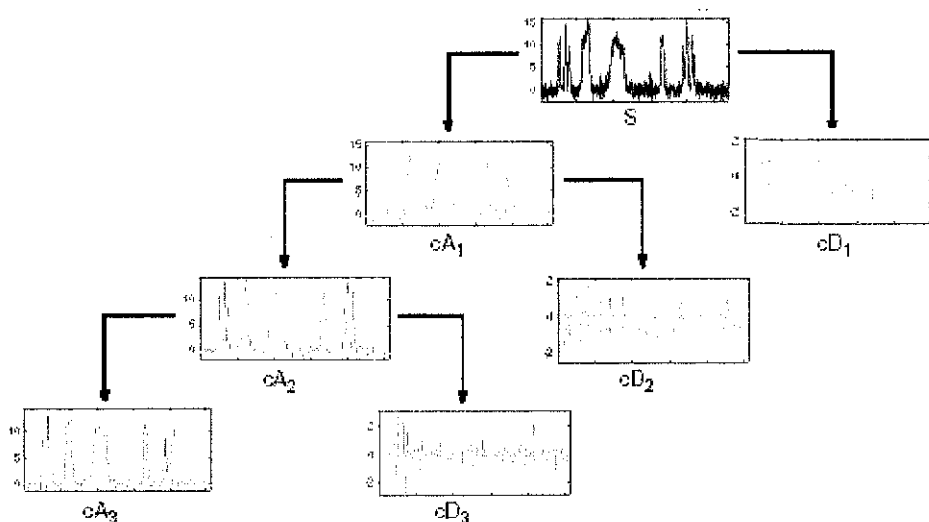
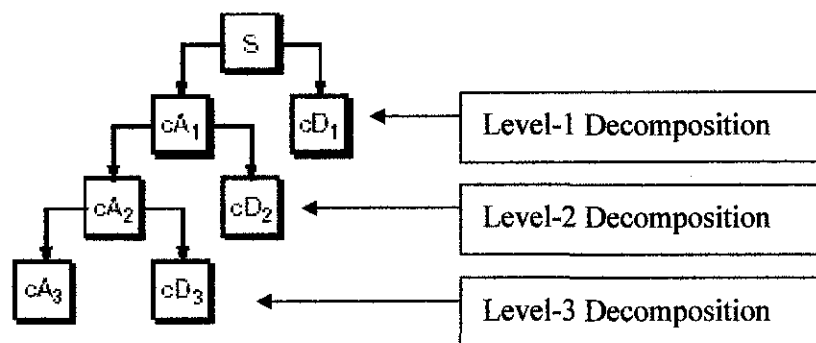


Figure 17 Multi-level Decomposition [4]

Filtering the low pass portion is to obtain the best frequency resolution at the lowest frequencies while accepting the poorer frequency resolution at higher frequencies. [5]

CHAPTER 3

METHODOLOGY / PROJECT WORK

3.1 Procedure Identification

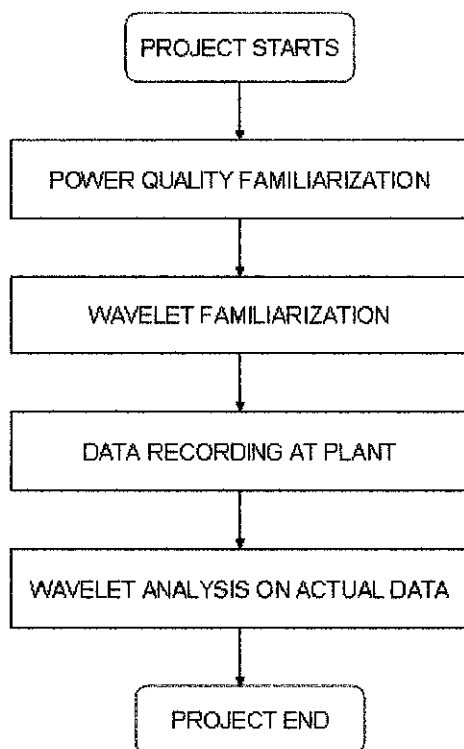


Figure 18 The Procedure Flow Chart

From the chart above, the project starts with a study on power quality as well as wavelet. The actual sag event then recorded at Gas Processing Plant B, Paka. Then, all the materials studied been applied in analyzing and classifying the waveforms captured at the plant as well as the data from Star LRT Sentul event.

3.2 Tools

3.2.1 Fluke 43B Power Quality Analyzer

The Fluke 43B Power Quality Analyzer performs the measurements to maintain power systems, troubleshoot power problems and diagnose equipment. By using this tool, a voltage sag scenario can be recorded as desired. This analyzer can measure both voltage and current and it also able to store memory up to 16 days. For the project, the recording has been done for 8 minutes only.

3.2.2 Wavelet Toolbox

The Wavelet Toolbox contains graphical tools and command line functions that can examine and explore characteristics of individual wavelet packets, perform wavelet packet analysis of one-dimensional and two-dimensional data and use wavelet packets to compress and remove noise from signals and images. [4] Since this project only involves in analyzing waveforms, only one-dimensional data analysis has been used. The analysis has been done by using the Discrete Wavelet Transform in the toolbox.

The analysis includes obtaining the amplitude ratio and the frequency at each level of analysis. The amplitude ratio has been done by finding the peak absolute value of both approximations and details for each level which can be obtained directly from the statistics option in the wavelet. The frequency of each level can be obtained by using command lines `scal2frq`.

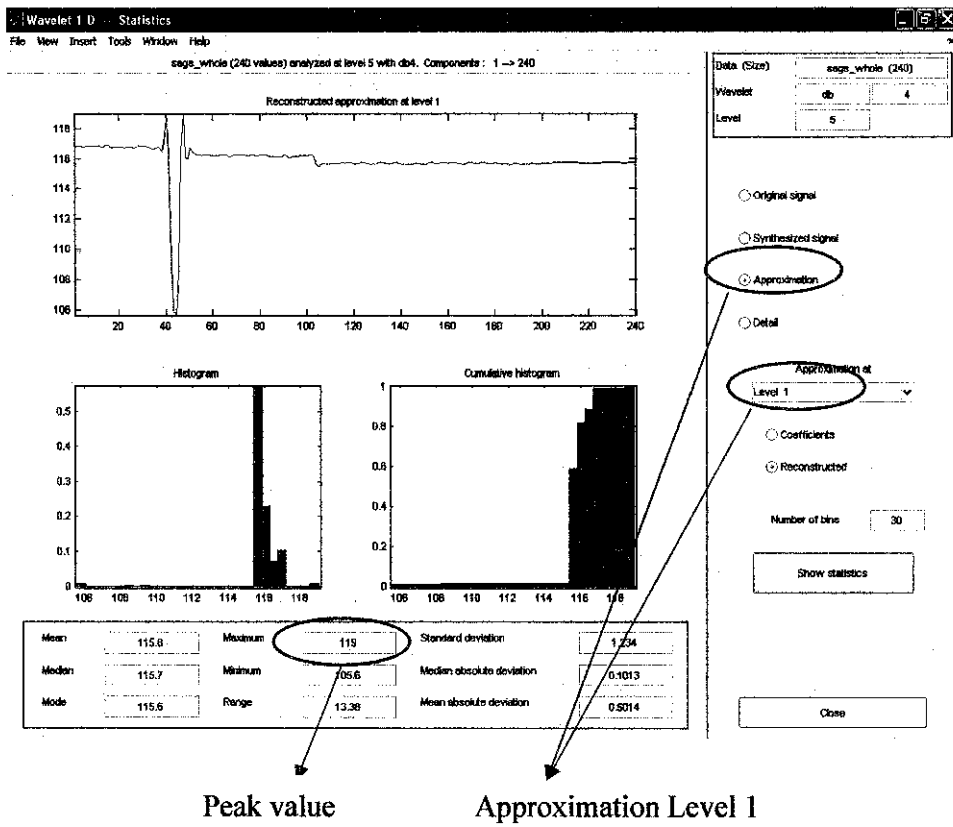


Figure 19 The Example of Statistic Options in Wavelet Toolbox

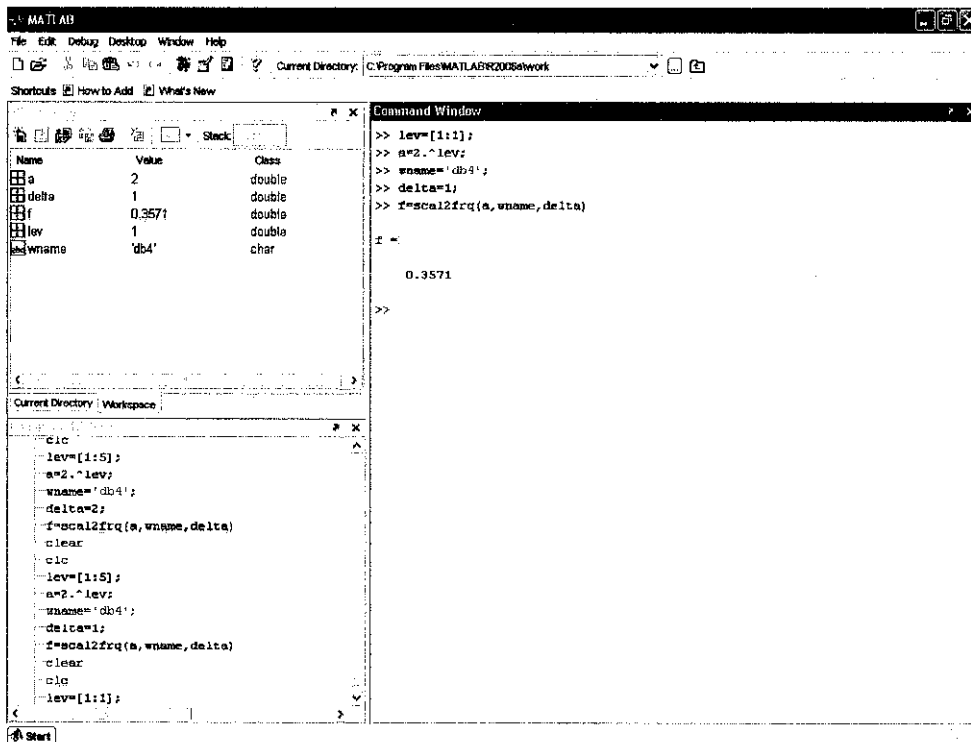


Figure 20 The Example of Obtaining Frequency using Command Line

CHAPTER 4

RESULTS AND DISCUSSIONS

4.1 Findings

4.1.1 Data Recording at Plant

A trip to the plant, Gas Processing Plant B at Paka, Terengganu has been carried out during the last semester break. The purpose of this trip is to record and collect the data of voltage and current during large motor starting. The recording has been done successfully with the help and guidance from all the engineers and technicians.

The recording has been done by using Fluke 43B, Power Quality Analyzer at the 6.6KV busbar in one of the substation called GPP6 Process Substation. The motor involved in this recording is PM6-201E, motor for Amine Pump at Acid Gas Removal Unit (Unit 2). The work procedure and job safety analysis (JSA) for the recording can be referred at Appendix A and B respectively.

The work procedure is necessary in order to do any tasks in plant so that accidents can be avoided as there are high risks of any accidents to occur in plants. Proper work procedure ensures all the tasks carried out smoothly and all the safety measures are taken into account. The safety job analysis is essential so that any possibilities of accident to occur during the tasks have been analyzed first and the all precautionary measures are taken to avoid it. Both of the documents are needed together to apply for the cold work permit for the motor test runs.

The recorder has been set to record for 8 minutes. When the test run is scheduled, all the tools preparation has been set up in the substation with the help of technicians.

The results are as follows:

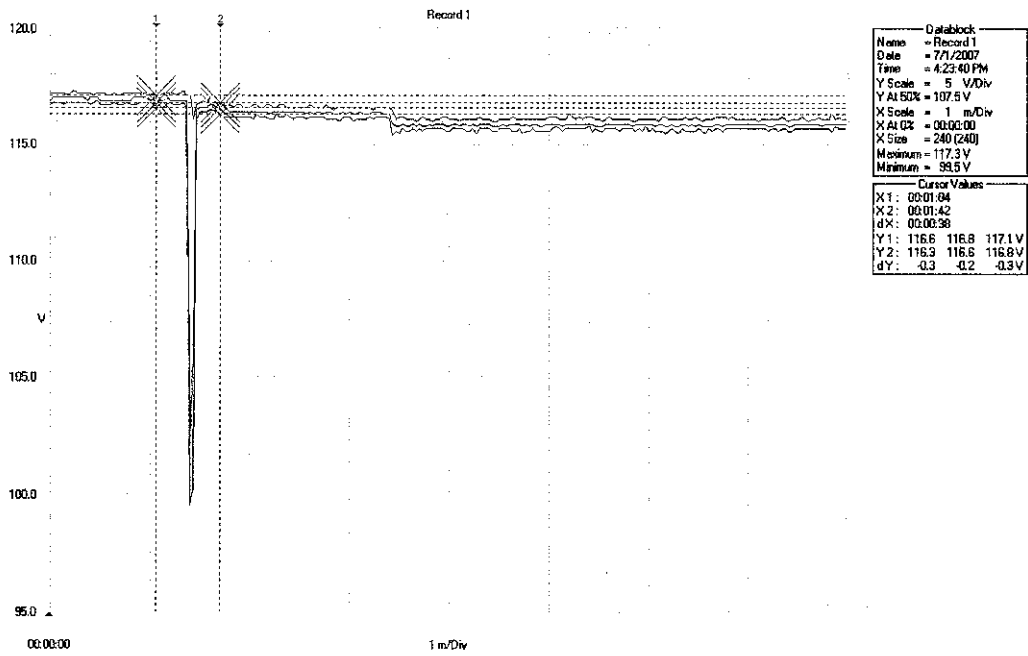


Figure 21 The Voltage Waveform

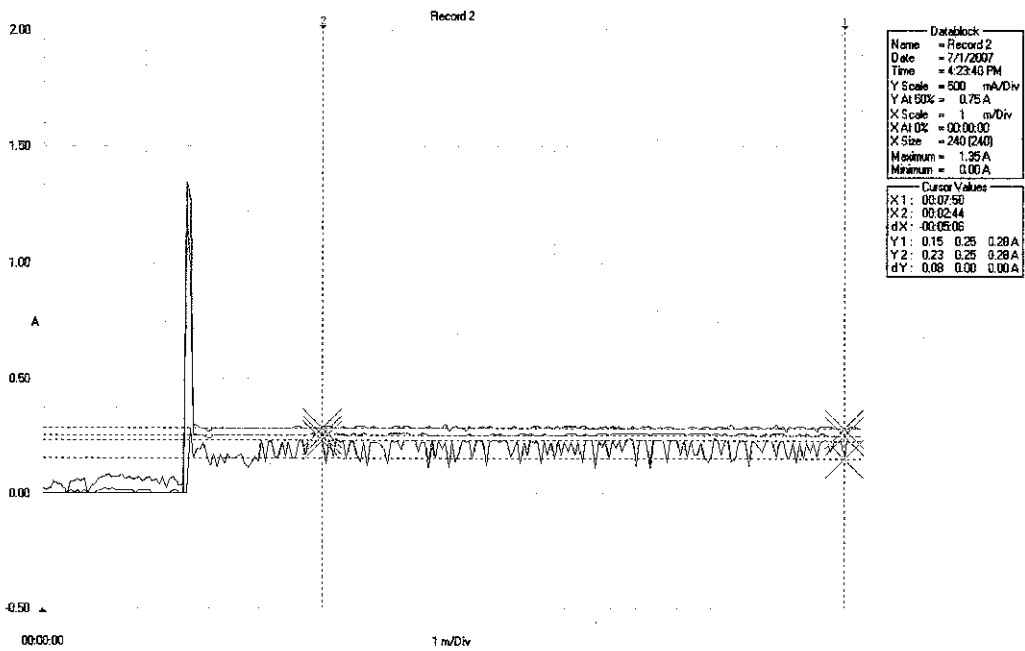


Figure 22 The Current Waveform

4.1.2 Wavelet Analysis on Actual Data

The wavelet analysis on the actual data has been carried out for the voltage recorded data. The aim for the analysis is to find the amplitude ratio and frequency component for all level of details and approximations. In order to find the amplitude for the signal, wavelet decomposition of level 5 using Daubechies 4 has been carried out. The analysis has been done to the overall signal, then to each part of the signal that is part of before, during and after the sag.

The results are as below:

Table 2 Result for amplitude ratio analysis for approximations

WAVEFORM TYPE	α_n	WHOLE	BEFORE	DURING	AFTER
Sag due to large load starting	n=1	0.9992	1.0000	1.0000	1.0000
	n=2	1.0000	1.0000	0.9479	1.0000
	n=3	0.9866	1.0000		0.9991
	n=4	0.9866	1.0000		0.9991
	n=5	0.9832	1.0000		0.9991
Sag due to fault	n=1	1.0000	1.0000	1.0000	1.0000
	n=2	0.9496		0.9266	0.9887
	n=3	0.9415		0.9211	0.9690
	n=4	0.9370		0.9220	
	n=5	0.9037			

Table 3 Result for amplitude ratio analysis for details

WAVEFORM TYPE	α_n	WHOLE	BEFORE	DURING	AFTER
Sag due to large load starting	n=1	1.0000	0.7529	0.1609	1.0000
	n=2	0.4280	1.0000	1.0000	0.6461
	n=3	0.6749	0.7312		0.7879
	n=4	0.1450	0.1315		0.7238
	n=5	0.1425	0.2464		0.2521
Sag due to fault	n=1	1.0000	1.0000	1.0000	1.0000
	n=2	0.3206		0.7607	0.3667
	n=3	0.3432		0.4722	0.1395
	n=4	0.3946		0.5786	
	n=5	0.4241			

Table 4 Result for frequency analysis

WAVEFORM TYPE	FREQUENCY			
	WHOLE	BEFORE	DURING	AFTER
Sag due to large load starting	0.1786	0.1786	0.1786	0.1786
	0.0893	0.0893	0.0893	0.0893
	0.0446	0.0446		0.0446
	0.0223	0.0223		0.0223
	0.0112	0.0112		0.0112
Sag due to fault	0.3571	0.3571	0.3571	0.3571
	0.1786		0.1786	0.1786
	0.0893		0.0893	0.0893
	0.0446		0.0446	
	0.0223			

4.2 Discussions

4.2.1 Data Recording at Plant

Figure 21 and 22 shows the result of the sag event recorded at plant. This recording was set to last for 8 minutes. From the figure, the characteristic of the current and voltage can be clearly seen. The voltage dropped abruptly the moment the motor was started. At the same time when the voltage dropped, the current started to increase. These are the waveforms of the sag event due to large load starting.

This value can be converted to the excel data by using Fluke 43B software. Then, this data can be converted to MATLAB file in order to do the analysis using the MATLAB Wavelet Toolbox.

4.2.2 Wavelet Analysis on Actual Data

Table 2 and table 3 shows the result of the wavelet analysis based on the amplitude ratio. Both of the waveform type results were shown at the same table. The amplitude ratio was calculated using the equation:

$$\alpha_n = \frac{\text{Peak absolute value of level } n \text{ approximations/details}}{\text{Highest peak absolute value among the levels}}$$

Where:

α_n = the amplitude ratio of level n

Table 4 shows the result for the frequency analysis. In order to find the frequency of waveforms, a command line function has been used; `scal2frq`. This function calculates the frequency based on the scales as the equation:

$$F_a = F_c / a \Delta \quad [4]$$

Where:

F_a = pseudo-frequency corresponding to the scale, a

F_c = centre frequency of a wavelet in Hz

a = scale

Δ = sampling period

These amplitude ratio and frequency was calculated using both the whole waveform and also each segment of the sag signature; that is before, during and after the sag. The analysis has been done that way so that the analysis can be narrowed down thus the differences can be seen a lot more clearly. The details of the calculation can be referred at Appendix C.

There are differences of energy content in the sag signature. Both of the events are actually different in process although both resulted in voltage sag event. Hence, the energy contents of the signatures are bound to be different.

The differences are quite appreciable. By using these indices in real-time it is possible to debug the voltage sag signature to identify whether it is due to large load starting or fault. Identification of the cause will facilitate determination of the mitigation options.

CHAPTER 5

CONCLUSIONS AND RECOMMENDATIONS

This project is useful since power quality has become an important issue in industry these days. The features identified in the project which is amplitude ratio and frequency components enable discrimination of one voltage sag signature from the other, enabling detection of the cause that led to voltage sag. Using these differentiating features, formulation of a fuzzy logic based classification procedure is recommended as a future work.

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APPENDICES

APPENDIX A

WORK PROCEDURE FOR VOLTAGE SAG RECORDING

	INTELLIGENT POWER QUALITY ASSESSMENT IN A PLANT DISTRIBUTION SYSTEM FINAL YEAR PROJECT	 <small>UNIVERSITI TEKNOLOGI MALAYSIA</small>
WORK PROCEDURE		

NO	WORK DESCRIPTION	ACTION	STATUS	REMARKS
1	Preparation of Permit To Work (PTW) and Job Safety Analysis (JSA)	Work Leader		
2	Preparation and inspection of tool/equipment	Work Leader & Electrical Inspector		
3	Inform HT Chargeman, Authorized Competent Person, and Operation Personnel	Work Leader		
4	Preparation at work area. Recording will start before motor starts so that the results before and after motor starts will be obtained.	Work Leader		6.6KV spare panel & SB6-DO3 (SB6-D01/DO2)
5	Work Step (refer to attachment for detail drawings): <u>CURRENT MEASUREMENT</u> 1. Identify the correct panel for the measurement 2. Clamp the Power Quality Analyzer at the respective cables 3. Make sure that all the checklist completed before start the recording 4. Recording is carried out for about 30 minutes	Work Leader		SB6-DO3 (SB6-D01/DO2) C11, C31 & C51 <i>(Attachment A)</i> <i>(Attachment B)</i>



	<p><u>VOLTAGE MEASUREMENT</u></p> <ol style="list-style-type: none"> 1. Identify the correct panel for the measurement 2. Do the connection at terminal block 3. Make sure that all the checklist completed before start the recording 4. Recording is carried out for about 30 minutes <p>*Voltage and current reading are recorded simultaneously</p>			<p>6.6KV spare panel (SB6-D01/DO2)</p> <p>E11, E31 & E51</p> <p><i>(Attachment C)</i></p> <p><i>(Attachment D)</i></p>
5	Recording stops after 30 minutes	Work Leader		
6	Housekeeping at work area	Work Leader		
5	Completion and inform HT Chargeman, Authorized Competent Person, and Operation Personnel	Work Leader		
6	Close PTW	Work Leader		

Prepared by:

Syairah Abdul Ghani

Reviewed and approved by:

Mr Ag Zulkarenain Awangku Rajid

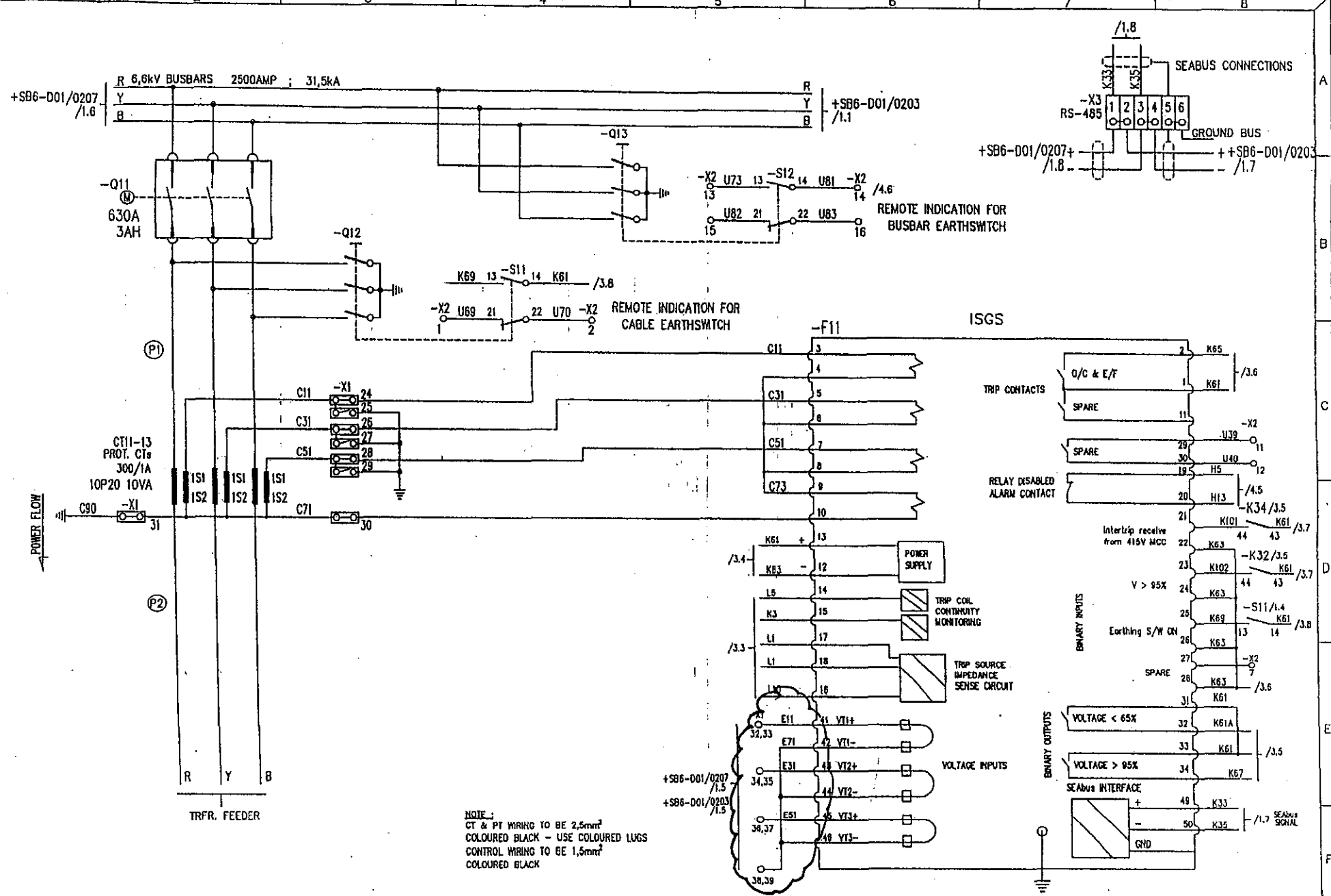
	INTELLIGENT POWER QUALITY ASSESSMENT IN A PLANT DISTRIBUTION SYSTEM FINAL YEAR PROJECT	 <small>UNIVERSITI TEKNOLOGI MALAYSIA</small>
	ATTACHMENT	

ATTACHMENT	DETAILS	REMARKS
A	<u>6.6KV Switchgear SB6-DO3, SB6-DO1/DO2 Circuit Diagram</u> Refer to Drawing 1	C11
B	<u>Current Measurement Checklist</u> Please make sure: <ol style="list-style-type: none"> 1. The clamp of the Power Quality Analyzer is properly clamped at the respective cables 2. Power Quality Analyzer is turned on 	
C	<u>6.6KV Switchgear Spare SB6-DO1/DO2 Circuit Diagram</u> Refer to Drawing 2	E11 & E 31
D	<u>Voltage Measurement Checklist</u> Please make sure: <ol style="list-style-type: none"> 1. The probes of the Power Quality Analyzer is properly connected to the terminal 2. The terminal is properly tighten – no loose connection 3. Power Quality Analyzer is turned on 	

Proprietor's name, Verwendungsname, Name, Unterschrift, Ver-
 nichtung und Unterschrift des Zeichners, Zeichnername,
 Commencement date, Datum der Ausführung, Beginn der Ausführung,
 Commencement date, Datum der Ausführung, Beginn der Ausführung,
 Confirmed as correct, Richtig, Korrektur, Richtig, Korrektur, Richtig, Korrektur,
 Confirmed as correct, Richtig, Korrektur, Richtig, Korrektur, Richtig, Korrektur

Weibung des Verwendungsname, Name, Unterschrift, Ver-
 nichtung und Unterschrift des Zeichners, Zeichnername,
 Beginn der Ausführung, Datum der Ausführung, Beginn der Ausführung,
 Beginn der Ausführung, Datum der Ausführung, Beginn der Ausführung,
 Beginn der Ausführung, Datum der Ausführung, Beginn der Ausführung

SYMBOLS: PETRONAS
 CAD-NR: 05308201



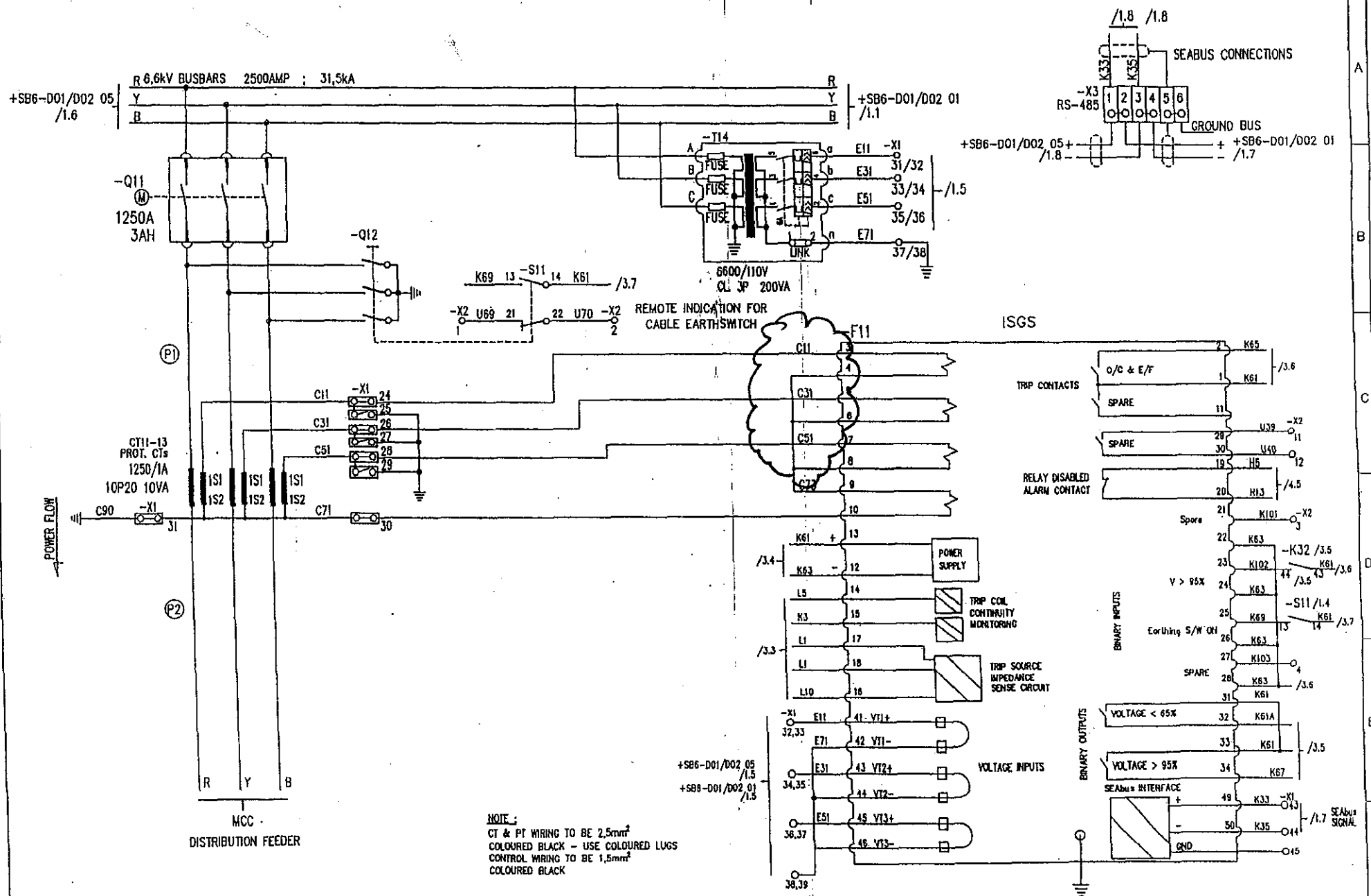
NOTE:
 CT & PT WIRING TO BE 2.5mm²
 COLOURED BLACK - USE COLOURED LUGS
 CONTROL WIRING TO BE 1.5mm²
 COLOURED BLACK

DATE	08/10/96	PETRONAS GAS BERHAD MALAYSIA		Siemens Pte. Ltd.		6.6kV SWITCHGEAR		SPC DRG. No.		= SPARE		57
SITE MOD.	04/98	GPP 5 & 6		Singapore Office		SPARE		060/6000/604		+ SB6-D01/0205		+
AS BUILT	08/97	LP APPR. P. DE VRIES		REPL. BY		SB6-D01/0202		CUSTOMER'S DRAWING No.		MANUFACTURE'S DRAWING No.		SHEET 1
REVISION	REMARKS	DATE	NAME/NORM	ORIG.	REPL. F.	CIRCUIT DIAGRAM		00-EX-E-641564		(3)G53005-G0053-5082-B		4 SHTS

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SYMBOLS: PETRONAS
 CAD-NR: 05308301




NOTE:
 CT & PT WIRING TO BE 2.5mm²
 COLOURED BLACK - USE COLOURED LUGS
 CONTROL WIRING TO BE 1.5mm²
 COLOURED BLACK

REVISION	REMARKS	DATE	NAMENOR	ORIG.	PREP.	DATE	NAMENOR	ORIG.	PREP.	6.6kV SWITCHGEAR SB6-D03 SB6-D01/D02 CIRCUIT DIAGRAM	SPC DRG. No. 060/6000/604	CUSTOMER'S DRAWING No. SB6-D03	MANUFACTURE'S DRAWING No. + SB6-D01/D0203	61 +
B	SITE MOD.	05/98	RL	RC ADAMS		08/10/96	RC ADAMS			PETRONAS GAS BERHAD MALAYSIA GPP 5 & 6				SHEET 1
A	AS BUILT	06/97	LP	P. DE VRIES						Siemens Pte. Ltd. Singapore Office				

APPENDIX B

JOB SAFETY ANALYSIS

	JOB SAFETY ANALYSIS (JSA)	JOB TITLE : VOLTAGE & CURRENT RECORDING AT 6.6KV BUSBAR PANEL DURING LARGE MOTOR STARTING	JSA NO :	PAGE : Page 1 of 1	<input type="checkbox"/> NEW <input type="checkbox"/> REVISED
		EQUIPMENT NO :	DATE : 14/06/07	REV. NO .	
		SUPERVISOR : Mr Ag Zulkarenain Awangku Rajid	ANALYSIS BY :		
		DEPARTMENT :	REVIEWED BY : Mr Ag Zulkarenain Awangku Rajid		
NAME OF PERSON WHO DOES JOB :		COMPANY :	APPROVED BY :		
DESIGNATION :					
SEQUENCE OF BASIC JOB STEPS	POTENTIAL HAZARDS	PRECAUTIONARY MEASURES	ACTION BY:		
Preparation at work area	All the tools and equipment needed are not properly arranged The tool used damaged	Make sure all the tools and equipment are neatly arranged Make sure the tool are in good condition [Test the tools and equipment prior to the installation]			
Identify the correct panel for the measurement (both for current and voltage measurement)	Wrong panel for measurement hence the result obtained will not be as desired	Confirm the panel tagging with drawings			
Clamp the Power Quality Analyzer at the respective cables for current measurement	Wrong cable clamped Hazardous position of clamp	Confirm the cable tagging with drawings Make sure the clamp position is safe (not too near with other components in the panel) Proper tagging/label to inform other personnel			
Do the connection at the terminal block for voltage measurement	Loose of connection Wrong terminal tagging for measurement	Make sure the terminals are tighten up Confirm the terminal and cable tagging with drawings Proper tagging/label to inform other personnel			
Housekeeping at work area after work completed	No Injuries	General clean up on all working areas			

APPENDIX C

CALCULATION OF RESULTS

Sags due to large load starting analysis

Original data: (already recorded in RMS value)

TIME (s)	VOLTAGE (v)
0.00	116.70
2.00	116.80
4.00	116.80
6.00	116.80
8.00	116.70
10.00	116.80
12.00	116.80
14.00	116.80
16.00	116.80
18.00	116.80
20.00	116.80
22.00	116.80
24.00	116.70
26.00	116.80
28.00	116.90
30.00	116.70
32.00	116.70
34.00	116.70
36.00	116.70
38.00	116.80
40.00	116.70
42.00	116.70
44.00	116.70
46.00	116.80
48.00	116.70
50.00	116.70
52.00	116.70
54.00	116.80
56.00	116.80

58.00	116.80
60.00	116.80
62.00	116.80
64.00	116.60
66.00	116.60
68.00	116.60
70.00	116.70
72.00	116.80
74.00	116.70
76.00	116.70
78.00	116.70
80.00	116.80
82.00	116.60
84.00	99.50
86.00	100.20
88.00	116.10
90.00	116.40
92.00	116.40
94.00	116.40
96.00	116.50
98.00	116.50
100.00	116.40
102.00	116.30
104.00	116.20
106.00	116.20
108.00	116.20
110.00	116.20
112.00	116.20
114.00	116.20
116.00	116.20

118.00	116.20
120.00	116.20
122.00	116.10
124.00	116.30
126.00	116.20
128.00	116.20
130.00	116.20
132.00	116.10
134.00	116.10
136.00	116.30
138.00	116.20
140.00	116.20
142.00	116.30
144.00	116.20
146.00	116.10
148.00	116.20
150.00	116.20
152.00	116.20
154.00	116.10
156.00	116.20
158.00	116.20
160.00	116.20
162.00	116.20
164.00	116.20
166.00	116.10
168.00	116.10
170.00	116.10
172.00	116.10
174.00	116.00
176.00	116.20

178.00	116.20
180.00	116.20
182.00	116.00
184.00	116.10
186.00	116.10
188.00	116.10
190.00	116.10
192.00	116.20
194.00	116.10
196.00	116.20
198.00	116.20
200.00	116.20
202.00	116.20
204.00	116.10
206.00	115.40
208.00	115.60
210.00	115.50
212.00	115.70
214.00	115.60
216.00	115.60
218.00	115.70
220.00	115.60
222.00	115.70
224.00	115.60
226.00	115.70
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244.00	115.70
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248.00	115.70
250.00	115.60
252.00	115.60
254.00	115.70
256.00	115.50
258.00	115.70

260.00	115.70
262.00	115.70
264.00	115.70
266.00	115.60
268.00	115.60
270.00	115.70
272.00	115.70
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276.00	115.70
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286.00	115.60
288.00	115.60
290.00	115.70
292.00	115.60
294.00	115.60
296.00	115.60
298.00	115.60
300.00	115.60
302.00	115.70
304.00	115.80
306.00	115.70
308.00	115.60
310.00	115.70
312.00	115.70
314.00	115.70
316.00	115.70
318.00	115.70
320.00	115.70
322.00	115.70
324.00	115.80
326.00	115.60
328.00	115.70
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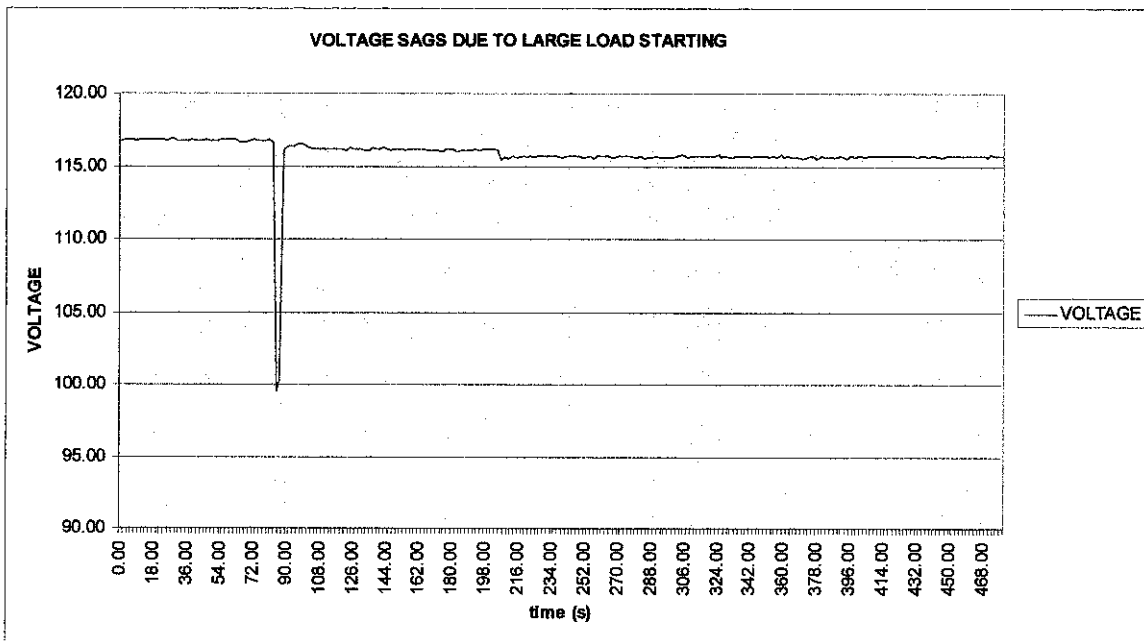
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356.00	115.60
358.00	115.80
360.00	115.60
362.00	115.70
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444.00	115.60
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448.00	115.70
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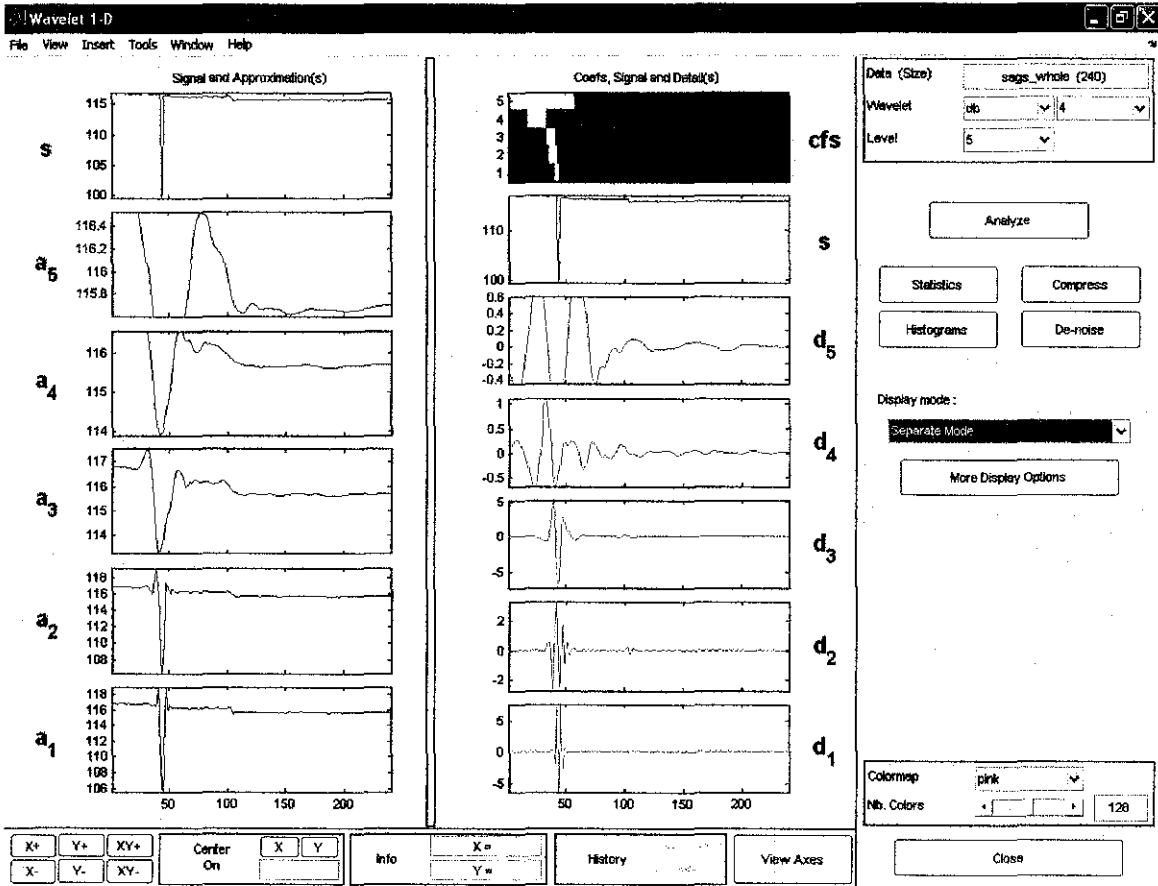
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466.00	115.70
468.00	115.70
470.00	115.60
472.00	115.80
474.00	115.70
476.00	115.70
478.00	115.70

Plot:



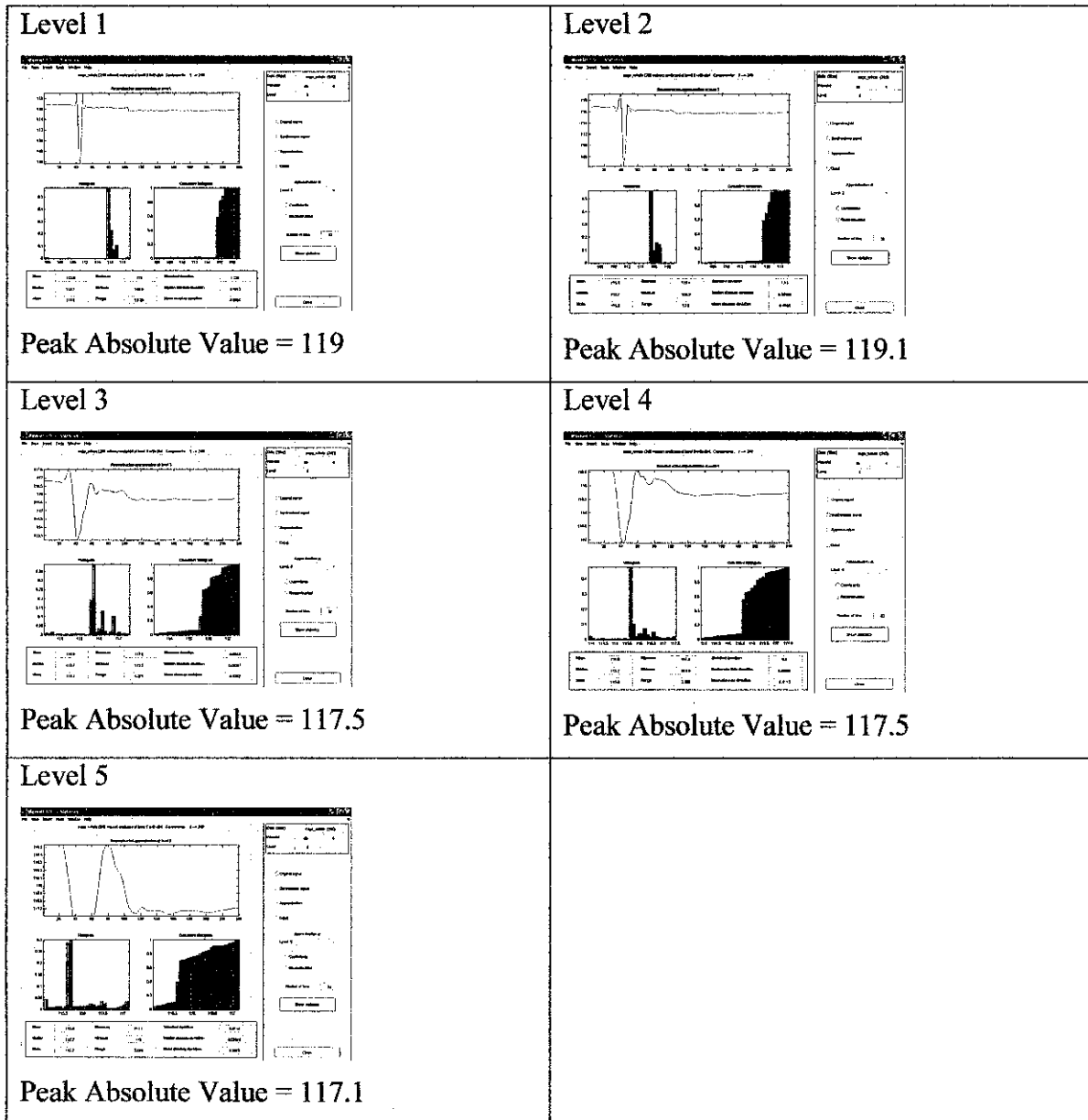
Wavelet Analysis:

Whole waveform analysis



- Amplitude ratio

For approximations:



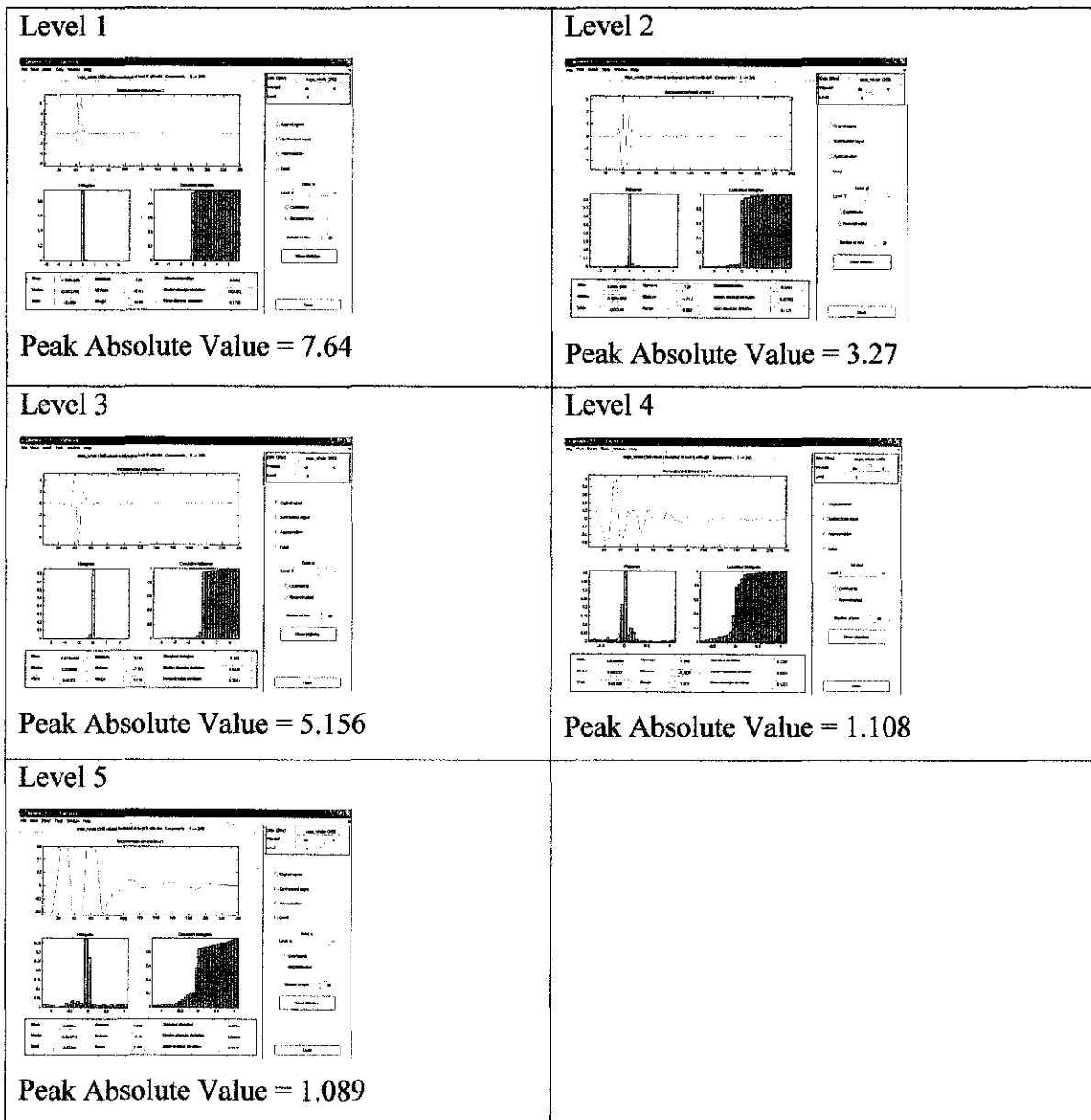
Ratio for each level of approximations:

$\alpha_n = \text{Peak absolute value of level } n \text{ approximation}$

Highest peak absolute value among the levels

α_n	VALUES
n=1	119/119.1 = 0.9992
n=2	119.1/119.1 = 1.0000
n=3	117.5/119.1 = 0.9866
n=4	117.5/119.1 = 0.9866
n=5	117.1/119.1 = 0.9832

For details:



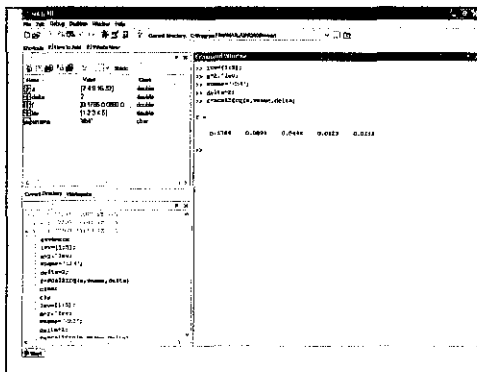
Ratio for each level of details:

$\alpha_n = \frac{\text{Peak absolute value of level } n \text{ details}}{\text{Highest peak absolute value among the levels}}$

Highest peak absolute value among the levels

α_n	VALUES
n=1	$7.64/7.64 = 1.0000$
n=2	$3.27/7.64 = 0.4280$
n=3	$5.156/7.64 = 0.6749$
n=4	$1.108/7.64 = 0.1450$
n=5	$1.089/7.64 = 0.1425$

- Frequency

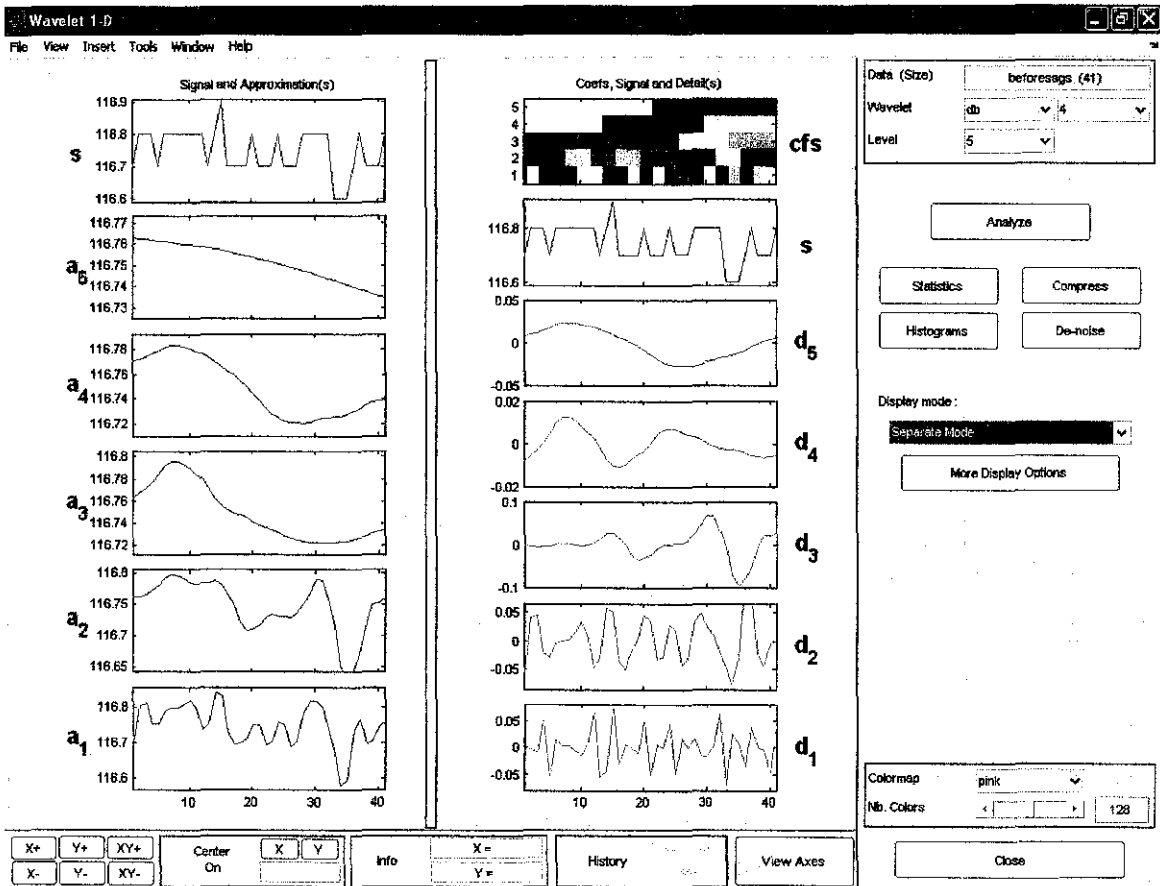


Result:

f =

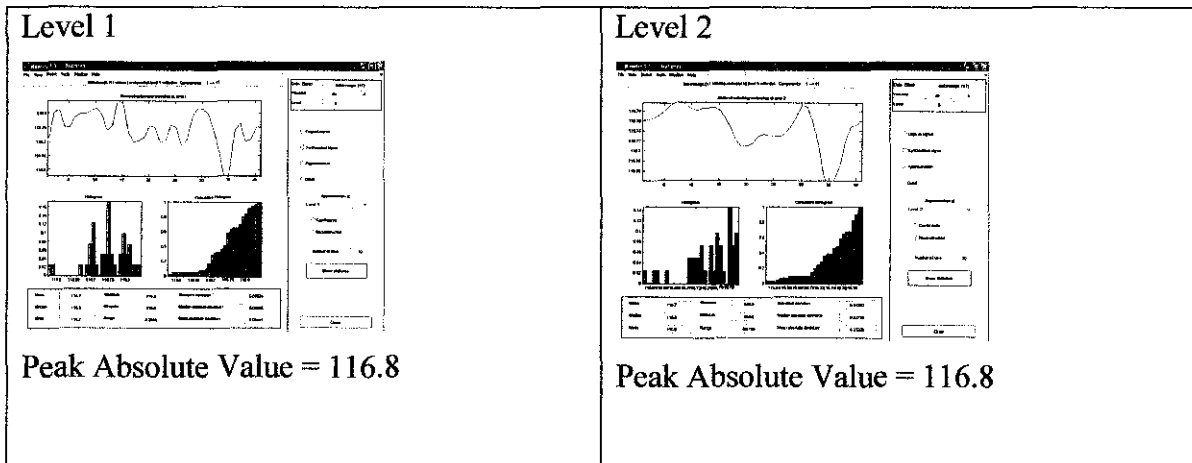
0.1786 0.0893 0.0446 0.0223 0.0112

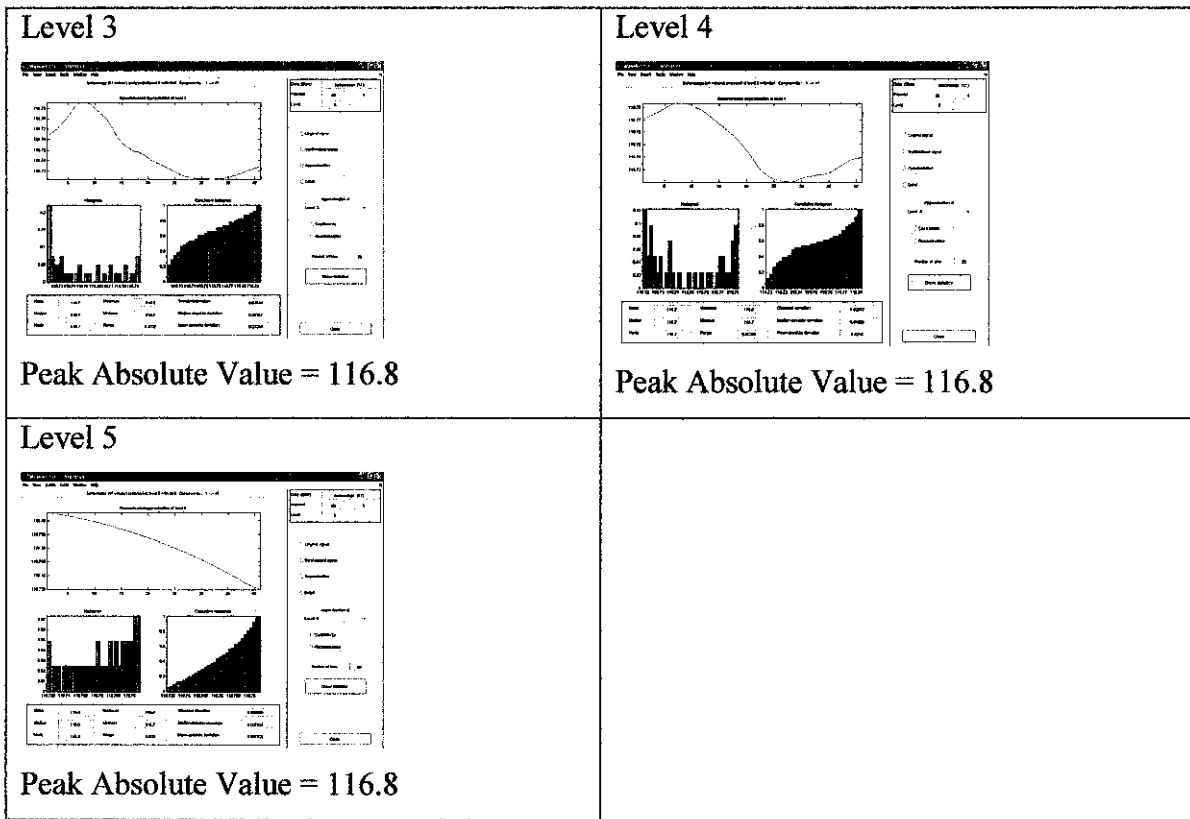
Before sag analysis



- Amplitude ratio

For approximations:





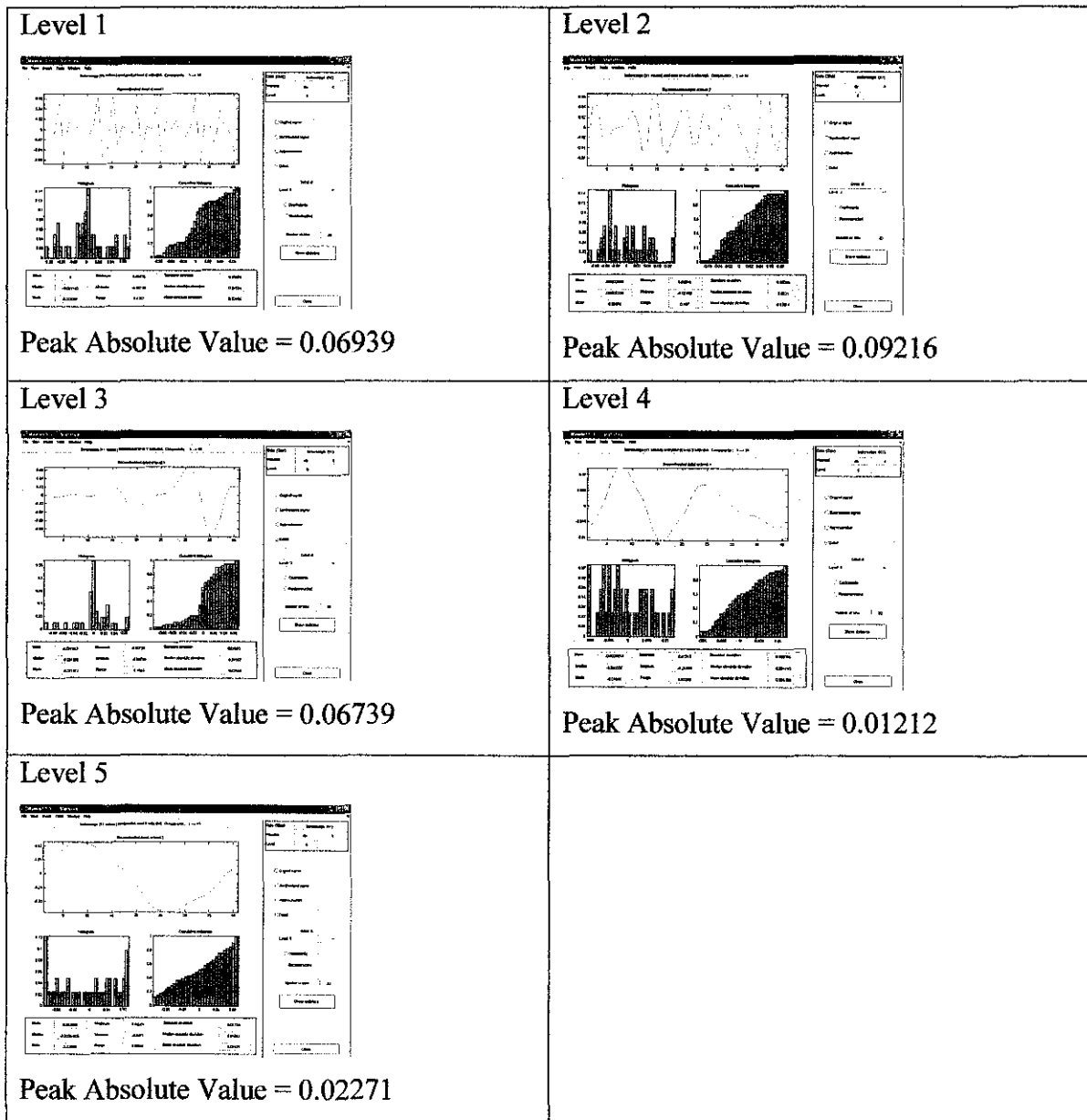
Ratio for each level of approximations:

$$\alpha_n = \frac{\text{Peak absolute value of level } n \text{ approximation}}{\text{Highest peak absolute value among the levels}}$$

Highest peak absolute value among the levels

α_n	VALUES
n=1	116.8/116.8 = 1.0000
n=2	116.8/116.8 = 1.0000
n=3	116.8/116.8 = 1.0000
n=4	116.8/116.8 = 1.0000
n=5	116.8/116.8 = 1.0000

For details:



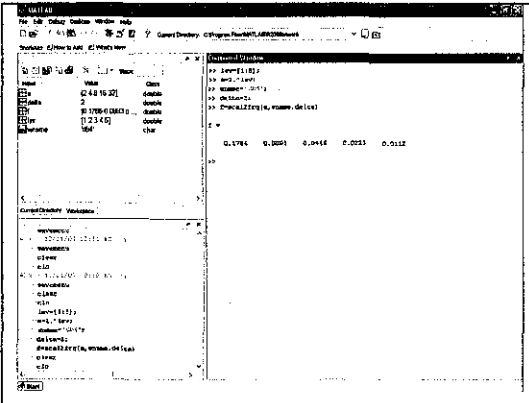
Ratio for each level of details:

$$\alpha_n = \frac{\text{Peak absolute value of level n details}}{\text{Highest peak absolute value among the levels}}$$

Highest peak absolute value among the levels

α_n	VALUES
n=1	0.06939/0.09216 = 0.7529
n=2	0.09216/0.09216 = 1.0000
n=3	0.06739/0.09216 = 0.7312
n=4	0.01212/0.09216 = 0.1315
n=5	0.02271/0.09216 = 0.2464

- Frequency



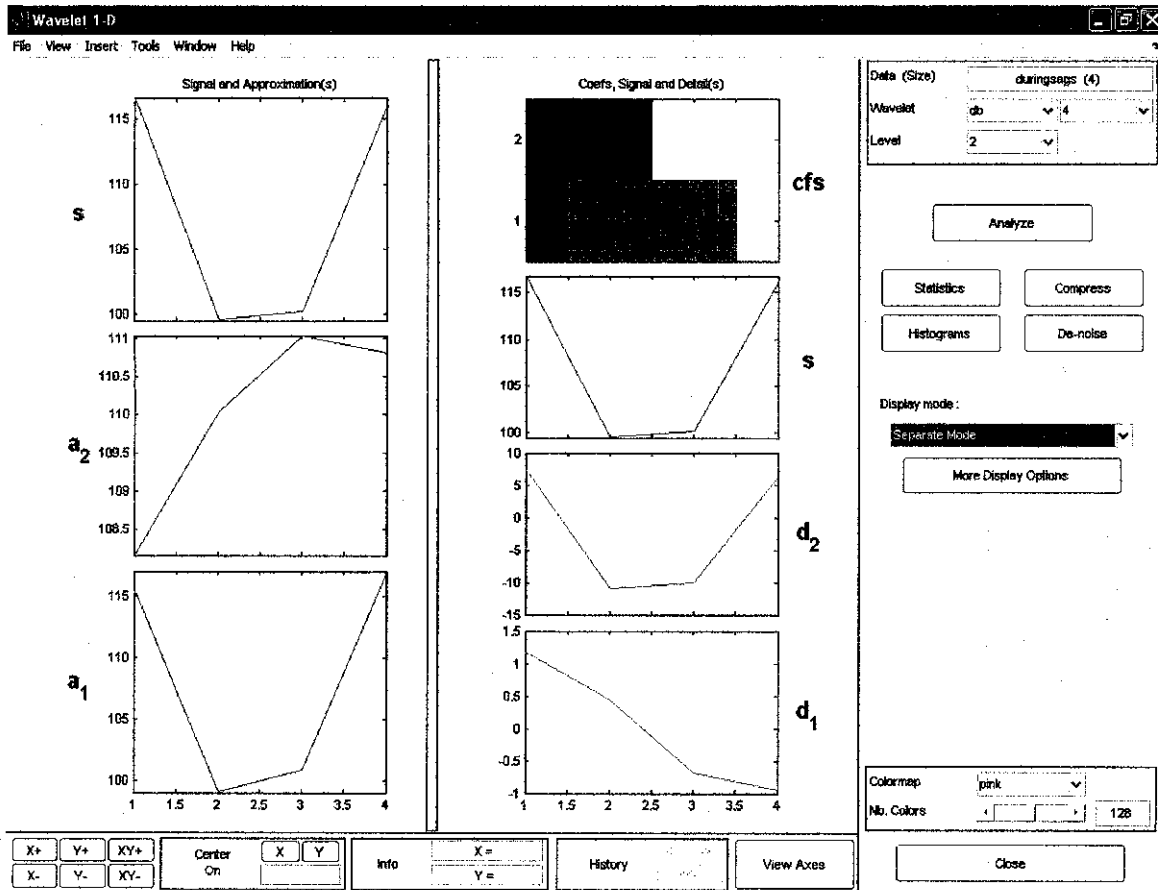
The screenshot shows a software interface with a table and a list. The table has columns 'Value' and 'Class'. The list below contains several values: 0.1786, 0.0893, 0.0446, 0.0223, 0.0112.

Result:

f =

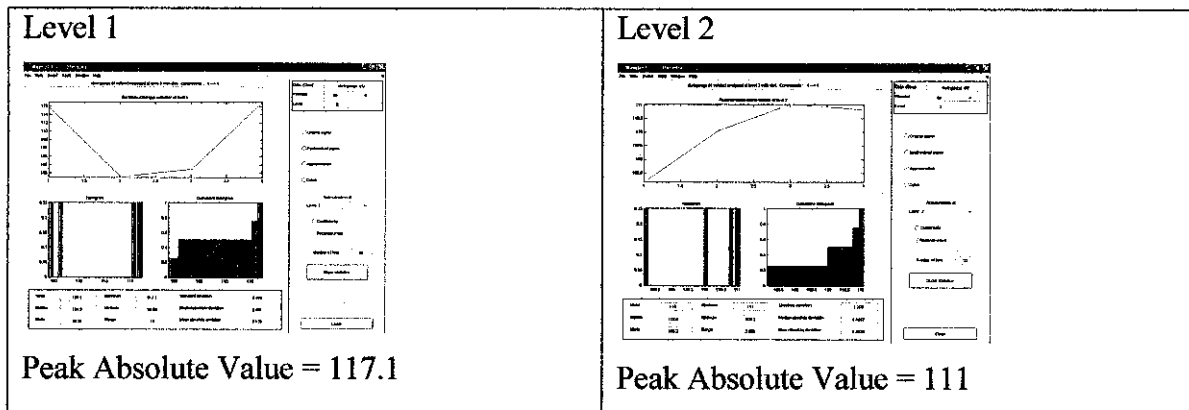
0.1786 0.0893 0.0446 0.0223 0.0112

During sag analysis



- Amplitude ratio

For approximations:



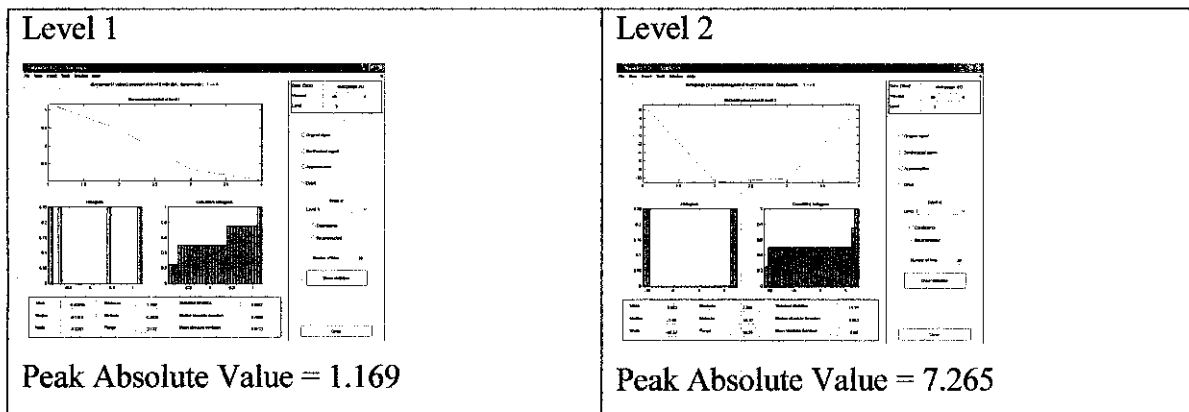
Ratio for each level of approximations:

$\alpha_n = \text{Peak absolute value of level } n \text{ approximation}$

Highest peak absolute value among the levels

α_n	VALUES
n=1	117.1/117.1 = 1.0000
n=2	111/117.1 = 0.9479

For details:



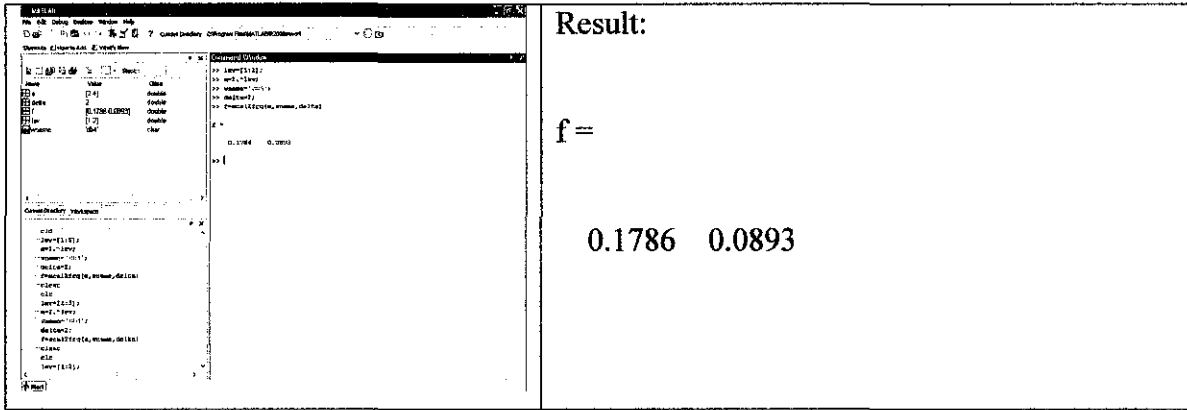
Ratio for each level of details:

$\alpha_n = \text{Peak absolute value of level } n \text{ details}$

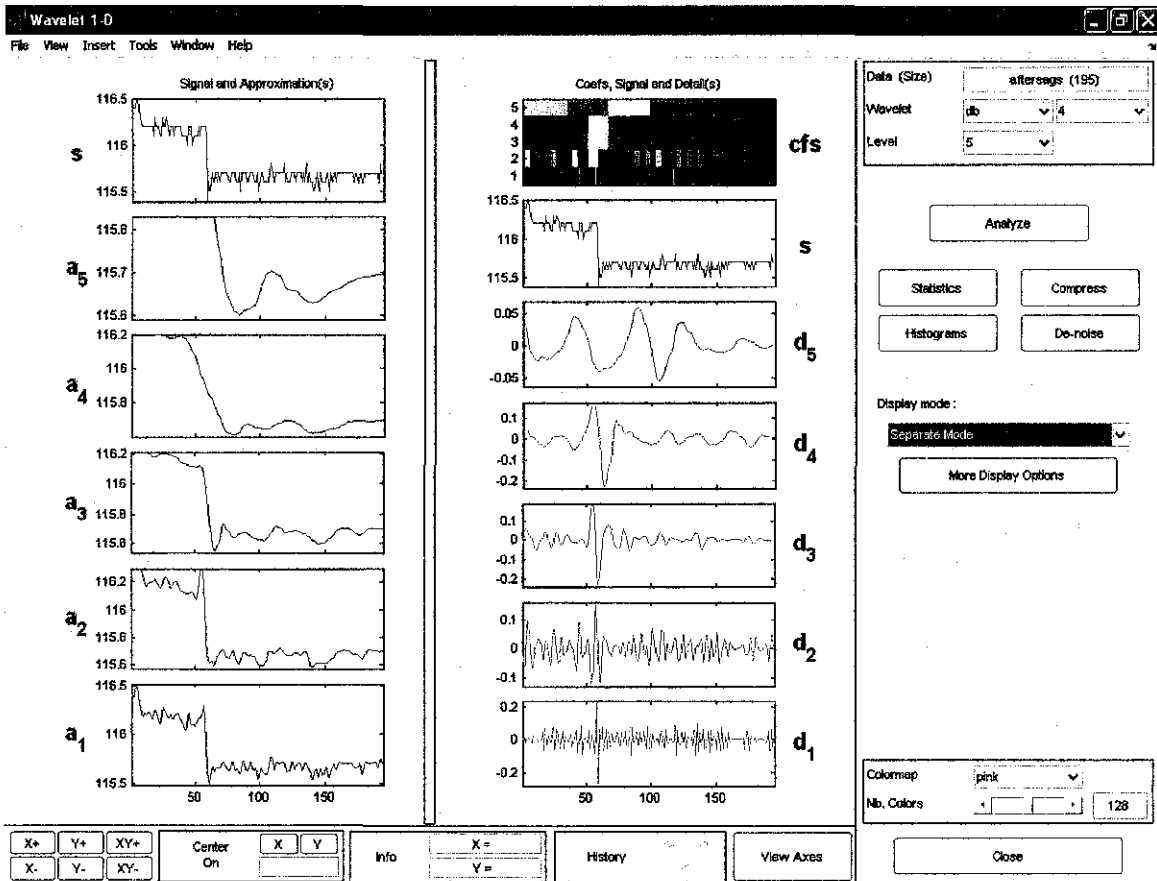
Highest peak absolute value among the levels

α_n	VALUES
n=1	1.169/7.265 = 0.1609
n=2	7.265/7.265 = 1.0000

- Frequency

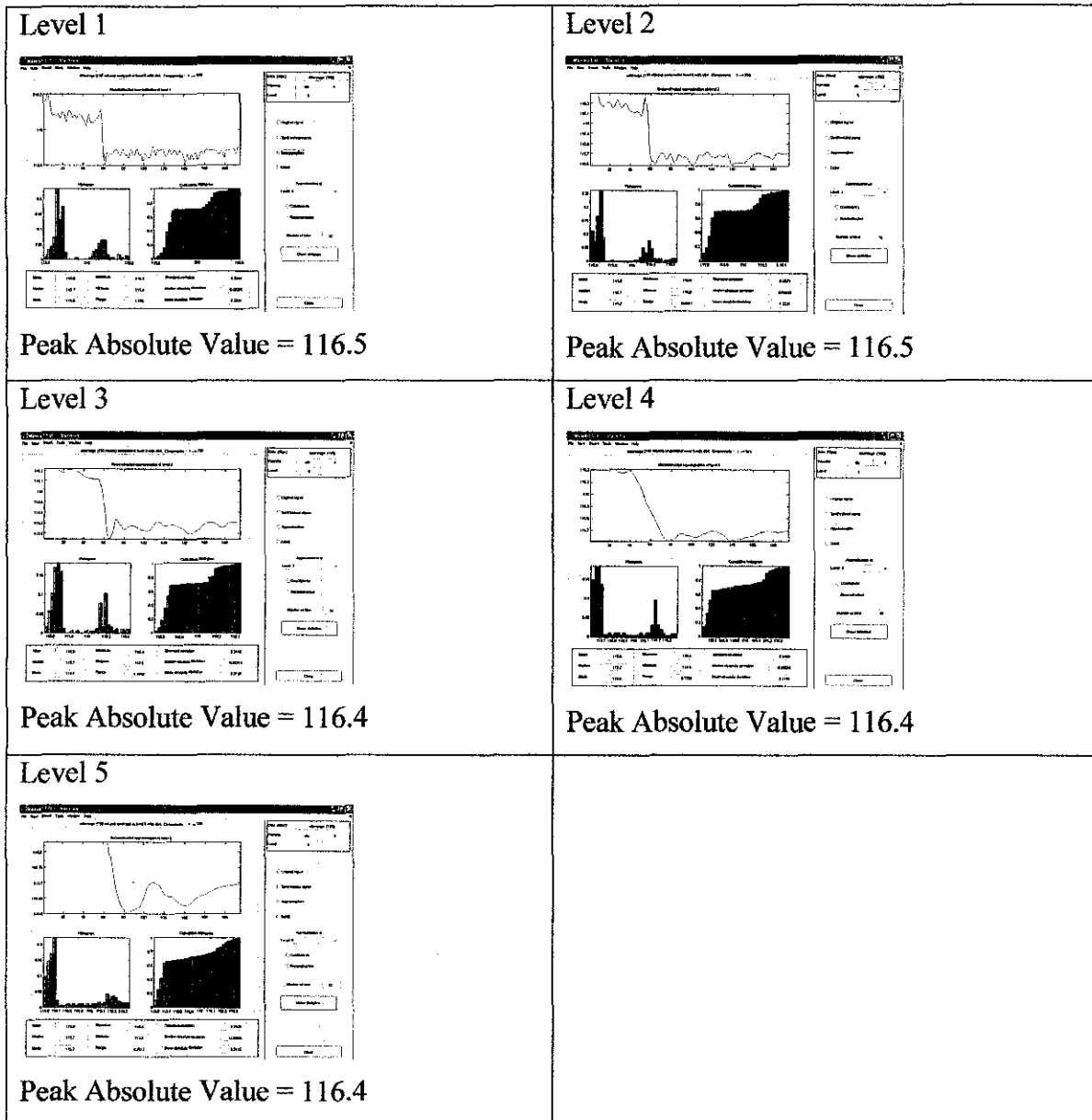


After sag analysis



- Amplitude ratio

For approximations:



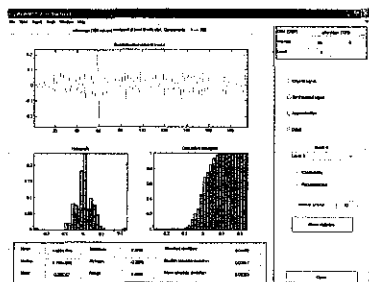
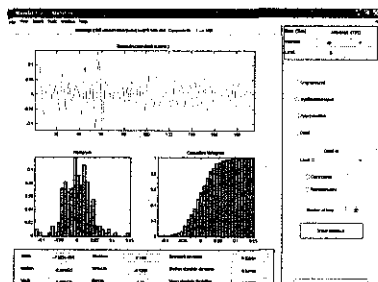
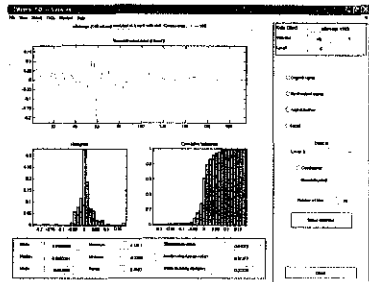
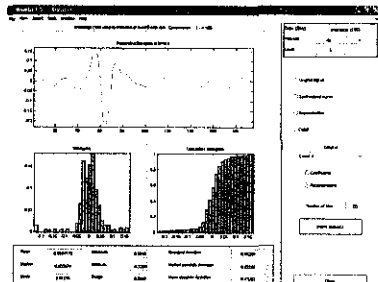
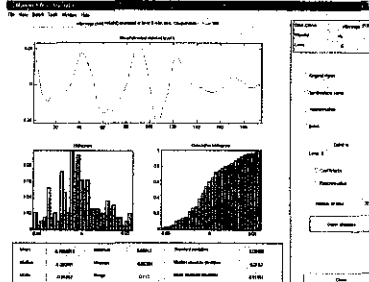
Ratio for each level of approximations:

$\alpha_n = \text{Peak absolute value of level } n \text{ approximation}$

Highest peak absolute value among the levels

α_n	VALUES
n=1	116.5/116.5 = 1.0000
n=2	116.5/116.5 = 1.0000
n=3	116.4/116.5 = 0.9991
n=4	116.4/116.5 = 0.9991
n=5	116.4/116.5 = 0.9991

For details:

<p>Level 1</p>  <p>Peak Absolute Value = 0.2306</p>	<p>Level 2</p>  <p>Peak Absolute Value = 0.149</p>
<p>Level 3</p>  <p>Peak Absolute Value = 0.1817</p>	<p>Level 4</p>  <p>Peak Absolute Value = 0.1669</p>
<p>Level 5</p>  <p>Peak Absolute Value = 0.05813</p>	

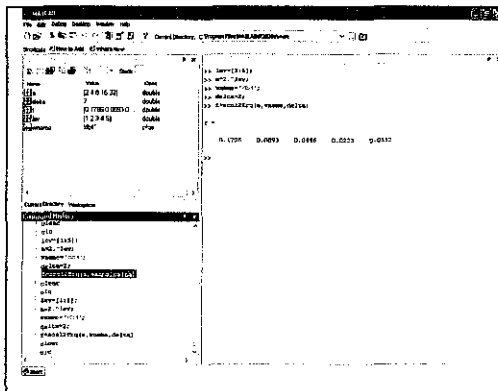
Ratio for each level of details:

$\alpha_n =$ Peak absolute value of level n details

Highest peak absolute value among the levels

α_n	VALUES
n=1	$0.2306/0.2306 = 1.0000$
n=2	$0.149/0.2306 = 0.6461$
n=3	$0.1817/0.2306 = 0.7879$
n=4	$0.1669/0.2306 = 0.7238$
n=5	$0.05813/0.2306 = 0.2521$

- Frequency



Result:

f =

0.1786 0.0893 0.0446 0.0223 0.0112

Sags due to fault

Original data:

(Phase data)

TIME (s)	VOLTAGE (V)
1	88.384
2	87.53
3	86.065
4	84.356
5	83.745
6	81.548
7	79.351
8	77.519
9	75.078
10	72.514
11	69.951
12	67.387
13	64.823
14	61.771
15	58.231
16	55.423
17	51.883
18	47.61
19	43.46
20	39.553
21	35.647
22	30.764
23	26.613
24	22.34
25	17.945
26	13.551
27	8.912
28	4.761
29	-0.244
30	-4.395
31	-8.79
32	-12.94

33	-17.335
34	-22.218
35	-25.88
36	-29.787
37	-33.816
38	-37.966
39	-42.117
40	-45.535
41	-49.197
42	-53.348
43	-56.4
44	-60.062
45	-62.748
46	-66.41
47	-68.73
48	-71.782
49	-74.467
50	-76.909
51	-79.717
52	-81.182
53	-83.745
54	-85.454
55	-87.164
56	-88.14
57	-89.239
58	-90.46
59	-91.192
60	-91.192
61	-91.68
62	-90.948
63	-90.215
64	-89.605
65	-88.628
66	-87.652

67	-86.309
68	-85.21
69	-83.501
70	-82.158
71	-79.961
72	-77.397
73	-75.566
74	-73.125
75	-70.439
76	-66.41
77	-65.067
78	-61.893
79	-58.719
80	-55.423
81	-51.273
82	-47.854
83	-43.582
84	-38.821
85	-34.67
86	-30.642
87	-26.491
88	-20.997
89	-18.434
90	-13.551
91	-9.156
92	-4.273
93	-0.488
94	4.273
95	9.278
96	14.283
97	17.823
98	21.73
99	25.758
100	30.275

101	34.426
102	38.088
103	42.483
104	46.878
105	49.93
106	54.08
107	56.888
108	60.184
109	62.626
110	65.922
111	68.852
112	71.782
113	74.59
114	76.909
115	78.984
116	80.083
117	79.961
118	78.74
119	75.81
120	73.003
121	70.439
122	70.317
123	70.073
124	70.927
125	69.951
126	70.439
127	70.073
128	70.195
129	69.584
130	67.753
131	66.654
132	64.945
133	63.358
134	61.893
135	61.649
136	61.527
137	61.405
138	61.405
139	60.917
140	60.062
141	58.353

142	56.034
143	52.738
144	50.784
145	47.61
146	45.535
147	42.605
148	39.675
149	36.623
150	32.473
151	26.247
152	20.021
153	12.452
154	5.249
155	-0.977
156	-6.226
157	-10.255
158	-13.184
159	-16.358
160	-19.166
161	-22.096
162	-25.026
163	-27.59
164	-30.275
165	-33.327
166	-36.501
167	-39.553
168	-42.117
169	-43.338
170	-44.314
171	-44.558
172	-44.925
173	-45.779
174	-47.488
175	-49.686
176	-52.249
177	-53.958
178	-56.522
179	-57.499
180	-57.743
181	-58.231
182	-59.33

183	-60.428
184	-61.771
185	-62.748
186	-64.457
187	-64.823
188	-64.335
189	-64.579
190	-63.847
191	-63.603
192	-62.138
193	-61.527
194	-60.551
195	-59.33
196	-57.743
197	-55.667
198	-54.935
199	-53.714
200	-52.127
201	-50.906
202	-49.319
203	-47.61
204	-44.803
205	-42.483
206	-40.896
207	-38.088
208	-35.647
209	-33.693
210	-31.496
211	-28.566
212	-25.514
213	-22.34
214	-20.021
215	-16.236
216	-12.94
217	-10.01
218	-8.057
219	-3.906
220	-0.488
221	2.808
222	6.226
223	9.522

224	13.429
225	15.748
226	18.434
227	21.486
228	24.416
229	27.467
230	30.153
231	32.473
232	35.891
233	37.112
234	39.553
235	41.262
236	43.338
237	45.291
238	46.756
239	48.465
240	49.441
241	51.517
242	53.104
243	53.958
244	55.057
245	56.156
246	56.156
247	57.865
248	59.086
249	59.818
250	60.428
251	60.551
252	61.283
253	61.405
254	60.795
255	60.306
256	60.917
257	60.428
258	60.673
259	58.475
260	57.987
261	56.644
262	55.057
263	53.958
264	52.86

265	50.662
266	49.075
267	46.756
268	44.803
269	42.483
270	40.53
271	38.21
272	35.647
273	33.083
274	30.275
275	27.834
276	24.538
277	21.974
278	19.288
279	16.114
280	13.306
281	10.743
282	7.569
283	4.761
284	1.953
285	-0.977
286	-4.029
287	-6.714
288	-10.377
289	-12.94
290	-15.748
291	-17.945
292	-21.119
293	-23.683
294	-26.003
295	-28.688
296	-31.252
297	-33.816
298	-35.647
299	-38.332
300	-40.774
301	-42.361
302	-44.68
303	-45.535
304	-48.465
305	-49.686

306	-51.273
307	-52.982
308	-54.447
309	-55.912
310	-56.766
311	-57.743
312	-58.597
313	-60.062
314	-59.696
315	-60.062
316	-60.551
317	-60.306
318	-59.818
319	-59.208
320	-59.086
321	-57.377
322	-57.377
323	-56.4
324	-55.179
325	-53.836
326	-52.249
327	-51.029
328	-49.564
329	-47.732
330	-45.901
331	-44.558
332	-42.239
333	-39.919
334	-37.356
335	-35.403
336	-34.06
337	-31.984
338	-30.153
339	-28.81
340	-26.979
341	-24.782
342	-22.462
343	-20.387
344	-18.312
345	-14.771
346	-11.475

347	-9.644
348	-6.592
349	-3.906
350	-1.099
351	1.221
352	5.005
353	8.545
354	11.597
355	14.649
356	17.823
357	21.119
358	24.66
359	28.2
360	31.008
361	34.182
362	36.867
363	39.553
364	41.629
365	44.314
366	46.756
367	49.319
368	51.761
369	54.691
370	56.888
371	59.33
372	60.306
373	61.771
374	62.87
375	63.725
376	65.067
377	66.166
378	67.631
379	68.73
380	69.462
381	69.828
382	70.561
383	70.683
384	70.317
385	70.073
386	69.096
387	68.364

388	67.509
389	66.899
390	65.8
391	64.945
392	63.603
393	62.626
394	60.428
395	58.841
396	56.4
397	53.958
398	52.005
399	49.93
400	49.197
401	48.221
402	46.634
403	43.826
404	41.629
405	37.966
406	34.304
407	30.031
408	25.88
409	21.608
410	17.457
411	13.795
412	10.377
413	6.958
414	2.808
415	-1.465
416	-5.493
417	-9.766
418	-14.283
419	-18.312
420	-22.829
421	-27.59
422	-30.153
423	-33.816
424	-36.623
425	-40.53
426	-43.338
427	-47.122
428	-51.151

429	-54.447
430	-57.499
431	-60.673
432	-62.504
433	-65.312
434	-67.387
435	-69.706
436	-72.27
437	-75.322
438	-77.275
439	-78.984
440	-81.304
441	-82.769
442	-82.769
443	-83.99
444	-83.99
445	-84.234
446	-84.722
447	-84.722
448	-84.6
449	-83.379
450	-82.402
451	-81.548
452	-80.693
453	-79.595
454	-78.374
455	-76.787
456	-75.078
457	-73.735
458	-71.171
459	-69.218
460	-66.41
461	-64.091
462	-61.161
463	-57.987
464	-54.691
465	-51.517
466	-47.732
467	-43.093
468	-39.431
469	-35.769

470	-31.74
471	-27.467
472	-22.829
473	-18.8
474	-15.138
475	-11.231
476	-6.836
477	-2.93
478	1.831
479	6.104
480	10.377
481	14.161
482	18.8
483	23.073
484	27.345
485	31.13
486	36.135
487	38.943
488	42.361
489	45.901
490	49.564
491	51.517
492	56.888
493	59.696
494	62.626
495	64.823
496	67.387
497	70.195
498	72.392
499	74.834
500	76.665
501	78.374
502	80.205
503	82.158
504	83.379
505	84.112
506	84.844
507	85.332
508	85.699
509	85.943
510	85.454

511	85.21
512	84.6
513	83.623
514	82.891
515	81.548
516	80.571
517	79.228
518	77.764
519	76.543
520	74.101
521	72.27
522	70.561
523	67.143
524	65.8
525	62.748
526	59.574
527	56.156
528	52.738
529	48.953
530	45.535
531	41.873
532	38.088
533	33.327
534	29.177
535	25.026
536	20.753
537	16.969
538	12.818
539	9.156
540	4.883
541	0.732
542	-2.197
543	-7.203
544	-11.109
545	-16.236
546	-20.021
547	-23.927
548	-27.834
549	-31.984
550	-36.135
551	-39.553

552	-42.849
553	-46.878
554	-50.784
555	-54.325
556	-57.254
557	-60.917
558	-62.87
559	-66.532
560	-70.195
561	-71.904
562	-73.857
563	-76.665
564	-78.862
565	-80.693
566	-83.501
567	-84.356
568	-85.21
569	-86.797
570	-87.652
571	-87.652
572	-87.408
573	-87.896
574	-87.774
575	-87.286
576	-86.187
577	-85.821
578	-84.722
579	-83.257
580	-82.402
581	-80.938
582	-79.228
583	-77.275
584	-75.2
585	-73.735
586	-71.049
587	-68.852
588	-66.166
589	-63.358
590	-60.428
591	-57.01
592	-53.226

593	-50.174
594	-46.267
595	-42.361
596	-37.966
597	-33.816
598	-29.299
599	-25.27
600	-20.875
601	-17.213
602	-12.696
603	-8.301
604	-4.273
605	-0.122
606	4.273
607	8.79
608	12.696
609	17.213
610	21.608
611	26.491
612	30.031
613	33.571
614	37.6
615	41.873
616	45.047
617	49.686
618	52.738
619	56.278
620	58.841
621	62.138
622	65.434
623	69.096
624	70.561
625	73.369
626	76.054
627	78.13
628	80.327
629	82.402
630	83.867
631	85.088
632	86.187
633	87.164

634	88.384
635	88.995
636	88.751
637	88.262
638	89.117
639	87.774
640	87.164
641	86.065
642	84.722
643	83.623
644	82.647
645	80.693
646	79.473
647	78.008
648	75.81
649	74.223
650	71.66
651	69.34
652	66.41
653	63.847
654	60.795
655	57.499
656	53.592
657	49.686
658	46.39
659	41.995
660	38.21
661	33.571
662	29.543
663	25.27
664	20.875
665	16.847
666	12.818
667	7.935
668	3.296
669	-1.587
670	-5.005
671	-9.522
672	-14.039
673	-18.434
674	-22.462

675	-25.88
676	-30.275
677	-34.182
678	-38.699
679	-42.483
680	-46.023
681	-49.564
682	-53.348
683	-56.888
684	-60.184
685	-63.236
686	-66.288
687	-69.218
688	-71.904
689	-74.834
690	-76.909
691	-79.473
692	-81.304
693	-83.257
694	-84.6
695	-86.553
696	-87.652
697	-88.995
698	-89.483
699	-90.093
700	-90.093
701	-90.582
702	-89.605
703	-88.751
704	-88.262
705	-87.286
706	-86.187
707	-84.844
708	-83.867
709	-82.402
710	-80.449
711	-79.228
712	-76.299
713	-74.712
714	-72.026
715	-69.462

716	-66.777
717	-63.847
718	-59.94
719	-56.766
720	-53.104
721	-49.319
722	-44.925
723	-41.384
724	-37.112
725	-32.106
726	-27.956
727	-23.805
728	-19.41
729	-15.016
730	-10.621
731	-6.714
732	-2.564
733	1.709
734	6.47
735	10.255
736	14.649
737	18.8
738	23.439
739	27.956
740	31.984
741	36.135
742	40.408
743	44.314
744	47.854
745	52.249
746	55.179
747	57.377
748	62.138
749	64.701
750	67.753
751	70.439
752	73.491
753	75.688
754	78.496
755	80.571
756	82.402

757	84.478
758	85.699
759	87.53
760	88.628
761	89.117
762	90.582
763	90.093
764	90.215
765	91.07
766	89.849
767	89.239
768	88.14
769	86.675
770	86.187
771	84.966
772	83.745
773	80.938
774	80.449
775	78.13
776	76.177
777	74.223
778	72.758
779	68.608
780	65.678
781	63.48
782	59.818
783	56.4
784	52.982
785	48.953
786	45.169
787	40.774
788	36.867
789	32.351
790	28.322
791	23.683
792	20.021
793	15.504
794	10.865
795	6.348
796	2.075
797	-2.442

798	-6.592
799	-11.475
800	-15.504
801	-20.387
802	-24.171
803	-27.956
804	-32.229
805	-36.745
806	-40.408
807	-44.314
808	-48.343
809	-51.639
810	-55.79
811	-59.452
812	-62.26
813	-64.945
814	-67.387
815	-71.171
816	-74.345
817	-76.909
818	-79.106
819	-81.06
820	-83.257
821	-85.21
822	-86.919
823	-88.751
824	-89.361
825	-90.704
826	-91.436
827	-92.535
828	-91.436
829	-90.826
830	-90.582
831	-89.971
832	-89.605
833	-88.384
834	-87.164
835	-85.821
836	-83.135
837	-82.28
838	-80.693

839	-78.984
840	-76.421
841	-74.223
842	-71.904
843	-68.974
844	-66.044
845	-62.87
846	-59.452
847	-56.156
848	-51.517
849	-48.709
850	-44.436
851	-39.431
852	-35.403
853	-31.496
854	-26.247
855	-22.096
856	-17.945
857	-13.673
858	-9.034
859	-4.883
860	0
861	4.029
862	8.423
863	12.696
864	18.19
865	22.34
866	25.636
867	30.153
868	34.67
869	38.577
870	42.361
871	46.145
872	50.296
873	53.836
874	57.621
875	59.33
876	63.969
877	66.532
878	69.584
879	71.904

880	75.078
881	77.397
882	79.106
883	81.548
884	83.257
885	85.577
886	86.919
887	87.652
888	89.605
889	90.215
890	90.826
891	90.948
892	91.436
893	90.826
894	90.215
895	89.849
896	89.361
897	87.774
898	86.919
899	85.332
900	84.356
901	82.402
902	80.205
903	78.008
904	76.421
905	73.613
906	71.293
907	67.143
908	65.922
909	63.847
910	59.574
911	55.912
912	52.371
913	48.343
914	44.314
915	40.164
916	35.28
917	31.496
918	27.223
919	22.951
920	19.166

921	14.039
922	10.01
923	5.371
924	0.855
925	-3.54
926	-7.447
927	-12.208
928	-16.358
929	-21.242
930	-25.27
931	-29.299
932	-33.938
933	-37.844
934	-41.873
935	-45.535
936	-49.564
937	-53.47
938	-57.132
939	-60.306
940	-64.213
941	-67.387
942	-69.096
943	-72.636
944	-75.078
945	-78.252
946	-80.449
947	-82.402
948	-84.6
949	-86.675
950	-88.384
951	-89.361
952	-90.582
953	-91.436
954	-91.925
955	-92.169
956	-92.047
957	-91.925
958	-91.68
959	-91.07
960	-89.849
961	-88.628

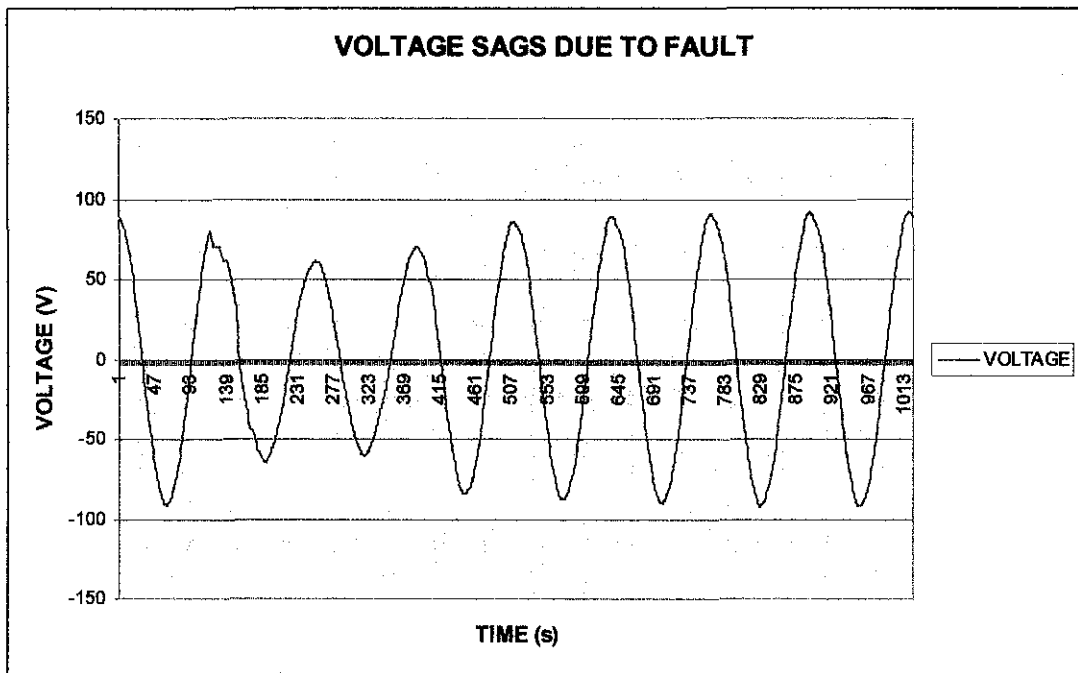
962	-88.018
963	-86.187
964	-84.722
965	-83.013
966	-81.06
967	-78.984
968	-77.397
969	-74.59
970	-72.148
971	-68.608
972	-65.922
973	-62.748
974	-59.574
975	-55.667
976	-52.249
977	-48.465
978	-43.948
979	-39.553
980	-34.914
981	-31.008
982	-26.491
983	-22.096
984	-17.945
985	-13.551
986	-8.668
987	-4.151
988	-0.366
989	4.395
990	9.034
991	13.795
992	17.701
993	22.584
994	26.735
995	32.106
996	35.158
997	39.431
998	43.704
999	48.343
1000	51.395
1001	54.691
1002	58.475

1003	61.893
1004	65.067
1005	67.509
1006	70.561
1007	73.491
1008	75.322
1009	78.252
1010	80.693
1011	82.647
1012	84.356
1013	86.675
1014	88.14
1015	89.605
1016	90.215
1017	90.704
1018	91.802
1019	92.169
1020	92.169
1021	91.436
1022	91.192
1023	90.46
1024	88.995

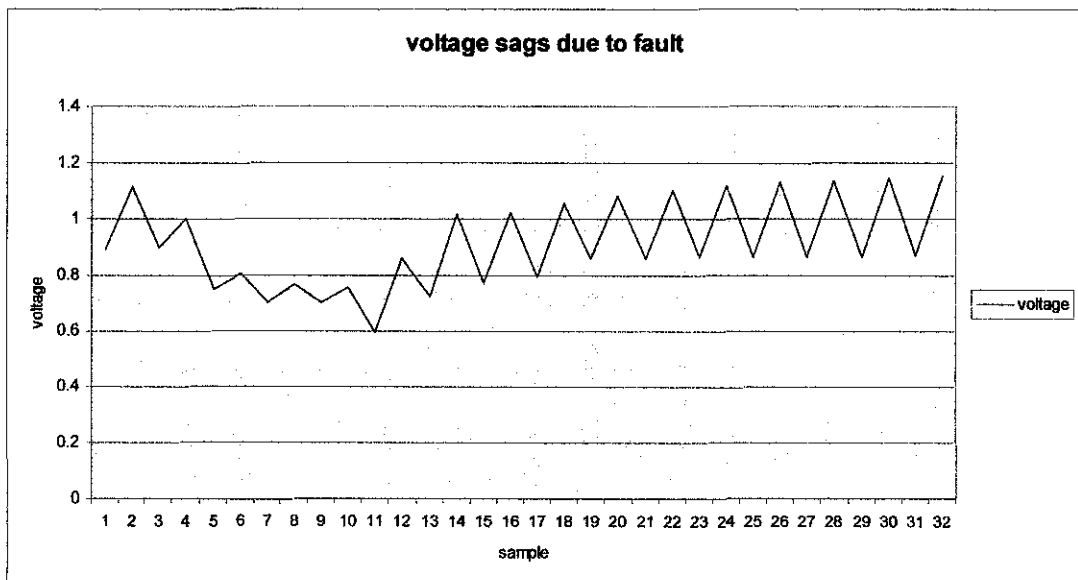
(RMS data)

SAMPLE	VOLTAGE (V)
1	0.89337
2	1.115206
3	0.895284
4	0.99767
5	0.752208
6	0.806516
7	0.703378
8	0.764938
9	0.703252
10	0.757076
11	0.594659
12	0.861931
13	0.725085
14	1.016431
15	0.775597
16	1.022585
17	0.792094
18	1.052274
19	0.859348
20	1.080928
21	0.862052
22	1.104236
23	0.864259
24	1.117027
25	0.864004
26	1.128211
27	0.866498
28	1.134642
29	0.864184
30	1.14787
31	0.870611

Plot:



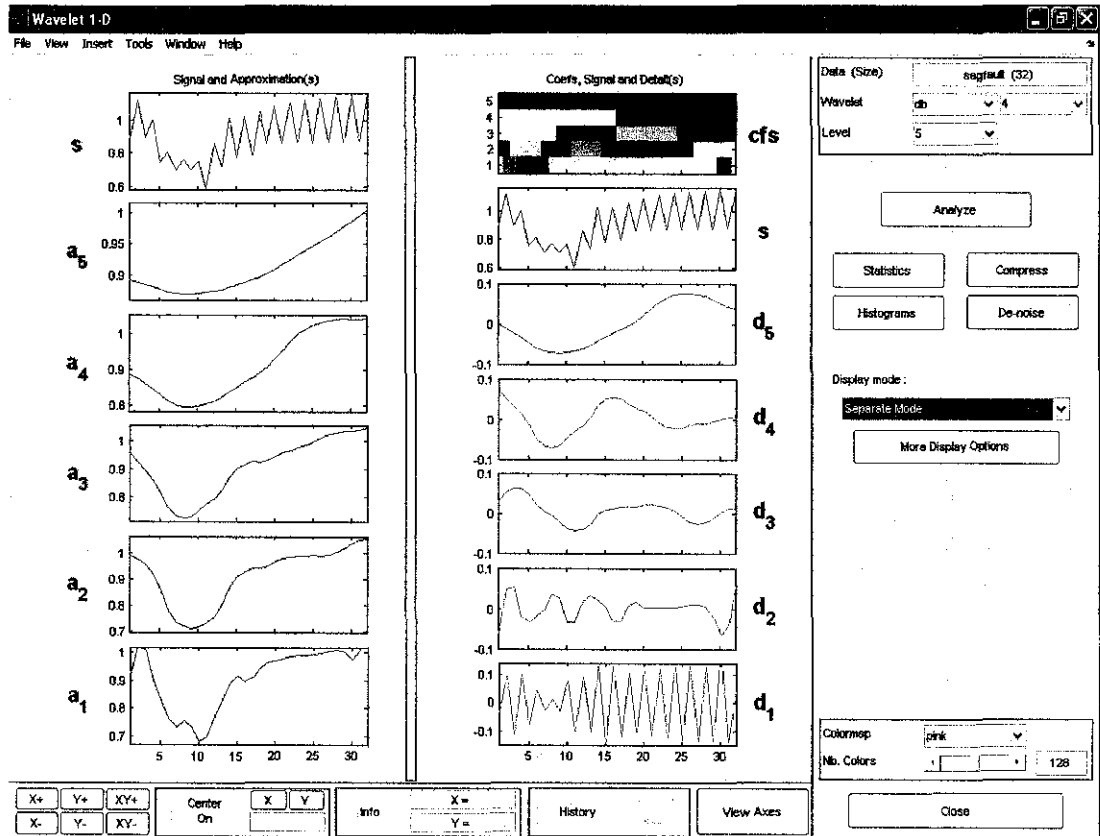
Waveform for instantaneous values



Waveform for RMS values

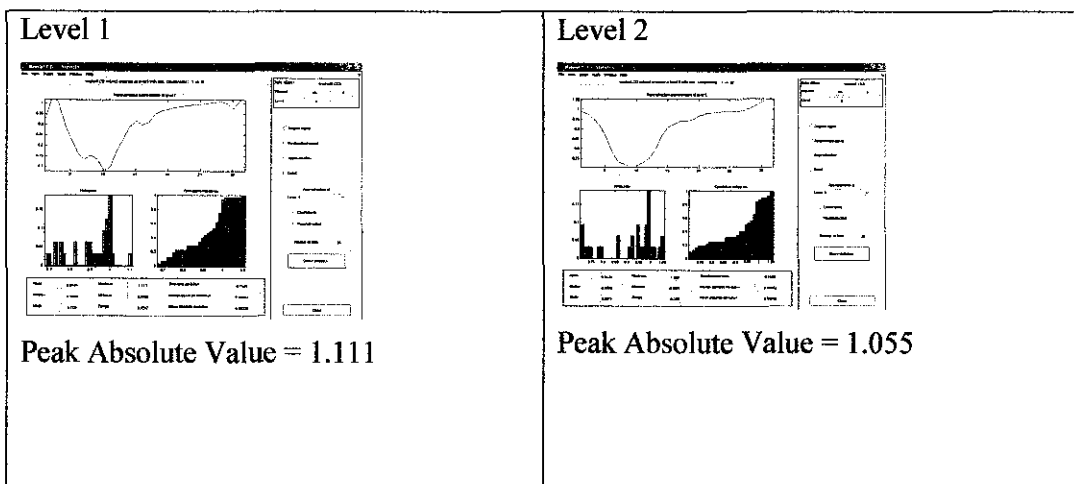
Wavelet Analysis:

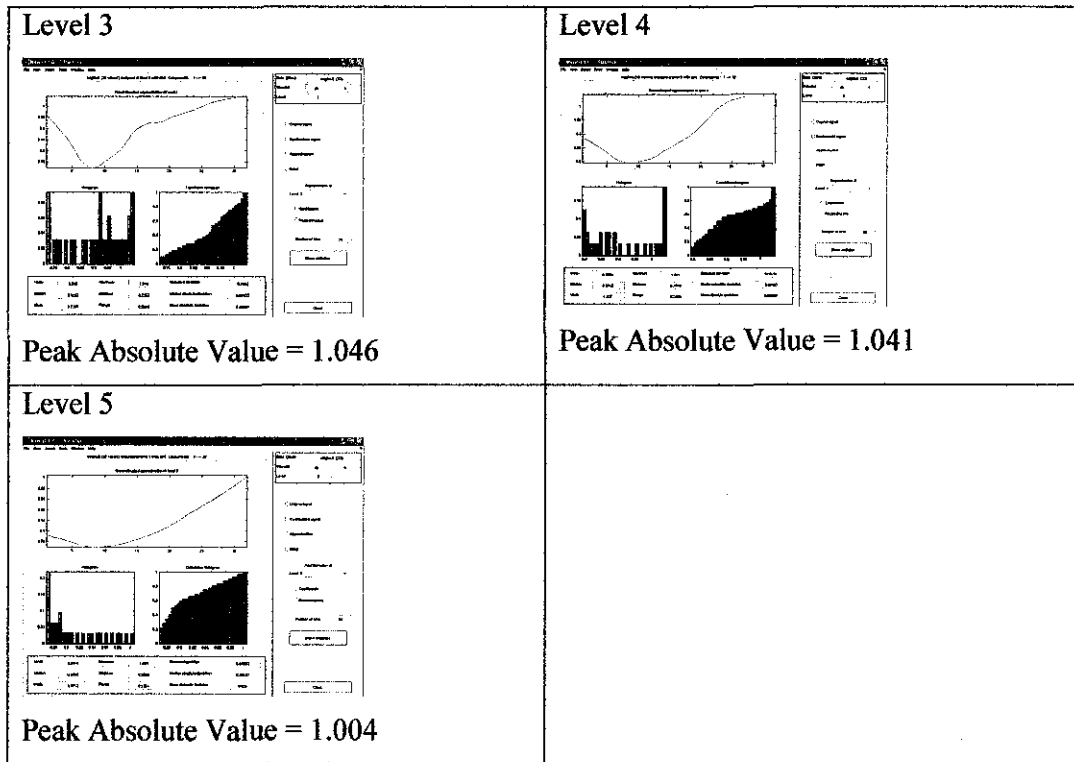
Whole waveform analysis



- Amplitude ratio

For approximations:



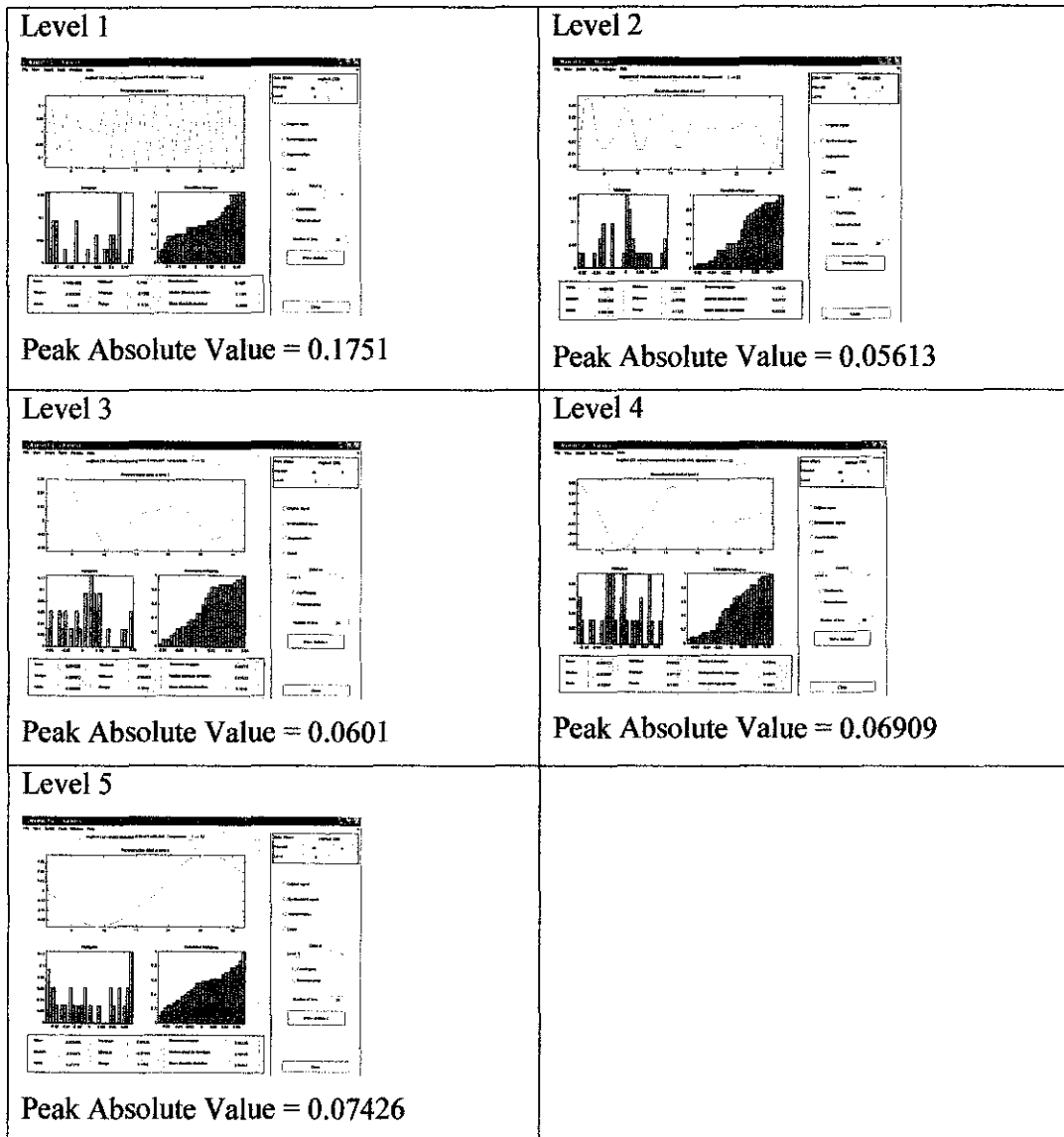


Ratio for each level of approximations:

$\alpha_n = \frac{\text{Peak absolute value of level n approximation}}{\text{Highest peak absolute value among the levels}}$

α_n	VALUES
n=1	1.111/1.111 = 1.0000
n=2	1.055/1.111 = 0.9496
n=3	1.046/1.111 = 0.9415
n=4	1.041/1.111 = 0.9370
n=5	1.004/1.111 = 0.9037

For details:



Ratio for each level of details:

$\alpha_n = \frac{\text{Peak absolute value of level n details}}{\text{Highest peak absolute value among the levels}}$

Highest peak absolute value among the levels

α_n	VALUES
n=1	0.1751/0.1751 = 1.0000
n=2	0.05613/0.1751 = 0.3206
n=3	0.0601/0.1751 = 0.3432
n=4	0.06909/0.1751 = 0.3946
n=5	0.07426/0.1751 = 0.4241

- Frequency

<pre> >> [cfs, s, a1, d1] = wavedec(fault_before_sag, 4, 'db4'); </pre>	<p>Result:</p> <p>f =</p> <p>0.3571 0.1786 0.0893 0.0446</p> <p>0.0223</p>
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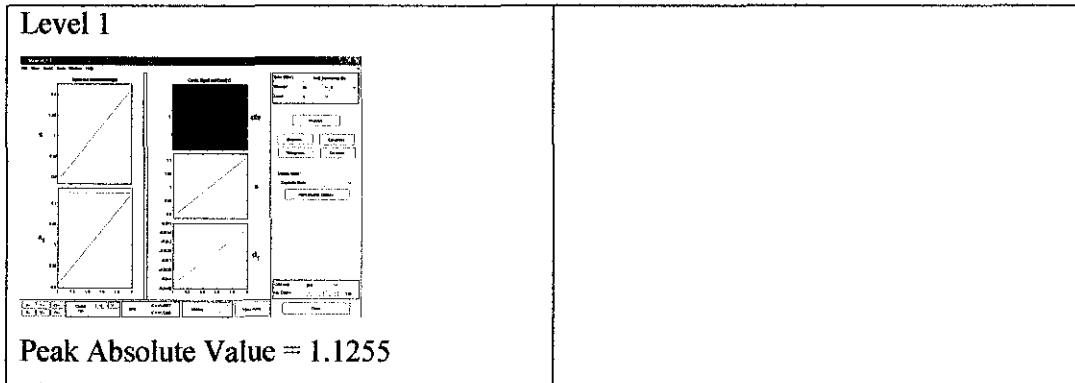
Before sag analysis

The interface displays the following components:

- Signal and Approximation(s):** Two vertically stacked plots. The top plot shows the original signal s and its approximation a_1 over the range [1, 2]. Both plots show a linear increase from approximately 0.9 to 1.1.
- Coefs, Signal and Detail(s):** A central area containing:
 - A dark square representing the coefficient matrix cfs .
 - A plot of the signal s .
 - A plot of the detail coefficient d_1 , showing values ranging from -0.0145 to 0.011.
- Control Panel (Right):**
 - File: fault_before_sag (2)
 - Wavelet: db, Level: 4
 - Buttons: Analyze, Statistics, Compress, Histograms, De-noise
 - Display mode: Separate Mode
 - Colormap: pink, No. Colors: 128
 - Close button
- Bottom Toolbar:** X+, Y+, XY+, X-, Y-, XY-, Center On, Info, X=, Y=, History, View Axes

- Amplitude ratio

For approximations:

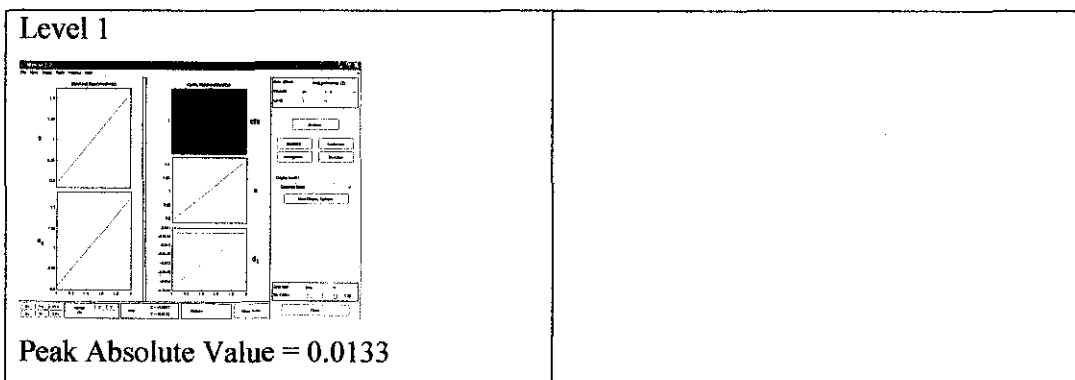


Ratio for each level of approximations:

$\alpha_n = \frac{\text{Peak absolute value of level n approximation}}{\text{Highest peak absolute value among the levels}}$

α_n	VALUES
n=1	1.1255/1.1255 = 1.0000

For details:



Ratio for each level of details:

$\alpha_n = \frac{\text{Peak absolute value of level n details}}{\text{Highest peak absolute value among the levels}}$

α_n	VALUES
$n=1$	$0.0133/0.0133 = 1.0000$

- Frequency

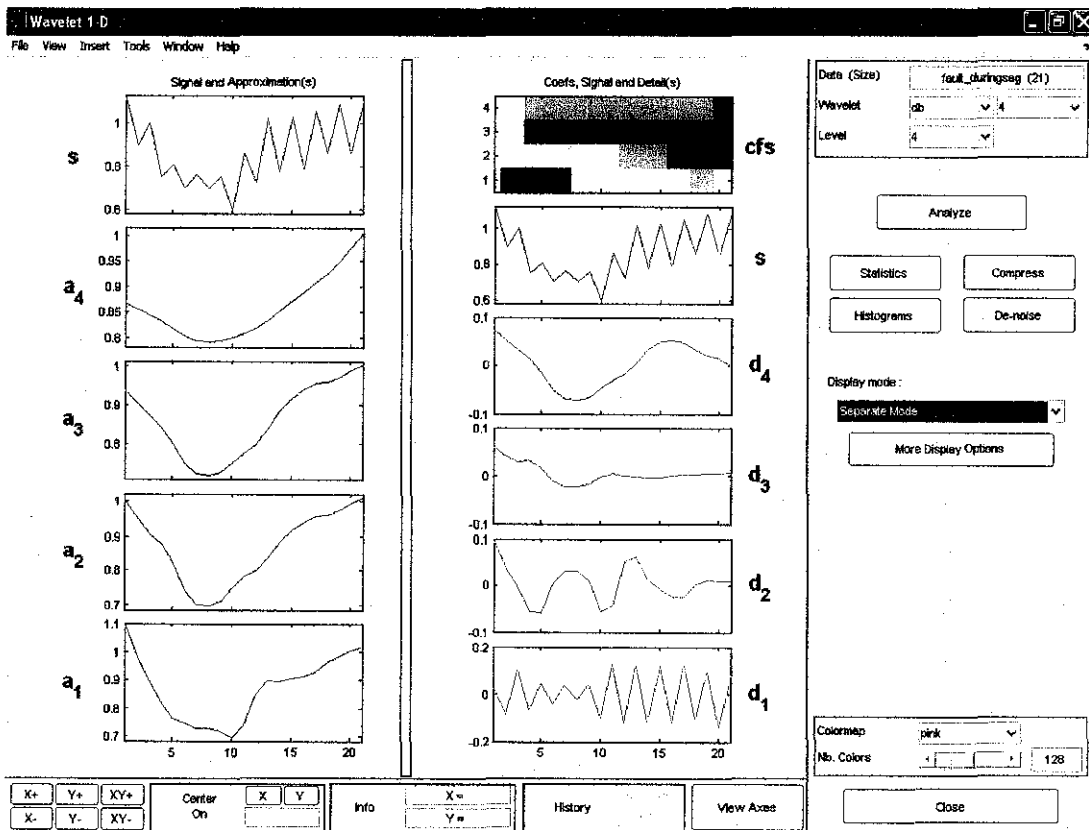
Name	Value	Class	Unit
f	0.3571	double	

Result:

f =

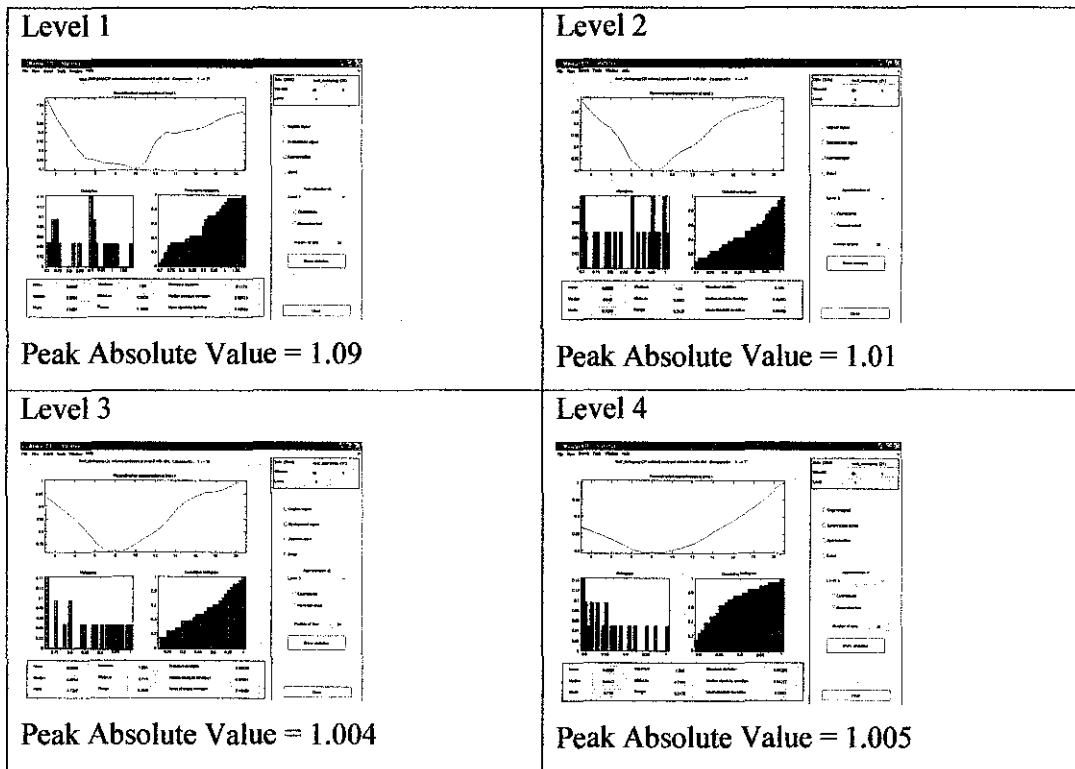
0.3571

During sag analysis



- Amplitude ratio

For approximations:



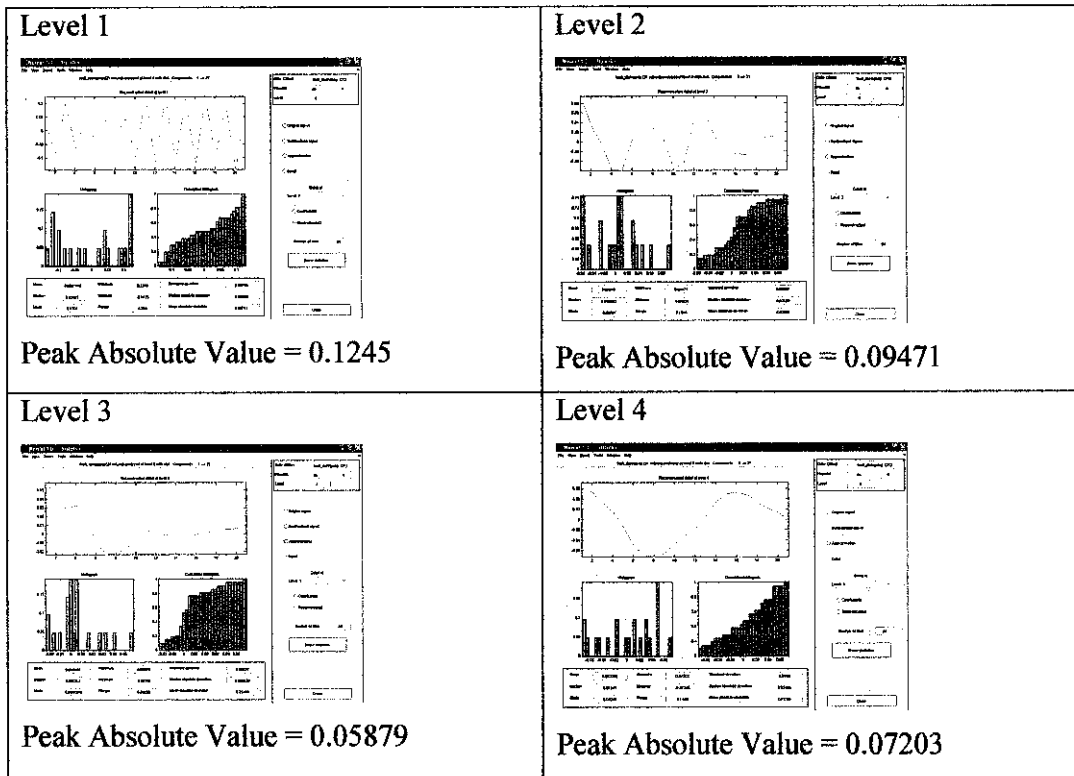
Ratio for each level of approximations:

$\alpha_n = \text{Peak absolute value of level } n \text{ approximation}$

Highest peak absolute value among the levels

α_n	VALUES
n=1	1.09/1.09 = 1.0000
n=2	1.01/1.09 = 0.9266
n=3	1.004/1.09 = 0.9211
n=4	1.005/1.09 = 0.9220

For details:



Ratio for each level of details:

$\alpha_n = \text{Peak absolute value of level n details}$

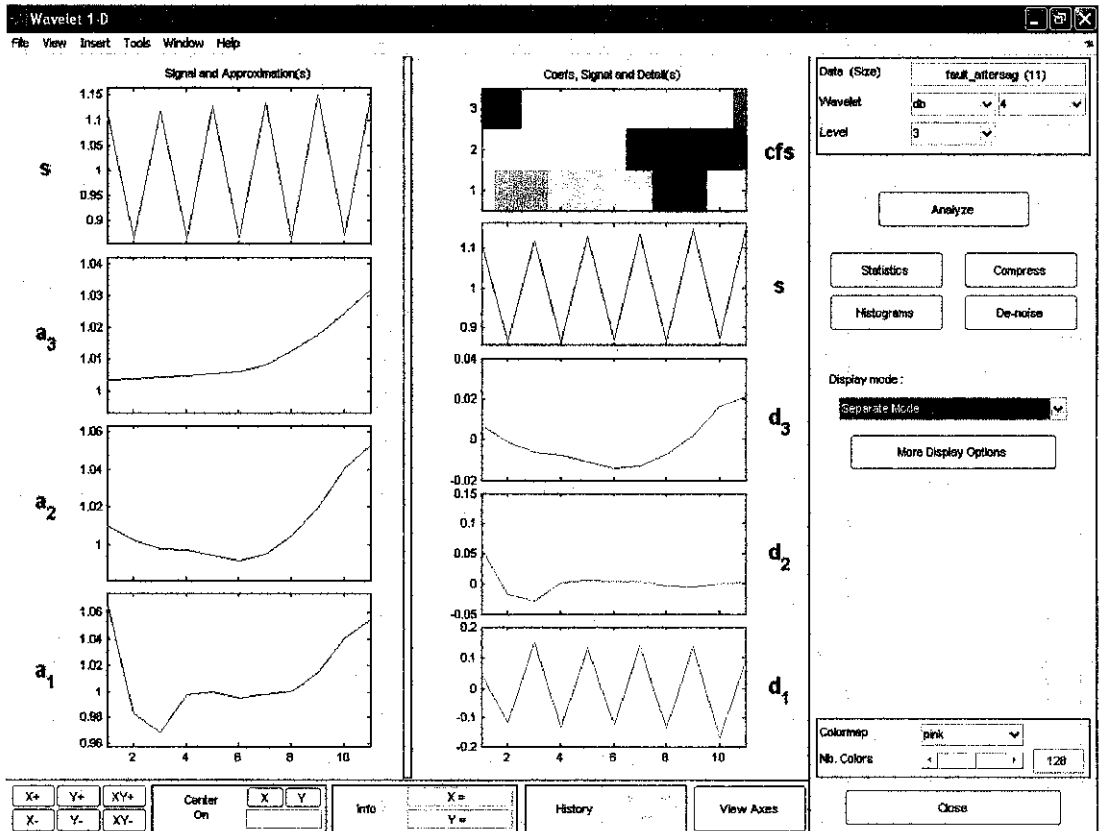
Highest peak absolute value among the levels

α_n	VALUES
n=1	$0.1245/0.1245 = 1.0000$
n=2	$0.09471/0.1245 = 0.7607$
n=3	$0.05879/0.1245 = 0.4722$
n=4	$0.07203/0.1245 = 0.5786$

- Frequency

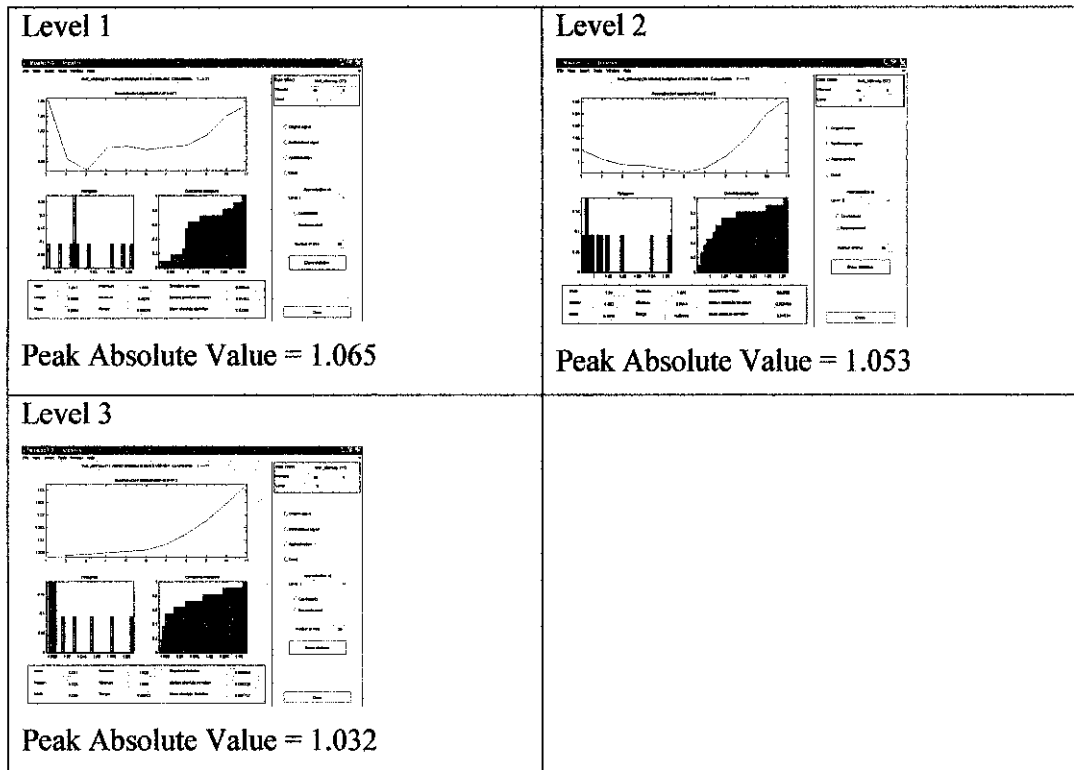
	<p>Result:</p> <p>$f =$</p> <p>0.3571 0.1786 0.0893 0.0446</p>
--	--

After sag analysis



- Amplitude ratio

For approximations:



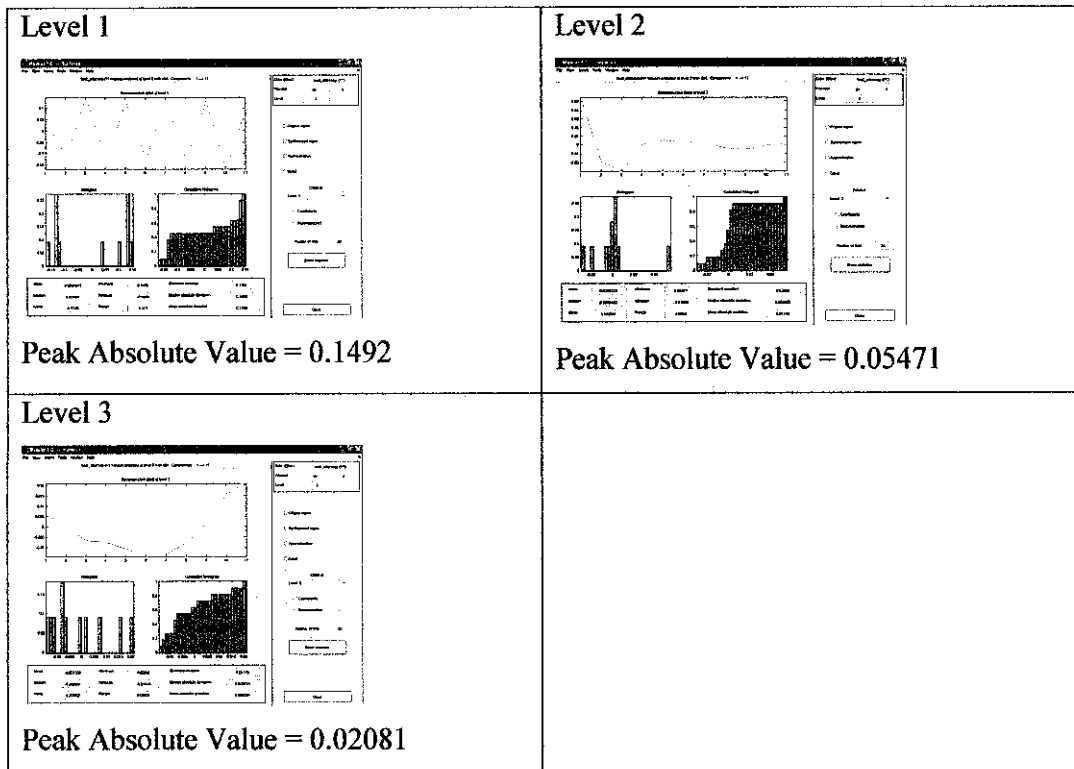
Ratio for each level of approximations:

$\alpha_n = \frac{\text{Peak absolute value of level } n \text{ approximation}}{\text{Highest peak absolute value among the levels}}$

Highest peak absolute value among the levels

α_n	VALUES
n=1	1.065/1.065 = 1.0000
n=2	1.053/1.065 = 0.9887
n=3	1.032/1.065 = 0.9690

For details:



Ratio for each level of details:

$\alpha_n = \text{Peak absolute value of level n details}$

Highest peak absolute value among the levels

α_n	VALUES
n=1	0.1492/0.1492 = 1.0000
n=2	0.05471/0.1492 = 0.3667
n=3	0.02081/0.1492 = 0.1395

- Frequency

	<p>Result:</p> <p>f =</p> <p>0.3571 0.1786 0.0893</p>
--	---

Summary

- Amplitude ratio

Approximations:

WAVEFORM TYPE	α_n	WHOLE	BEFORE	DURING	AFTER
Sag due to large load starting	n=1	0.9992	1.0000	1.0000	1.0000
	n=2	1.0000	1.0000	0.9479	1.0000
	n=3	0.9866	1.0000		0.9991
	n=4	0.9866	1.0000		0.9991
	n=5	0.9832	1.0000		0.9991
Sag due to fault	n=1	1.0000	1.0000	1.0000	1.0000
	n=2	0.9496		0.9266	0.9887
	n=3	0.9415		0.9211	0.9690
	n=4	0.9370		0.9220	
	n=5	0.9037			

Details:

WAVEFORM TYPE	α_n	WHOLE	BEFORE	DURING	AFTER
Sag due to large load starting	n=1	1.0000	0.7529	0.1609	1.0000
	n=2	0.4280	1.0000	1.0000	0.6461
	n=3	0.6749	0.7312		0.7879
	n=4	0.1450	0.1315		0.7238
	n=5	0.1425	0.2464		0.2521
Sag due to fault	n=1	1.0000	1.0000	1.0000	1.0000
	n=2	0.3206		0.7607	0.3667
	n=3	0.3432		0.4722	0.1395
	n=4	0.3946		0.5786	
	n=5	0.4241			

- Frequency

WAVEFORM TYPE	FREQUENCY			
	WHOLE	BEFORE	DURING	AFTER
Sag due to large load starting	0.1786	0.1786	0.1786	0.1786
	0.0893	0.0893	0.0893	0.0893
	0.0446	0.0446		0.0446
	0.0223	0.0223		0.0223
	0.0112	0.0112		0.0112
Sag due to fault	0.3571	0.3571	0.3571	0.3571
	0.1786		0.1786	0.1786
	0.0893		0.0893	0.0893
	0.0446		0.0446	
	0.0223			