## APPENDIX A

## CASE STUDIES: DECISION AND COALITION

## Case Study 1: High-rise Building Column Selection

### 1.1 Background

In this case study three decision makers namely Design Architect, Design Engineer and Construction Manager were involved in selection of high-rise building column of a marketing office building (Utomo, et al., 2009d). Columns are one of the most important structural systems in a building. Column design decomposes an element into a collection of system components. In new design, the column system selection can be part of the building design. For example, the building can be strengthened to support a heavy structural column system. The selection process is difficult because of the large number of factors, many of which are unrelated or conflicting with one another. A computer integrated knowledge based system would greatly benefit the selection process.

In this case, the optimum column was selected based on four possibilities of varying strength, size, reinforcement and shape. However, at certain level of the building, the strength requirement was ignored, because the construction manager wanted to use concrete of the same strength in the column as was used in the floor above. Also, the corner columns were all square, because it simplified the connection of the facing material. In addition, columns adjacent to stairs or elevators were square or rectangular. Nevertheless, in almost every column at every level, the optimization made some changes. By having knowledge of all the functions, a proper and reasonable decision was made. At certain levels, concrete strength variation was limited since same concrete strength was desirable in a floor. Also, column shape variation was not implemented in corner columns, since square columns were desired to fit plan.

With a general understanding of the available design options, considerations of the following technical and non technical criteria can lead to a selection of the most appropriate design for a project. The criteria are based on value analysis namely function and cost. Considering function, there are eight functions of optimizing column design as attributes of decision (Figure A.1). Those are satisfying décor, meet capacity and coordinate strength, maximize space, assure constructability, minimize/reduce creep, expedite design, reuse material, and minimize error. It is critical that the selected system sufficiently satisfies all of the criteria.

Column design selection criteria depend on the perspective of the individual decision makers. For example, a design architect might be more interested in satisfying decor function that will be influenced by column design whereas a design engineer is more interested in domain issues related to optimize design such as maximize space, minimize creep and expedite design. This makes it difficult for a decision maker to agree on the evaluation criteria. In this case study, there are four alternatives of column design as possible solution to be selected and be evaluated by eight criteria of function, two criteria of cost, and three decision makers. The alternatives are:

1. Alternative al (36x36; 6.0; 1.92), size: $36 \times 36$.

Percent Steel : 1.92
2. Alternative a2 (40x40; 6.0; 0.95), size: $40 \times 40$

Percent Steel $\quad 0.95$
3. Alternative a 3 ( $32 \times 32 ; 9.0 ; 1.07$ ), size: $32 \times 32$

Percent Steel : 1.07
4. Alternative a4 ( 36 diameters; $9.0 ; 0.99$ ), size: 36 diameters Percent Steel : 0.99

The selection of column design for high-rise building and other case studies in this research report undergoes the following steps:

Step 1: Each decision maker defines his/her evaluation criteria and sets the weight of each criterion (win condition).

Step 2: Using AHP, every decision maker evaluates and ranks the column design alternatives based on his/her win conditions.

Step 3: The ranking of the column design alternatives with respect to different decision makers are generated and compared in order to identify conflict.
Step 4: Identify agreement options, as well as a column design alternatives ranking that reflects the combined preferences of all decision makers (coalition).

Step 5: Determine the 'best fit' options for each coalition on first negotiation round.

### 1.2 Function Analysis of Building Column

This process provides an organized approach for determining the needs and desires of the stakeholders during value analysis of a project. The attribute of decision was set based on previous studies and standard function analysis in American Society for Testing and Material (ASTM) 2004, book of Building Economics. Function analysis consists of four sequential steps: (1) determination of project function, (2) examination and sorting of these functions into categories, (3) selection of critical functions and arrangement into a logical order, and (4) analyzing the importance of the function. Functions are analyzed through a structured logical format called Function Analysis System Technique (FAST). FAST is a diagramming technique that specifically illustrates the relationship and interrelationship of all functions within a specific project using a "How-Why" logic pattern.


Figure A-1 FAST Diagram of Optimizing High-rise Building Column

### 1.3 Life Cycle Cost of Building Column

A proper selection of the higher order basic function can affect cost. Major elements that contribute to the cost of a column are:
a. Size of concrete column.
b. Strength of column.
c. Vertical column formwork (temporary).
d. Reinforcement.

The major part of the load is carried by the concrete, but for alternative al, two thirds of the cost is for other items. The cost of reinforcement and temporary formwork should therefore be reduced proportionally. When construction managers instructed their design engineer, they focused on how to design column that will support the load. On alternative a2 the higher order function column design was changed to optimize column. Cost was inserted in the main critical path rather than as an all-thetime function. The column design fitted design criteria such as size, strength and percent of reinforcement. For alternative a3 the higher order function was changed to construct design. The a1, a2, a3 were proposed by design architect, design engineer and construction manager respectively, while the a4 was proposed as opponent of previous alternatives. It was based on the possibility of varying size, strength, reinforcement and shape.

Formwork is a necessary part of a concrete column that contributes nothing to load carrying capacity. Logically, its cost should be minimized. The shape of a column directly affects the ratio of the amount of formwork (circumference) required to the load carrying capacity (area). Circular and square shapes have equal circumference/area ratio, while rectangular columns have ratio greater than circular or square columns of the same area. Therefore, rectangular columns are less economical. Furthermore, circular columns are now being furnished in one-piece reusable (rentable) units, thus optimizing the cost of fabrication. Therefore, circular columns are most economical. Table A-1 presents the cost of each alternative of columns in a high-rise office building based on material category including concrete column and
reinforced (main vertical, dowels, and ties). Construction cost category consists of temporary formwork.

Table A-1 Cost of High-Rise Building Columns

| Cost category | Cost of each solution in Present Worth (10,000USD) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | ---: |
|  | (a1): $36 \times 36$ | (a2): $40 \times 40$ | (a3): $32 \times 32$ | (a4): 36 dim |
|  | 1.92 | 0.92 | 1.07 | 0.99 |
| Material | 698.3 | 598.7 | 521.6 | 533.9 |
| Construction | 272.2 | 302.4 | 241.8 | 98.3 |
| TOTAL | 970.4 | 901.1 | 763.5 | 632.2 |

### 1.4 Building Column Selection

The decision hierarchy on this case consists of four levels. Level 1 is set of goal. The goal of the problem ( $\mathrm{G}=$ ="To optimize high-rise building columns") is addressed by some alternatives $(\mathrm{A}=\mathrm{a} 1 ; \mathrm{a} 2 ; \mathrm{a} 3 ; \mathrm{a} 4)$ at level 4 . The problem is split into sub problems: $\mathrm{f} 1, \mathrm{f} 2, \mathrm{f} 3, \mathrm{f} 4, \mathrm{f} 5, \mathrm{f} 6, \mathrm{f} 7, \mathrm{f} 8, \mathrm{c} 1$ and c 2 , which are the evaluation criteria that will be used to select the best column. Level 3 of the decision hierarchy is a set of sub criteria derived from function analysis in Figure A. 1 Level 2 of the decision hierarchy is selection criteria which are function and cost.


Figure A-2 Decision Hierarchies for Optimizing High-rise Building Column

Table A-2 below presents the ranking of high-rise building column options for each decision maker or stakeholder. Analytical Hierarchy Process (AHP) method is used to determine the ranking.

Table A-2 Weighting Factor of Each Alternative to Each Stakeholder

| Designer | Weighting factor for each alternative in each criteria for design architect$(\lambda=8.688172, \mathrm{CI}=0.09831, \mathrm{CR}=0.069724)$ |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { C1 } \\ (0.289) \end{gathered}$ | $\begin{gathered} \mathrm{C} 2 \\ (0.217) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 3 \\ (0.080) \\ \hline \end{gathered}$ | $\begin{gathered} \text { C4 } \\ (0.144) \\ \hline \end{gathered}$ | $\begin{gathered} \text { C5 } \\ (0.040) \\ \hline \end{gathered}$ | $\begin{gathered} \text { C6 } \\ (0.057) \\ \hline \end{gathered}$ | $\begin{gathered} \text { C7 } \\ (0.025) \\ \hline \end{gathered}$ | $\begin{gathered} \text { C8 } \\ (0.023) \\ \hline \end{gathered}$ | $\begin{gathered} \text { C9 } \\ (0.104) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 10 \\ (0.021) \\ \hline \end{gathered}$ | $\Sigma$ | Ranking |
| a1 (36x36; 6.0; 1.92) | 0.130 | 0.060 | 0.013 | 0.024 | 0.009 | 0.015 | 0.005 | 0.006 | 0.009 | 0.002 | 0.272 | $1^{\text {st }}$ |
| a2 ( $40 \times 40 ; 6.0 ; 0.92$ ) | 0.052 | 0.084 | 0.018 | 0.017 | 0.019 | 0.026 | 0.007 | 0.012 | 0.015 | 0.001 | 0.251 | $2^{\text {nd }}$ |
| a3 (32x32; 9.0; 1.07) | 0.081 | 0.043 | 0.009 | 0.033 | 0.005 | 0.007 | 0.004 | 0.004 | 0.049 | 0.004 | 0.239 | $3^{\text {rd }}$ |
| a4 (36dia; 9.0; 0.99) | 0.026 | 0.030 | 0.039 | 0.070 | 0.007 | 0.010 | 0.010 | 0.002 | 0.031 | 0.014 | 0.237 | $4^{\text {th }}$ |
| Programmer | Weighting factor for each alternative in each criteria for design engineer$(\lambda=8.853712, \mathrm{CI}=0.121959, \mathrm{CR}=0.086496)$ |  |  |  |  |  |  |  |  |  |  |  |
|  | $\begin{gathered} \mathrm{C} 1 \\ (0.010) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 2 \\ (0.007) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 3 \\ (0.032) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 4 \\ (0.022) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 5 \\ (0.019) \\ \hline \end{gathered}$ | $\begin{gathered} \text { C6 } \\ (0.016) \\ \hline \end{gathered}$ | $\begin{gathered} \text { C7 } \\ (0.012) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 8 \\ (0.007) \\ \hline \end{gathered}$ | $\begin{gathered} \text { C9 } \\ (0.583) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 10 \\ (0.292) \\ \hline \end{gathered}$ | $\sum$ | Ranking |
| a1 (36x36; 6.0; 1.92) | 0.005 | 0.002 | 0.005 | 0.004 | 0.004 | 0.004 | 0.002 | 0.002 | 0.051 | 0.026 | 0.104 | $4^{\text {th }}$ |
| a2 (40x40; 6.0; 0.92) | 0.002 | 0.003 | 0.008 | 0.003 | 0.009 | 0.007 | 0.003 | 0.004 | 0.083 | 0.015 | 0.136 | $3^{\text {rd }}$ |
| a3 (32x32; 9.0; 1.07) | 0.003 | 0.001 | 0.004 | 0.005 | 0.002 | 0.002 | 0.002 | 0.001 | 0.276 | 0.062 | 0.358 | ${ }^{\text {nd }}$ |
| a4 (36dia; 9.0; 0.99) | 0.001 | 0.001 | 0.016 | 0.011 | 0.003 | 0.003 | 0.005 | 0.001 | 0.174 | 0.189 | 0.402 | $1^{\text {st }}$ |
| Construction manager | Weighting factor for each alternative in each criteria for construction manager$(\lambda=8.793054, \mathrm{CI}=0.113293, \mathrm{CR}=0.08035)$ |  |  |  |  |  |  |  |  |  |  |  |
|  | $\begin{gathered} \mathrm{C} 1 \\ (0.078) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 2 \\ (0.029) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 3 \\ (0.139) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 4 \\ (0.031) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 5 \\ (0.030) \\ \hline \end{gathered}$ | $\begin{gathered} \text { C6 } \\ (0.050) \\ \hline \end{gathered}$ | $\begin{gathered} \text { C7 } \\ (0.155) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 8 \\ (0.238) \\ \hline \end{gathered}$ | $\begin{gathered} \text { C9 } \\ (0.031) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 10 \\ (0.219) \\ \hline \end{gathered}$ | $\sum$ | Ranking |
| a1 ( $36 \times 36 ; 6.0 ; 1.92$ ) | 0.035 | 0.008 | 0.023 | 0.005 | 0.007 | 0.013 | 0.031 | 0.057 | 0.003 | 0.019 | 0.202 | $3^{\text {rd }}$ |
| a2 ( $40 \times 40 ; 6.0 ; 0.92$ ) | 0.014 | 0.011 | 0.032 | 0.004 | 0.014 | 0.022 | 0.043 | 0.123 | 0.005 | 0.011 | 0.280 | $2^{\text {nd }}$ |
| a3 (32x32; 9.0; 1.07) | 0.022 | 0.006 | 0.016 | 0.007 | 0.004 | 0.006 | 0.022 | 0.037 | 0.015 | 0.046 | 0.180 | $4^{\text {th }}$ |
| a4 (36dia; 9.0; 0.99) | 0.007 | 0.004 | 0.067 | 0.015 | 0.005 | 0.009 | 0.060 | 0.020 | 0.009 | 0.142 | 0.339 | $1^{\text {st }}$ |
| Aggregation | $\begin{gathered} \text { C1 } \\ (0.126) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 2 \\ (0.084) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 3 \\ (0.084) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 4 \\ (0.066) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 5 \\ (0.029) \\ \hline \end{gathered}$ | $\begin{gathered} \text { C6 } \\ (0.041) \\ \hline \end{gathered}$ | $\begin{gathered} \text { C7 } \\ (0.064) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 8 \\ (0.089) \\ \hline \end{gathered}$ | $\begin{gathered} \text { C9 } \\ (0.240) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} 10 \\ (0.177) \\ \hline \end{gathered}$ | $\sum$ | Ranking |
| a1 ( $36 \times 36 ; 6.0 ; 1.92$ ) | 0.057 | 0.023 | 0.014 | 0.011 | 0.007 | 0.011 | 0.013 | 0.022 | 0.021 | 0.016 | 0.193 | $4^{\text {th }}$ |
| a2 ( $40 \times 40 ; 6.0 ; 0.92$ ) | 0.023 | 0.033 | 0.019 | 0.008 | 0.014 | 0.018 | 0.018 | 0.046 | 0.034 | 0.009 | 0.222 | $3^{\text {rd }}$ |
| a3 (32x32; 9.0; 1.07) | 0.035 | 0.017 | 0.010 | 0.015 | 0.003 | 0.005 | 0.009 | 0.014 | 0.113 | 0.037 | 0.259 | $2^{\text {nd }}$ |
| a4 (36dia; 9.0; 0.99) | 0.011 | 0.012 | 0.041 | 0.032 | 0.005 | 0.007 | 0.025 | 0.008 | 0.071 | 0.115 | 0.326 | $1^{\text {st }}$ |

In this case there were three decision makers. Decision before coalition revealed the result of weighting each alternative for each decision maker. The design architect chose $36 \times 36$ columns as the best solution, meanwhile design engineer and construction manager chose a cylinder column.

### 1.5 Satisfying Option on Value Criteria

One way of categorizing the options of technical solution for high-rise building column is to identify material cost and construction method cost as 'Cost', and to
identify all functions as 'Function'. Table A-3 show the selectability (Ps) and rejectability (Pr) that represent function and cost of technical solution of high-rise building column respectively.

Table A-3 Cost and Function of High-rise Building Column Options

|  | Cost |  |  |  | Function |  |  |  |  |  |  |  | Normalization |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | c1 | c2 | $\Sigma$ | Loss | f1 | f2 | f3 | f4 | F5 | f6 | f7 | $f 8$ | Cost (Pr) | Function (Ps) |
| a1 | 0.09 | 0.09 | 0.18 | 0.95 | 0.45 | 0.27 | 0.17 | 0.17 | 0.23 | 0.26 | 0.20 | 0.09 | 0.381 | 0.229 |
| a2 | 0.14 | 0.05 | 0.19 | 0.93 | 0.18 | 0.39 | 0.23 | 0.12 | 0.48 | 0.45 | 0.27 | 0.14 | 0.373 | 0.283 |
| a3 | 0.47 | 0.21 | 0.68 | 0.44 | 0.28 | 0.20 | 0.12 | 0.23 | 0.12 | 0.12 | 0.14 | 0.47 | 0.176 | 0.210 |
| a4 | 0.30 | 0.65 | 0.95 | 0.18 | 0.09 | 0.14 | 0.48 | 0.48 | 0.17 | 0.17 | 0.39 | 0.30 | 0.071 | 0.278 |

Based on the result presented on Table 3, Figure 3 provides a cross plot of function of the technical solution options. Observe that although a2 has the highest function, it also has high cost which is resulted its value below $\mathrm{F} / \mathrm{C}=1$. In this case, the highest basic value is a4 since it gives the highest satisfaction due to its high function and low cost.
Basic Value


$$
\begin{array}{ll}
\square-\mathrm{a} 1(36 \times 36 ; 6.0 ; 1.92) & \text { ■-a2 (40x40; } 6.0 ; 0.92) \\
\longrightarrow \mathrm{a} 3(32 \times 32 ; 9.0 ; 1.07) & - \\
\text { Value }=\mathrm{F} / \mathrm{C}=1
\end{array}
$$

Figure A-3 Basic Value of High-rise Building Column Options

Figures A-4, A-5, and A-6 provide a cross plot of function and cost of design architect, design engineer, and construction manager respectively. It means that the value of technical solution depends on the preference of stakeholder. Observe that the construction manager's preference has influence on a3. Basically a3 has value more than $\mathrm{F} / \mathrm{C}=1$ or this option has selectability options. The construction manager's preference has changed it to a value below $\mathrm{F} / \mathrm{C}=1$ or rejectability options.


Figure A-4 Value of High-rise Building Column Options for Design Architect


Figure A-5 Value of High-rise Building Column Options for Design Engineer

## Construction Manager



Figure A-6 Value of High-rise Building Column Options for Construction Manager

### 1.6 Agreement Options and Coalition

(1) Determining the weighting factor (weight of preferences) of each criteria for individual decision maker.

Figures A-7 and A-8 reveal different preferences between the decision makers. In contrast to the programmer who put most weight on material cost, the designer put satisfying decor as the most preferred criteria; meanwhile the construction manager put most preference on minimizing errors. The difference presents rationality amongst the decision makers.


Figure A-7 Weighting Factor for Each Stakeholder on Criteria


Figure A-8 Weighting Factor of Criteria for Each Stakeholder
(2) Grading alternative for each evaluation criteria.

Figure A-9 presents that a2 is the 'best fit' for f2, f5, f6, and f8. The 'best fit' solution for fl is a 1 ; a 3 is best fit for criteria c 1 that is material cost; meanwhile a 4 is the 'best fit' for $\mathrm{f} 3, \mathrm{f} 4, \mathrm{f} 7$ and c2.


Figure A-9 Weighting Factor of Alternatives for Each Criteria
(3) Scoring every alternative for every stakeholder.

Figure A-10 shows that stakeholders have different best option as a solution alternative. Before coalition, the design architect chose $36 \times 36$ columns as the best solution, while the design engineer and the construction manager chose a cylinder column.


Figure A-10 Weighting Factor of Alternative for Each Stakeholder
(4) Determining payoff optimum.

Determination of the payoff optimum follows the algorithm in Equations 6.1, 6.2, 6.3, and 6.4 presented in Chapter Six. The process and result are presented on Tables A-4 and A-5 for Cost and Function respectively.

Table A-4 Cost Payoff Optimum for Each Coalition on Building Column Selection

| Coalition |  | Alternatives |  |  |  |  |  |  | Payoff Optimum |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SH1+2+3 |  | a1 | a2 |  |  | a3 |  | a4 | Max-min | Optimum |
|  | SH1 |  | 0.403 |  | 0.365 |  | 0.082 | 0.150 | 0.321 | 0.403 |
|  | SH2 |  | 0.412 |  | 0.387 |  | 0.115 | 0.087 | 0.325 | 0.397 |
|  | SH3 |  | 0.347 |  | 0.362 |  | 0.254 | 0.038 | 0.324 | 0.362 |
|  |  |  | 1.161 |  | 1.113 |  | 0.450 | 0.275 |  |  |
| SH1+2 |  | a1 |  | a2 |  | a3 |  | a4 |  |  |
|  | SH1 |  | 0.403 |  | 0.365 |  | 0.082 | 0.150 | 0.321 | 0.403 |
|  | SH2 |  | 0.412 |  | 0.387 |  | 0.115 | 0.087 | 0.325 | 0.412 |
|  |  |  | 0.815 |  | 0.752 |  | 0.197 | 0.237 |  |  |
| SH1+3 |  | a1 |  | a2 |  | a3 |  | a4 |  |  |
|  | SH1 |  | 0.403 |  | 0.365 |  | 0.082 | 0.150 | 0.321 | 0.403 |
|  | SH3 |  | 0.347 |  | 0.362 |  | 0.254 | 0.038 | 0.324 | 0.347 |
|  |  |  | 0.750 |  | 0.727 |  | 0.335 | 0.188 |  |  |
| SH2+3 |  | a1 |  | a2 |  | a3 |  | a4 |  |  |
|  | SH2 |  | 0.412 |  | 0.387 |  | 0.115 | 0.087 | 0.325 | 0.397 |
|  | SH3 |  | 0.347 |  | 0.362 |  | 0.254 | 0.038 | 0.324 | 0.362 |
|  |  |  | 0.758 |  | 0.748 |  | 0.369 | 0.125 |  |  |

Table A-5 Function Payoff Optimum for Each Coalition on Building Column Selection


Payoff optimum for cost and function become the data for the best fit options algorithm. The result of the process is presented at stage (5) below.
(5) Analyzing the best fit option for every coalition and grand coalition.

The result is presented on Table A-6. It shows the priorities that followed the best fit option process and algorithm in Equation 6.5 in Chapter Six. It also presents the result of priorities of the technical solution for high-rise building column in first negotiation round. In this case, the a4 ( $36 \mathrm{dim} ; 0.99$ ) is the best fit option.

Table A-6 Ranking of Building Column Options for each Coalition

| Alternative ranking and coalition | Priorities |  |  |  |
| :--- | :--- | :---: | :---: | :---: |
|  | a1 | a 2 | a 3 | a 4 |
| SH 1 (Design Architect) | $1^{\text {st }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $4^{\text {th }}$ |
| SH 2 (Design Engineer) | $4^{\text {th }}$ | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $1^{\text {st }}$ |
| SH 3 (Construction Manager) | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $4^{\text {th }}$ | $1^{\text {st }}$ |
| Coalition SH1 and SH2 | $4^{\text {th }}$ | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $1^{\text {st }}$ |
| Coalition SH1 and SH3 | $3^{\text {rd }}$ | $1^{\text {st }}$ | $2^{\text {nd }}$ | $4^{\text {th }}$ |
| Coalition SH2 and SH3 | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $4^{\text {th }}$ | $1^{\text {st }}$ |
| Grand coalition SH1,2,3 | $4^{\text {th }}$ | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $1^{\text {st }}$ |
| RESULT | $3^{\text {rd }}$ | $2^{\text {nd }}$ | - | $1^{\text {st }}$ |

### 1.7 Similarity Index

Similarity index of three models of group decision are presented on Table A-7. The table shows that model 3 proposed on this research is the only model giving satisfaction to all stakeholders. The closer the value of individual stakeholder to the best fit group, the more satisfying the model is to every stakeholder.

Table A-7 Similarity Index Result for High-rise Building Column Selection

|  | Model 1: <br> Single weighting | Model 2: <br> Aggregation | Model 3: <br> Coalition algorithm |
| :--- | :---: | :---: | :---: |
| Stakeholder 1 | $>1=1$ | $>1=1$ | 0.0857 |
| Stakeholder 2 | $>1=1$ | 0.74496644 | 0.4564 |
| Stakeholder 3 | $>1=1$ | $>1=1$ | 0.4110 |

### 1.8 Conclusion of the Case Study

The coalition table (Table A-6) reveals the start of the first negotiation round. Some of the solutions will not be an option if no individual stakeholder or coalition of stakeholders desires to select it. In this case, alternative solution a3 is not an option. Table A-6 also indicates the alternative solution that will be determined to be the best fit solution. As the the 'best fit' solution, a4 is contrary to the best option selected by the design architect, who chose al. On the process of trade off in the next negotiation round, the design architect can propose a new preference if he or she did not accept a4 as the best option. The process of validation using similarity index revealed the best group decision model that satisfied all stakeholders. That came from the algorithm of the proposed negotiation support model.

## Case study 2: Wall System Selection

### 2.1 Background

This case study involved the selection of wall system (Utomo, et al., 2008c). Five decision makers were involved: Property Manager, Project Manager, Architect, QS, and Engineer. As one of the most important system in a building, wall system selection can be part of the building design. The selection process is difficult because of the large number of factors, many of which are unrelated or conflicting with one another, and the lack of key data (such as realistic design service life). Like in highrise building column selection, a computer integrated knowledge based system would also greatly benefit to wall system selection process.

Based on value criteria which are function and cost, there are seven attributes of wall functions that need to be considered in decision making, namely work function, environmental support, security assurance, user need, image, property management support, building economics. It is critical that the selected system sufficiently satisfies all of the criteria. Wall system selection criteria depend on the perspective of the individual decision makers. For example, an architect might be more interested in the image of building that will be influenced by the wall system and user satisfaction, whereas a project manager is more interested in domain issues related to owner and constraints such as budget that reflected on initial cost. This makes it difficult for decision makers to agree on the evaluation criteria.

In this case study, there are five possible solutions of wall system to be evaluated according to six criteria of function and cost, involving five decision makers. The possible solutions are:

1. Reinforced brick wall.
2. Precast wall concrete.
3. Metal frame wall.
4. Timber wall panel.
5. Glass wall

### 2.2 Function Analysis of Wall System

The function of building wall system can be identified using the function analysis system technique (FAST). Figure A-11 shows the FAST diagram. The diagram is determined by Focus Group research. In this case, there are eight functions identified on the wall system which are structural stability; exclusion of rain and water; thermal properties; acoustics properties; protection to occupant's asset; fire safety; satisfy and user convenience; image and aesthetic. Further the identified function will become the attributes for decision.


Figure A-11 FAST Diagram of the Building Wall System

### 2.3 Life Cycle Cost of Wall System

Cost drivers of the wall system which are initial cost and operation maintenance cost are identified. Since operation and maintenance (O\&M) costs have annual basis, Equation (2.3) in Chapter Two was used to calculate the O\&M costs. Table A-8 below presents the cost of the wall system for each technical solution which are al (reinforced brick wall), a2 (Precast wall concrete), a3 (Metal frame wall), a4 (Timber wall panel), and a5 (Glass wall). The cost drivers namely c 1 (initial cost) and c 2 (operation and maintenance cost) become evaluation criteria in the selection of wall
system solution.
Table A-8 Cost of Wall System

| Cost category | Present Worth (1000USD) |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
|  | a1 | a2 | a3 | a4 | a5 |
| (c1) Initial | 250 | 1600 | 800 | 1600 | 1200 |
| (c2) Operation and maintenance | 800 | 200 | 400 | 2000 | 800 |

### 2.4 Wall System Selection

In order to obtain a good representation of the problem, it has to be structured into different components called activities. Figure A-12 shows that the goal of the problem ( $G=$ "To select wall system") is addressed by some alternatives $(A=a 1$; a2; a3, a4, a5) which are metal frame wall, precast wall concrete, glass wall, timber wall panel, and reinforced brick wall respectively. The problem is split into value criteria namely function and cost and subproblem (f1, f2, f3, f4, f5, f6, f7, f8, c1, c2) which are the evaluation criteria.


Figure A-12 Decision Hierarchy to Select the Best Wall System

The weighting factor of each alternative in wall system for each decision maker is presented on Table A-9. It represents the ranking of the solutions. The process to determine the ranking is followed to AHP calculation presented on Appendix B. Aggregation value that represents the group value is also presented in the table. Later the aggregation value will be compared with the result from coalition by similarity index in the next section.

Table A-9 Judgment Synthesis of Every Stakeholder on Each Wall System Solutions

| Property Manager |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | f1 | f2 | f3 | f4 | f5 | f6 | f7 | f8 | c1 | c2 | Weight |
|  | 0.022 | 0.117 | 0.053 | 0.040 | 0.190 | 0.264 | 0.093 | 0.097 | 0.013 | 0.113 |  |
| a1 | 0.022 | 0.117 | 0.053 | 0.040 | 0.190 | 0.264 | 0.093 | 0.097 | 0.013 | 0.113 | 0.2734 |
| a2 | 0.001 | 0.012 | 0.022 | 0.017 | 0.044 | 0.109 | 0.024 | 0.020 | 0.007 | 0.018 | 0.2890 |
| a3 | 0.002 | 0.015 | 0.016 | 0.012 | 0.088 | 0.082 | 0.006 | 0.014 | 0.001 | 0.055 | 0.1619 |
| a4 | 0.003 | 0.029 | 0.007 | 0.006 | 0.031 | 0.043 | 0.007 | 0.007 | 0.003 | 0.026 | 0.0879 |
| a5 | 0.006 | 0.004 | 0.006 | 0.002 | 0.017 | 0.008 | 0.037 | 0.004 | 0.000 | 0.004 | 0.1878 |
| Project Manager |  |  |  |  |  |  |  |  |  |  |  |
|  | f1 | f2 | f3 | f4 | f5 | f6 | f7 | f8 | c1 | c2 | Weight |
|  | 0.038 | 0.021 | 0.013 | 0.007 | 0.009 | 0.054 | 0.074 | 0.034 | 0.675 | 0.075 |  |
| a1 | 0.002 | 0.002 | 0.005 | 0.003 | 0.002 | 0.022 | 0.019 | 0.007 | 0.374 | 0.012 | 0.4487 |
| a2 | 0.003 | 0.003 | 0.004 | 0.002 | 0.004 | 0.017 | 0.004 | 0.005 | 0.035 | 0.036 | 0.1129 |
| a3 | 0.005 | 0.005 | 0.002 | 0.001 | 0.002 | 0.009 | 0.006 | 0.002 | 0.177 | 0.017 | 0.2252 |
| a4 | 0.010 | 0.001 | 0.001 | 0.000 | 0.001 | 0.002 | 0.030 | 0.001 | 0.025 | 0.003 | 0.0732 |
| a5 | 0.018 | 0.010 | 0.001 | 0.001 | 0.000 | 0.005 | 0.015 | 0.018 | 0.065 | 0.007 | 0.1399 |
| Architect |  |  |  |  |  |  |  |  |  |  |  |
|  | f1 | f2 | f3 | f4 | f5 | f6 | f7 | f8 | c1 | c2 | Weight |
|  | 0.123 | 0.043 | 0.040 | 0.057 | 0.040 | 0.083 | 0.183 | 0.307 | 0.083 | 0.042 |  |
| a1 | 0.007 | 0.004 | 0.017 | 0.025 | 0.009 | 0.034 | 0.047 | 0.062 | 0.046 | 0.007 | 0.2576 |
| a2 | 0.008 | 0.006 | 0.013 | 0.016 | 0.018 | 0.026 | 0.011 | 0.043 | 0.004 | 0.020 | 0.1656 |
| a3 | 0.016 | 0.011 | 0.005 | 0.008 | 0.007 | 0.014 | 0.014 | 0.023 | 0.022 | 0.009 | 0.1285 |
| a4 | 0.031 | 0.002 | 0.004 | 0.003 | 0.004 | 0.002 | 0.073 | 0.011 | 0.003 | 0.001 | 0.1354 |
| a5 | 0.060 | 0.021 | 0.002 | 0.005 | 0.002 | 0.007 | 0.037 | 0.168 | 0.008 | 0.004 | 0.3129 |
| QS |  |  |  |  |  |  |  |  |  |  |  |
|  | f1 | f2 | f3 | f4 | f5 | f6 | f7 | f8 | c1 | c2 | Weight |
|  | 0.143 | 0.022 | 0.034 | 0.025 | 0.130 | 0.176 | 0.099 | 0.038 | 0.250 | 0.083 |  |
| a1 | 0.008 | 0.002 | 0.014 | 0.011 | 0.030 | 0.073 | 0.025 | 0.008 | 0.139 | 0.013 | 0.3229 |
| a2 | 0.010 | 0.003 | 0.011 | 0.007 | 0.060 | 0.055 | 0.006 | 0.005 | 0.013 | 0.040 | 0.2100 |
| a3 | 0.019 | 0.005 | 0.005 | 0.003 | 0.021 | 0.029 | 0.008 | 0.003 | 0.065 | 0.019 | 0.1772 |
| a4 | 0.036 | 0.001 | 0.004 | 0.001 | 0.012 | 0.005 | 0.040 | 0.001 | 0.009 | 0.003 | 0.1122 |
| a5 | 0.069 | 0.011 | 0.001 | 0.002 | 0.006 | 0.015 | 0.020 | 0.021 | 0.024 | 0.008 | 0.1777 |
| Engineer |  |  |  |  |  |  |  |  |  |  |  |
|  | f1 | f2 | f3 | f4 | f5 | f6 | f7 | f8 | c1 | c2 | Weight |
|  | 0.070 | 0.185 | 0.122 | 0.043 | 0.065 | 0.126 | 0.027 | 0.029 | 0.067 | 0.267 |  |
| a1 | 0.004 | 0.019 | 0.050 | 0.019 | 0.015 | 0.052 | 0.007 | 0.006 | 0.037 | 0.042 | 0.2509 |
| a2 | 0.005 | 0.024 | 0.038 | 0.012 | 0.030 | 0.039 | 0.002 | 0.004 | 0.003 | 0.130 | 0.2874 |
| a3 | 0.009 | 0.046 | 0.016 | 0.006 | 0.011 | 0.021 | 0.002 | 0.002 | 0.017 | 0.060 | 0.1908 |
| a4 | 0.018 | 0.007 | 0.013 | 0.002 | 0.006 | 0.004 | 0.011 | 0.001 | 0.002 | 0.009 | 0.0726 |
| a5 | 0.034 | 0.089 | 0.005 | 0.003 | 0.003 | 0.011 | 0.005 | 0.016 | 0.006 | 0.026 | 0.1983 |
| Aggregation |  |  |  |  |  |  |  |  |  |  |  |
|  | f1 | f2 | f3 | f4 | f5 | f6 | f7 | f8 | c1 | c2 | Weight |
|  | 0.079 | 0.078 | 0.053 | 0.034 | 0.087 | 0.141 | 0.095 | 0.101 | 0.218 | 0.116 |  |
| a1 | 0.005 | 0.008 | 0.022 | 0.015 | 0.020 | 0.058 | 0.024 | 0.020 | 0.121 | 0.018 | 0.3107 |
| a2 | 0.005 | 0.010 | 0.016 | 0.010 | 0.040 | 0.044 | 0.006 | 0.014 | 0.011 | 0.056 | 0.2130 |
| a3 | 0.010 | 0.019 | 0.007 | 0.005 | 0.014 | 0.023 | 0.007 | 0.007 | 0.057 | 0.026 | 0.1767 |
| a4 | 0.020 | 0.003 | 0.006 | 0.002 | 0.008 | 0.004 | 0.038 | 0.004 | 0.008 | 0.004 | 0.0963 |
| a5 | 0.038 | 0.037 | 0.002 | 0.003 | 0.004 | 0.012 | 0.019 | 0.055 | 0.021 | 0.011 | 0.2033 |

### 2.5 Satisfying Option on Value Criteria

In this case study, initial cost and O\&M cost are identified as 'Cost' and the other eight functions which are structural stability; exclusion of rain and water; thermal properties; acoustics properties; protection to occupant's asset; fire safety; satisfy and user convenience; image and aesthetic are identified as 'Function'. Table A-10 shows the selectability (Ps) and rejectability (Pr) that represent function and cost of technical solution of wall system respectively.

Table A-10 Cost and Function of Wall System Options

|  | Cost |  | Function |  |  |  |  |  |  |  | Normalization |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | c1 | c2 | f1 | f2 | f3 | f4 | f5 | f6 | f7 | f8 | Cost (Pr) | Function <br> (Ps) |
| a1 | 0.554 | 0.158 | 0.058 | 0.103 | 0.411 | 0.437 | 0.234 | 0.412 | 0.255 | 0.202 | 0.037 | 0.264 |
| a2 | 0.051 | 0.486 | 0.069 | 0.132 | 0.311 | 0.288 | 0.463 | 0.310 | 0.059 | 0.140 | 0.128 | 0.222 |
| a3 | 0.261 | 0.227 | 0.132 | 0.249 | 0.133 | 0.139 | 0.163 | 0.164 | 0.079 | 0.074 | 0.154 | 0.142 |
| a4 | 0.037 | 0.034 | 0.253 | 0.037 | 0.105 | 0.056 | 0.091 | 0.030 | 0.402 | 0.037 | 0.372 | 0.126 |
| a5 | 0.096 | 0.096 | 0.487 | 0.480 | 0.040 | 0.080 | 0.048 | 0.085 | 0.205 | 0.547 | 0.309 | 0.247 |

Based on the result presented on Table A-10, Figure A-13 provides a cross plot of function of the technical solution options. In this case the highest basic value is a1. It gives the highest satisfaction since it has high function and low cost.


Figure A-13 Basic Value of Wall System Options

Figures A-14, A-15, A-16, A-17 and A-18 provide a cross plot of function and cost for property manager, project manager, architect, QS, and engineer respectively. It means that the value of technical solution depends on the preference of stakeholders. Observe the influence of the engineer's preference on a3. Basically a3 has a value below $\mathrm{F} / \mathrm{C}=1$, which is a rejected option. However, the engineer's preference changes it to a value greater than $\mathrm{F} / \mathrm{C}=1$, thus a3 becomes a selected option.


Figure A-14 Value of Wall System Options for Property Manager

Project Manager


Figure A-15 Value of Wall System Options for Project Manager


Figure A-16 Value of Wall System Options for Architect


Figure A-17 Value of Wall System Options for QS

## Engineer



Figure A-18 Value of Wall System Options for Engineer

### 2.6 Agreement Options and Coalition

(1) Determining the weighting factor (weight of preferences) of criteria for each stakeholder.

Figure A-19 reveals different preferences between stakeholders.


Figure A-19 Weight of Preferences of Wall System Criteria for Each Stakeholder
(2) Grading alternative for each evaluation criteria.

Figure A-20 presents that a 5 is the 'best fit' for $\mathrm{f} 1, \mathrm{f} 2$, f 8 whereas a 1 is the 'best fit' for $\mathrm{f} 3, \mathrm{f} 4, \mathrm{f} 6$, and c1.


Figure A-20 Weighting Factor of Each Wall System Option for Each Criterion
(3) Scoring every alternative for every stakeholder.

Figure A-21 shows that stakeholders have different best option as solution alternative. In this case only Stakeholder 1 (Property Manager) chose precast (a2) as the best option, architect chose a5, engineer choose a2 and other two stakeholders choose al as the best solution for wall system.


Figure A-21 Weighting Factor of Each Wall System Option for Each Stakeholder

## (4) Determining payoff optimum

The process of determining payoff optimum and the result are presented on Tables A-11 and A-12 for cost and function respectively.

Table A-11 Cost Payoff Optimum for Each Coalition on Wall System Selection

| Coalition | Alternatives |  |  |  |  | Payoff Optimum |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SH1+2+3+4+5 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| SH1 | 0.031 | 0.145 | 0.270 | 0.246 | 0.308 | 0.276 | 0.123 |
| SH2 | 0.282 | 0.220 | 0.263 | 0.205 | 0.030 | 0.253 | 0.282 |
| SH3 | 0.295 | 0.285 | 0.197 | 0.202 | 0.021 | 0.274 | 0.295 |
| SH4 | 0.203 | 0.217 | 0.243 | 0.218 | 0.120 | 0.124 | 0.243 |
| SH5 | 0.249 | 0.251 | 0.220 | 0.210 | 0.070 | 0.180 | 0.251 |
|  | 1.060 | 1.117 | 1.194 | 1.080 | 0.548 |  | 1.194 |
| SH1+2 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| SH1 | 0.031 | 0.145 | 0.270 | 0.246 | 0.308 | 0.276 | 0.251 |
| SH2 | 0.282 | 0.220 | 0.263 | 0.205 | 0.030 | 0.253 | 0.282 |
|  | 0.313 | 0.365 | 0.533 | 0.451 | 0.337 |  | 0.533 |
| SH1+3 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| SH1 | 0.031 | 0.145 | 0.270 | 0.246 | 0.308 | 0.276 | 0.172 |
| SH3 | 0.295 | 0.285 | 0.197 | 0.202 | 0.021 | 0.274 | 0.295 |
|  | 0.326 | 0.430 | 0.467 | 0.448 | 0.329 |  | 0.467 |
| SH1+4 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| SH1 | 0.031 | 0.145 | 0.270 | 0.246 | 0.308 | 0.276 | 0.270 |
| SH4 | 0.203 | 0.217 | 0.243 | 0.218 | 0.120 | 0.124 | 0.243 |
|  | 0.234 | 0.362 | 0.513 | 0.464 | 0.427 |  | 0.513 |
| SH1+5 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| SH1 | 0.031 | 0.145 | 0.270 | 0.246 | 0.308 | 0.276 | 0.239 |
| SH5 | 0.249 | 0.251 | 0.220 | 0.210 | 0.070 | 0.180 | 0.251 |
|  | 0.280 | 0.396 | 0.490 | 0.456 | 0.378 |  | 0.490 |
| SH2+3 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| SH2 | 0.282 | 0.220 | 0.263 | 0.205 | 0.030 | 0.253 | 0.282 |
| SH3 | 0.295 | 0.285 | 0.197 | 0.202 | 0.021 | 0.274 | 0.295 |
|  | 0.577 | 0.505 | 0.461 | 0.407 | 0.051 |  | 0.577 |
| SH2+4 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| SH2 | 0.282 | 0.220 | 0.263 | 0.205 | 0.030 | 0.253 | 0.263 |
| SH4 | 0.203 | 0.217 | 0.243 | 0.218 | 0.120 | 0.124 | 0.243 |
|  | 0.485 | 0.437 | 0.507 | 0.423 | 0.149 |  | 0.507 |
| SH2+5 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| SH2 | 0.282 | 0.220 | 0.263 | 0.205 | 0.030 | 0.077 | 0.282 |
| SH5 | 0.249 | 0.251 | 0.220 | 0.210 | 0.070 | 0.041 | 0.249 |
|  | 0.531 | 0.471 | 0.484 | 0.415 | 0.100 |  |  |
| SH3+4 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| SH3 | 0.295 | 0.285 | 0.197 | 0.202 | 0.021 | 0.274 | 0.258 |
| SH4 | 0.203 | 0.217 | 0.243 | 0.218 | 0.120 | 0.124 | 0.243 |
|  | 0.498 | 0.502 | 0.441 | 0.419 | 0.141 |  | 0.502 |
| SH3+5 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| SH3 | 0.295 | 0.285 | 0.197 | 0.202 | 0.021 | 0.274 | 0.293 |


|  | SH5 | $\begin{aligned} & 0.249 \\ & 0.544 \end{aligned}$ | $\begin{aligned} & 0.251 \\ & 0.536 \end{aligned}$ | $\begin{aligned} & 0.220 \\ & 0.418 \end{aligned}$ | $\begin{aligned} & 0.210 \\ & 0.411 \end{aligned}$ | $\begin{aligned} & 0.070 \\ & 0.092 \end{aligned}$ | 0.180 | 0.251 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SH4+5 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | SH4 | 0.203 | 0.217 | 0.243 | 0.218 | 0.120 | 0.124 | 0.243 |
|  | SH5 | 0.249 | 0.251 | 0.220 | 0.210 | 0.070 | 0.180 | 0.224 |
|  |  | 0.452 | 0.467 | 0.464 | 0.427 | 0.190 |  | 0.467 |
| SH1+2+3 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | SH1 | 0.031 | 0.145 | 0.270 | 0.246 | 0.308 | 0.276 | 0.154 |
|  | SH2 | 0.282 | 0.220 | 0.263 | 0.205 | 0.030 | 0.253 | 0.282 |
|  | SH3 | 0.295 | 0.285 | 0.197 | 0.202 | 0.021 | 0.274 | 0.295 |
|  |  | 0.608 | 0.650 | 0.730 | 0.653 | 0.359 |  | 0.730 |
| SH1+2+4 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | SH1 | 0.031 | 0.145 | 0.270 | 0.246 | 0.308 | 0.276 | 0.251 |
|  | SH2 | 0.282 | 0.220 | 0.263 | 0.205 | 0.030 | 0.253 | 0.282 |
|  | SH4 | 0.203 | 0.217 | 0.243 | 0.218 | 0.120 | 0.124 | 0.243 |
|  |  | 0.516 | 0.582 | 0.776 | 0.669 | 0.457 |  | 0.776 |
| SH1+2+5 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | SH1 | 0.031 | 0.145 | 0.270 | 0.246 | 0.308 | 0.276 | 0.221 |
|  | SH2 | 0.282 | 0.220 | 0.263 | 0.205 | 0.030 | 0.253 | 0.282 |
|  | SH5 | 0.249 | 0.251 | 0.220 | 0.210 | 0.070 | 0.180 | 0.251 |
|  |  | 0.562 | 0.616 | 0.753 | 0.661 | 0.408 |  | 0.753 |
| SH1+3+4 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | SH1 | 0.031 | 0.145 | 0.270 | 0.246 | 0.308 | 0.276 | 0.172 |
|  | SH3 | 0.295 | 0.285 | 0.197 | 0.202 | 0.021 | 0.274 | 0.295 |
|  | SH4 | 0.203 | 0.217 | 0.243 | 0.218 | 0.120 | 0.124 | 0.243 |
|  |  | 0.529 | 0.647 | 0.711 | 0.666 | 0.449 |  | 0.711 |
| SH1+3+5 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | SH1 | 0.031 | 0.145 | 0.270 | 0.246 | 0.308 | 0.276 | 0.142 |
|  | SH3 | 0.295 | 0.285 | 0.197 | 0.202 | 0.021 | 0.274 | 0.295 |
|  | SH5 | 0.249 | 0.251 | 0.220 | 0.210 | 0.070 | 0.180 | 0.251 |
|  |  | 0.575 | 0.681 | 0.688 | 0.658 | 0.399 |  |  |
| SH1+4+5 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | SH1 | 0.031 | 0.145 | 0.270 | 0.246 | 0.308 | 0.276 | 0.239 |
|  | SH4 | 0.203 | 0.217 | 0.243 | 0.218 | 0.120 | 0.124 | 0.243 |
|  | SH5 | 0.249 | 0.251 | 0.220 | 0.210 | 0.070 | 0.180 | 0.251 |
|  |  | 0.483 | 0.612 | 0.734 | 0.674 | 0.498 |  | 0.734 |
| SH2+3+4 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | SH2 | 0.282 | 0.220 | 0.263 | 0.205 | 0.030 | 0.253 | 0.282 |
|  | SH3 | 0.295 | 0.285 | 0.197 | 0.202 | 0.021 | 0.274 | 0.254 |
|  | SH4 | 0.203 | 0.217 | 0.243 | 0.218 | 0.120 | 0.124 | 0.243 |
|  |  | 0.780 | 0.722 | 0.704 | 0.624 | 0.170 |  | 0.780 |
| SH2+3+5 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | SH2 | 0.282 | 0.220 | 0.263 | 0.205 | 0.030 | 0.253 | 0.282 |
|  | SH3 | 0.295 | 0.285 | 0.197 | 0.202 | 0.021 | 0.274 | 0.293 |
|  | SH5 | 0.249 | 0.251 | 0.220 | 0.210 | 0.070 | 0.180 | 0.251 |
|  |  | 0.826 | 0.756 | 0.681 | 0.616 | 0.121 |  | 0.826 |
| SH2+4+5 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | SH2 | 0.282 | 0.220 | 0.263 | 0.205 | 0.030 | 0.253 | 0.239 |
|  | SH4 | 0.203 | 0.217 | 0.243 | 0.218 | 0.120 | 0.124 | 0.243 |
|  | SH5 | 0.249 | 0.251 | 0.220 | 0.210 | 0.070 | 0.180 | 0.251 |
|  |  | 0.734 | 0.687 | 0.727 | 0.632 | 0.219 |  | 0.734 |


| SH3+4+5 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| :---: | :--- | :--- | :--- | :--- | :--- | ---: | ---: |
| SH3 | 0.295 | 0.285 | 0.197 | 0.202 | 0.021 | 0.274 | 0.258 |
| SH4 | 0.203 | 0.217 | 0.243 | 0.218 | 0.120 | 0.124 | 0.243 |
| SH5 | 0.249 | 0.251 | 0.220 | 0.210 | 0.070 | 0.180 | 0.251 |
|  | 0.746 | 0.752 | 0.661 | 0.629 | 0.211 |  | 0.752 |
| SH1+2+3+4 | a 1 | a 2 | a 3 | a 4 | a5 | Max-min | Optimum |
| SH1 | 0.031 | 0.145 | 0.270 | 0.246 | 0.308 | 0.276 | 0.154 |
| SH2 | 0.282 | 0.220 | 0.263 | 0.205 | 0.030 | 0.253 | 0.282 |
| SH3 | 0.295 | 0.285 | 0.197 | 0.202 | 0.021 | 0.274 | 0.295 |
| SH4 | 0.203 | 0.217 | 0.243 | 0.218 | 0.120 | 0.124 | 0.243 |
|  | 0.811 | 0.867 | 0.974 | 0.871 | 0.478 |  | 0.974 |
| SH1+2+3+5 | a 1 | a 2 | a 3 | a 4 | a 5 | Max-min | Optimum |
| SH1 | 0.031 | 0.145 | 0.270 | 0.246 | 0.308 | 0.276 | 0.123 |
| SH2 | 0.282 | 0.220 | 0.263 | 0.205 | 0.030 | 0.253 | 0.282 |
| SH3 | 0.295 | 0.285 | 0.197 | 0.202 | 0.021 | 0.274 | 0.295 |
| SH5 | 0.249 | 0.251 | 0.220 | 0.210 | 0.070 | 0.180 | 0.251 |
|  | 0.857 | 0.901 | 0.951 | 0.863 | 0.429 |  | 0.951 |
| SH1 $+2+4+5$ | a 1 | a 2 | a 3 | a 4 | a 5 | Max-min | Optimum |
| SH1 | 0.031 | 0.145 | 0.270 | 0.246 | 0.308 | 0.276 | 0.221 |
| SH2 | 0.282 | 0.220 | 0.263 | 0.205 | 0.030 | 0.253 | 0.282 |
| SH4 | 0.203 | 0.217 | 0.243 | 0.218 | 0.120 | 0.124 | 0.243 |
| SH5 | 0.249 | 0.251 | 0.220 | 0.210 | 0.070 | 0.180 | 0.251 |
|  | 0.765 | 0.832 | 0.997 | 0.879 | 0.527 |  | 0.997 |
| SH1 $+3+4+5$ | a 1 | a 2 | a 3 | a 4 | a 5 | Max-min | Optimum |
| SH1 | 0.031 | 0.145 | 0.270 | 0.246 | 0.308 | 0.276 | 0.142 |
| SH3 | 0.295 | 0.285 | 0.197 | 0.202 | 0.021 | 0.274 | 0.295 |
| SH4 | 0.203 | 0.217 | 0.243 | 0.218 | 0.120 | 0.124 | 0.243 |
| SH5 | 0.249 | 0.251 | 0.220 | 0.210 | 0.070 | 0.180 | 0.251 |
|  | 0.778 | 0.897 | 0.931 | 0.875 | 0.519 |  | 0.931 |
| SH2 $+3+4+5$ | a 1 | a 2 | a 3 | a 4 | a 5 | Max-min | Optimum |
| SH2 | 0.282 | 0.220 | 0.263 | 0.205 | 0.030 | 0.253 | 0.282 |
| SH3 | 0.295 | 0.285 | 0.197 | 0.202 | 0.021 | 0.274 | 0.252 |
| SH4 | 0.203 | 0.217 | 0.243 | 0.218 | 0.120 | 0.124 | 0.243 |
| SH5 | 0.249 | 0.251 | 0.220 | 0.210 | 0.070 | 0.180 | 0.251 |
|  | 1.028 | 0.972 | 0.925 | 0.834 | 0.241 |  | 1.028 |
|  |  |  |  |  |  |  |  |

Table A-12 Function Payoff Optimum for Each Coalition on Wall System Selection

| Coalition |  |  |  |  |  |  | Alternatives |  |  |  |
| ---: | :--- | :--- | :--- | :--- | :--- | ---: | ---: | :---: | :---: | :---: |
| SH1+2+3+4+5 | a1 | a 2 | a 3 | a 4 | Payoff Optimum |  |  |  |  |  |
| SH1 | 0.254 | 0.220 | 0.301 | 0.162 | 0.063 | 0.238 | Max-min |  |  |  |
| Optimum |  |  |  |  |  |  |  |  |  |  |
| SH2 | 0.147 | 0.196 | 0.123 | 0.145 | 0.389 | 0.265 | 0.389 |  |  |  |
| SH3 | 0.105 | 0.189 | 0.139 | 0.165 | 0.403 | 0.299 | 0.403 |  |  |  |
| SH4 | 0.169 | 0.201 | 0.188 | 0.157 | 0.285 | 0.128 | 0.285 |  |  |  |
| SH5 | 0.137 | 0.195 | 0.163 | 0.161 | 0.344 | 0.208 | 0.344 |  |  |  |
|  | 0.811 | 1.001 | 0.915 | 0.789 | 1.485 |  | 1.485 |  |  |  |
| SH1+2 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |  |  |  |
| SH1 | 0.254 | 0.220 | 0.301 | 0.162 | 0.063 | 0.238 | 0.063 |  |  |  |
| SH2 | 0.147 | 0.196 | 0.123 | 0.145 | 0.389 | 0.265 | 0.389 |  |  |  |
|  | 0.401 | 0.416 | 0.425 | 0.306 | 0.452 |  | 0.452 |  |  |  |


| SH1+3 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { SH1 } \\ & \text { SH3 } \end{aligned}$ | 0.254 | 0.220 | 0.301 | 0.162 | 0.063 | 0.238 | 0.278 |
|  |  | 0.105 | 0.189 | 0.139 | 0.165 | 0.403 | 0.299 | 0.189 |
|  |  | 0.358 | 0.409 | 0.440 | 0.326 | 0.467 |  | 0.467 |
| SH1+4 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | SH1 | 0.254 | 0.220 | 0.301 | 0.162 | 0.063 | 0.238 | 0.204 |
|  | SH4 | 0.169 | 0.201 | 0.188 | 0.157 | 0.285 | 0.128 | 0.285 |
|  |  | 0.422 | 0.421 | 0.489 | 0.319 | 0.349 |  | 0.489 |
| SH1+5 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | $\begin{aligned} & \hline \text { SH1 } \\ & \text { SH5 } \end{aligned}$ | 0.254 | 0.220 | 0.301 | 0.162 | 0.063 | 0.238 | 0.270 |
|  |  | 0.137 | 0.195 | 0.163 | 0.161 | 0.344 | 0.208 | 0.195 |
|  |  | 0.390 | 0.415 | 0.464 | 0.322 | 0.408 |  | 0.464 |
| SH2+3 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | $\begin{aligned} & \mathrm{SH} 2 \\ & \mathrm{SH} 3 \end{aligned}$ | 0.147 | 0.196 | 0.123 | 0.145 | 0.389 | 0.265 | 0.389 |
|  |  | 0.105 | 0.189 | 0.139 | 0.165 | 0.403 | 0.299 | 0.403 |
|  |  | 0.252 | 0.384 | 0.262 | 0.310 | 0.792 |  | 0.792 |
| SH2+4 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | $\begin{aligned} & \mathrm{SH} 2 \\ & \mathrm{SH} 4 \end{aligned}$ | 0.147 | 0.196 | 0.123 | 0.145 | 0.389 | 0.265 | 0.389 |
|  |  | 0.169 | 0.201 | 0.188 | 0.157 | 0.285 | 0.128 | 0.285 |
|  |  | 0.316 | 0.397 | 0.311 | 0.302 | 0.674 |  | 0.674 |
| SH2+5 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | $\begin{aligned} & \text { SH2 } \\ & \text { SH5 } \end{aligned}$ | 0.147 | 0.196 | 0.123 | 0.145 | 0.389 | 0.072 | 0.196 |
|  |  | 0.137 | 0.195 | 0.163 | 0.161 | 0.344 | 0.058 | 0.195 |
|  |  | 0.284 | 0.391 | 0.287 | 0.306 | 0.733 |  |  |
| SH3+4 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | $\begin{aligned} & \hline \text { SH3 } \\ & \text { SH4 } \end{aligned}$ | 0.105 | 0.189 | 0.139 | 0.165 | 0.403 | 0.299 | 0.189 |
|  |  | 0.169 | 0.201 | 0.188 | 0.157 | 0.285 | 0.128 | 0.201 |
|  |  | 0.273 | 0.390 | 0.327 | 0.322 | 0.688 |  | 0.390 |
| SH3+5 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | $\begin{aligned} & \hline \text { SH3 } \\ & \text { SH5 } \end{aligned}$ | 0.105 | 0.189 | 0.139 | 0.165 | 0.403 | 0.299 | 0.403 |
|  |  | 0.137 | 0.195 | 0.163 | 0.161 | 0.344 | 0.208 | 0.344 |
|  |  | 0.241 | 0.384 | 0.302 | 0.326 | 0.747 |  |  |
| SH4+5 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | $\begin{aligned} & \hline \text { SH4 } \\ & \text { SH5 } \end{aligned}$ | 0.169 | 0.201 | 0.188 | 0.157 | 0.285 | 0.128 | 0.285 |
|  |  | 0.137 | 0.195 | 0.163 | 0.161 | 0.344 | 0.208 | 0.344 |
|  |  | 0.305 | 0.396 | 0.351 | 0.318 | 0.629 |  | 0.629 |
| SH1+2+3 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | $\begin{aligned} & \hline \text { SH1 } \\ & \text { SH2 } \\ & \text { SH3 } \end{aligned}$ | 0.254 | 0.220 | 0.301 | 0.162 | 0.063 | 0.238 | 0.063 |
|  |  | 0.147 | 0.196 | 0.123 | 0.145 | 0.389 | 0.265 | 0.389 |
|  |  | 0.105 | 0.189 | 0.139 | 0.165 | 0.403 | 0.299 | 0.403 |
|  |  | 0.506 | 0.604 | 0.563 | 0.471 | 0.855 |  | 0.855 |
| SH1+2+4 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | $\begin{aligned} & \text { SH1 } \\ & \text { SH2 } \\ & \text { SH4 } \end{aligned}$ | 0.254 | 0.220 | 0.301 | 0.162 | 0.063 | 0.238 | 0.063 |
|  |  | 0.147 | 0.196 | 0.123 | 0.145 | 0.389 | 0.265 | 0.389 |
|  |  | 0.169 | 0.201 | 0.188 | 0.157 | 0.285 | 0.128 | 0.285 |
|  |  | 0.570 | 0.617 | 0.612 | 0.463 | 0.737 |  | 0.737 |
| SH1+2+5 |  | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
|  | SH1 | 0.254 | 0.220 | 0.301 | 0.162 | 0.063 | 0.238 | 0.063 |
|  | SH2 | 0.147 | 0.196 | 0.123 | 0.145 | 0.389 | 0.265 | 0.389 |
|  | SH5 | 0.137 | 0.195 | 0.163 | 0.161 | 0.344 | 0.208 | 0.344 |
|  |  | 0.538 | 0.611 | 0.588 | 0.467 | 0.796 |  | 0.796 |


| SH1+3+4 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SH1 | 0.254 | 0.220 | 0.301 | 0.162 | 0.063 | 0.238 | 0.063 |
| SH3 | 0.105 | 0.189 | 0.139 | 0.165 | 0.403 | 0.299 | 0.403 |
| SH4 | 0.169 | 0.201 | 0.188 | 0.157 | 0.285 | 0.128 | 0.285 |
| SH1+3+5 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| SH1 | 0.254 | 0.220 | 0.301 | 0.162 | 0.063 | 0.238 | 0.063 |
| SH3 | 0.105 | 0.189 | 0.139 | 0.165 | 0.403 | 0.299 | 0.403 |
| SH5 | 0.137 | 0.195 | 0.163 | 0.161 | 0.344 | 0.208 | 0.344 |
|  | 0.495 | 0.604 | 0.603 | 0.487 | 0.811 |  |  |
| SH1+4+5 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| SH1 | 0.254 | 0.220 | 0.301 | 0.162 | 0.063 | 0.238 | 0.063 |
| SH4 | 0.169 | 0.201 | 0.188 | 0.157 | 0.285 | 0.128 | 0.285 |
| SH5 | 0.137 | 0.195 | 0.163 | 0.161 | 0.344 | 0.208 | 0.344 |
|  | 0.559 | 0.616 | 0.652 | 0.480 | 0.693 |  | 0.693 |
| SH2+3+4 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| SH2 | 0.147 | 0.196 | 0.123 | 0.145 | 0.389 | 0.265 | 0.389 |
| SH3 | 0.105 | 0.189 | 0.139 | 0.165 | 0.403 | 0.299 | 0.403 |
| SH4 | 0.169 | 0.201 | 0.188 | 0.157 | 0.285 | 0.128 | 0.285 |
|  | 0.421 | 0.586 | 0.450 | 0.467 | 1.077 |  | 1.077 |
| SH2+3+5 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| SH2 | 0.147 | 0.196 | 0.123 | 0.145 | 0.389 | 0.265 | 0.389 |
| SH3 | 0.105 | 0.189 | 0.139 | 0.165 | 0.403 | 0.299 | 0.403 |
| SH5 | 0.137 | 0.195 | 0.163 | 0.161 | 0.344 | 0.208 | 0.344 |
|  | 0.389 | 0.579 | 0.426 | 0.470 | 1.136 |  | 1.136 |
| SH2+4+5 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| SH2 | 0.147 | 0.196 | 0.123 | 0.145 | 0.389 | 0.265 | 0.389 |
| SH4 | 0.169 | 0.201 | 0.188 | 0.157 | 0.285 | 0.128 | 0.285 |
| SH5 | 0.137 | 0.195 | 0.163 | 0.161 | 0.344 | 0.208 | 0.344 |
|  | 0.453 | 0.592 | 0.475 | 0.463 | 1.018 |  | 1.018 |
| SH3+4+5 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| SH3 | 0.105 | 0.189 | 0.139 | 0.165 | 0.403 | 0.299 | 0.403 |
| SH4 | 0.169 | 0.201 | 0.188 | 0.157 | 0.285 | 0.128 | 0.285 |
| SH5 | 0.137 | 0.195 | 0.163 | 0.161 | 0.344 | 0.208 | 0.344 |
|  | 0.410 | 0.585 | 0.490 | 0.483 | 1.032 |  | 1.032 |
| SH1+2+3+4 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| SH1 | 0.254 | 0.220 | 0.301 | 0.162 | 0.063 | 0.238 | 0.063 |
| SH2 | 0.147 | 0.196 | 0.123 | 0.145 | 0.389 | 0.265 | 0.389 |
| SH3 | 0.105 | 0.189 | 0.139 | 0.165 | 0.403 | 0.299 | 0.403 |
| SH4 | 0.169 | 0.201 | 0.188 | 0.157 | 0.285 | 0.128 | 0.285 |
|  | 0.675 | 0.806 | 0.751 | 0.628 | 1.140 |  | 1.140 |
| SH1+2+3+5 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| SH1 | 0.254 | 0.220 | 0.301 | 0.162 | 0.063 | 0.238 | 0.063 |
| SH2 | 0.147 | 0.196 | 0.123 | 0.145 | 0.389 | 0.265 | 0.389 |
| SH3 | 0.105 | 0.189 | 0.139 | 0.165 | 0.403 | 0.299 | 0.403 |
| SH5 | 0.137 | 0.195 | 0.163 | 0.161 | 0.344 | 0.208 | 0.344 |
|  | 0.643 | 0.799 | 0.727 | 0.632 | 1.199 |  | 1.199 |
| SH1+2+4+5 | a1 | a2 | a3 | a4 | a5 | Max-min | Optimum |
| SH1 | 0.254 | 0.220 | 0.301 | 0.162 | 0.063 | 0.238 | 0.063 |
| SH2 | 0.147 | 0.196 | 0.123 | 0.145 | 0.389 | 0.265 | 0.389 |
| SH4 | 0.169 | 0.201 | 0.188 | 0.157 | 0.285 | 0.128 | 0.285 |
| SH5 | 0.137 | 0.195 | 0.163 | 0.161 | 0.344 | 0.208 | 0.344 |


|  | 0.707 | 0.812 | 0.776 | 0.624 | 1.081 |  | 1.081 |
| :---: | :--- | :--- | :--- | :--- | :--- | ---: | ---: |
| SH1 $+3+4+5$ | a 1 | a 2 | a 3 | a 4 | a 5 | Max-min | Optimum |
| SH1 | 0.254 | 0.220 | 0.301 | 0.162 | 0.063 | 0.238 | 0.063 |
| SH3 | 0.105 | 0.189 | 0.139 | 0.165 | 0.403 | 0.299 | 0.403 |
| SH4 | 0.169 | 0.201 | 0.188 | 0.157 | 0.285 | 0.128 | 0.285 |
| SH5 | 0.137 | 0.195 | 0.163 | 0.161 | 0.344 | 0.208 | 0.344 |
|  | 0.664 | 0.805 | 0.791 | 0.644 | 1.096 |  | 1.096 |
| SH2+3+4+5 | a 1 | a 2 | a 3 | a 4 | a 5 | Max-min | Optimum |
| SH2 | 0.147 | 0.196 | 0.123 | 0.145 | 0.389 | 0.265 | 0.389 |
| SH3 | 0.105 | 0.189 | 0.139 | 0.165 | 0.403 | 0.299 | 0.403 |
| SH4 | 0.169 | 0.201 | 0.188 | 0.157 | 0.285 | 0.128 | 0.285 |
| SH5 | 0.137 | 0.195 | 0.163 | 0.161 | 0.344 | 0.208 | 0.344 |
|  | 0.557 | 0.781 | 0.613 | 0.627 | 1.421 |  | 1.421 |

Payoff optimum for cost and function become the data for the best fit options algorithm. The result of the process is presented at stage (5) below.
(5) Analyzing the best fit option for every coalition and grand coalition.

The result is presented on Table A-13. It shows the priorities that followed the best fit options process and algorithm in Equation 6.5 in Chapter Six. It also presents the result of priorities of the technical solution for wall system in the first negotiation round.

Table A-13 Ranking of Wall System Options for each Coalition

| No | Alternative ranking and <br> coalition | Alternatives |  |  |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathbf{a 2}$ | $\mathbf{a 3}$ | $\mathbf{a 4}$ | $\mathbf{a 5}$ |  |
| 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2 | SH 1 (Property Manager) | $2^{\text {nd }}$ | $1^{\text {st }}$ | $4^{\text {th }}$ | $5^{\text {th }}$ | $3^{\text {rd }}$ |
| 3 | SH 2 (Project Manager) | $1^{\text {st }}$ | $4^{\text {th }}$ | $2^{\text {nd }}$ | $5^{\text {th }}$ | $3^{\text {rd }}$ |
| 4 | SH 3 (Architect) | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $5^{\text {th }}$ | $4^{\text {th }}$ | $1^{\text {st }}$ |
| 5 | SH 4 (QS) | $1^{\text {st }}$ | $2^{\text {nd }}$ | $4^{\text {th }}$ | $5^{\text {th }}$ | $3^{\text {rd }}$ |
| 6 | SH 5 (Engineer) | $2^{\text {nd }}$ | $1^{\text {st }}$ | $4^{\text {th }}$ | $5^{\text {th }}$ | $3^{\text {rd }}$ |
| 7 | Coalition SH1,2 | $4^{\text {th }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $1^{\text {st }}$ | $5^{\text {th }}$ |
| 8 | Coalition SH1,3 | $4^{\text {th }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $1^{\text {st }}$ | $5^{\text {th }}$ |
| 9 | Coalition SH1,4 | $4^{\text {th }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $1^{\text {st }}$ | $5^{\text {th }}$ |
| 10 | Coalition SH1,5 | $4^{\text {th }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $1^{\text {st }}$ | $5^{\text {th }}$ |
| 11 | Coalition SH2,3 | $5^{\text {th }}$ | $3^{\text {rd }}$ | $4^{\text {th }}$ | $2^{\text {nd }}$ | $1^{\text {st }}$ |
| 12 | Coalition SH2,4 | $4^{\text {th }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $1^{\text {st }}$ | $5^{\text {th }}$ |
| 13 | Coalition SH2,5 | $1^{\text {st }}$ | $3^{\text {rd }}$ | $4^{\text {th }}$ | $2^{\text {nd }}$ | $5^{\text {th }}$ |
| 14 | Coalition SH3,4 | $5^{\text {th }}$ | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $1^{\text {st }}$ | $4^{\text {th }}$ |
| 15 | Coalition SH3,5 | $5^{\text {th }}$ | $4^{\text {th }}$ | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $1^{\text {st }}$ |
| 16 | Coalition SH4,5 | $5^{\text {th }}$ | $4^{\text {th }}$ | $3^{\text {rd }}$ | $1^{\text {st }}$ | $2^{\text {nd }}$ |
| 17 | Coalition SH1,2,3 | $4^{\text {th }}$ | $5^{\text {th }}$ | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $1^{\text {st }}$ |


| No | Alternative ranking and | Alternatives |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  | $\mathbf{a 1}$ | $\mathbf{a 2}$ | $\mathbf{a 3}$ | $\mathbf{a 4}$ | $\mathbf{a 5}^{\text {a }}$ |
| 18 |  | $3^{\text {rd }}$ | $5^{\text {th }}$ | $2^{\text {nd }}$ | $1^{\text {st }}$ | $4^{\text {th }}$ |
| 19 | Coalition SH1,2,5 | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $4^{\text {th }}$ | $1^{\text {st }}$ | $5^{\text {th }}$ |
| 20 | Coalition SH1,3,4 | $2^{\text {nd }}$ | $4^{\text {th }}$ | $3^{\text {rd }}$ | $1^{\text {st }}$ | $5^{\text {th }}$ |
| 21 | Coalition SH1,3,5 | $4^{\text {th }}$ | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $1^{\text {st }}$ | $5^{\text {th }}$ |
| 22 | Coalition SH1,4,5 | $4^{\text {th }}$ | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $1^{\text {st }}$ | $5^{\text {th }}$ |
| 23 | Coalition SH2,3,4 | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $4^{\text {th }}$ | $1^{\text {st }}$ | $5^{\text {th }}$ |
| 24 | Coalition SH2,3,5 | $5^{\text {th }}$ | $2^{\text {nd }}$ | $4^{\text {th }}$ | $1^{\text {st }}$ | $3^{\text {rd }}$ |
| 25 | Coalition SH2,4,5 | $4^{\text {th }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $1^{\text {st }}$ | $5^{\text {th }}$ |
| 26 | Coalition SH3,4,5 | $4^{\text {th }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $1^{\text {st }}$ | $5^{\text {th }}$ |
| 27 | Coalition SH1,2,3,4 | $4^{\text {th }}$ | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $1^{\text {st }}$ | $5^{\text {th }}$ |
| 28 | Coalition SH1,2,3,5 | $4^{\text {th }}$ | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $1^{\text {st }}$ | $5^{\text {th }}$ |
| 29 | Coalition SH1,2,4,5 | $4^{\text {th }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $1^{\text {st }}$ | $5^{\text {th }}$ |
| 30 | Coalition SH1,3,4,5 | $4^{\text {th }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $1^{\text {st }}$ | $5^{\text {th }}$ |
| 31 | Coalition SH2,3,4,5 | $5^{\text {th }}$ | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $1^{\text {st }}$ | $4^{\text {th }}$ |
| 32 | Coalition SH1,2,3,4,5 | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $4^{\text {th }}$ | $1^{\text {st }}$ | $5^{\text {th }}$ |
| Result | $3^{\text {rd }}$ | $4^{\text {th }}$ | - | $1^{\text {st }}$ | $2^{\text {nd }}$ |  |

### 2.7 Similarity Index

The result of similarity index is presented on Table A-14. The similarity index shows that the coalition algorithm model gives satisfaction to all stakeholders.

Table A-14 Similarity Index Result for Wall System Selection

|  | Model 1: <br> Single weighting | Model 2: <br> Aggregation | Model 3: <br> Coalition algorithm |
| :--- | :---: | :---: | :---: |
| Stakeholder 1 | $>1=1$ | $>1=1$ | 0.466823 |
| Stakeholder 2 | $>1=1$ | 0.660666 | 0.151679 |
| Stakeholder 3 | 1 | 0.664501 | 0.199419 |
| Stakeholder 4 | $>1=1$ | $>1=1$ | 0.008331 |
| Stakeholder 5 | $>1=1$ | 0.79176 | 0.142212 |

### 2.8 Conclusion of the Case Study

In this case study, solutions a3 is not options for wall system. Table A-13 also indicates the alternative solution that will be determined to be the best fit solution. In the first negotiation round a4 was the 'best fit' solution for the group. It means that timber wall panel is the best technical solution for wall system. This result is very interesting because on the individual stakeholder preferences, no one choose a4.

## Case study 3: Highway Guardrail Selection

### 3.1 Background

This case study involved making decision on highway guardrail model in a big housing complex developed by a private company. The decision attributes were set based on previous studies and standard function analysis in ASTM 2004. In this case, a highway guardrail was selected (Utomo, et al., 2009c). Five decision makers were involved namely Estate Manager, Project Manager, QS, In-house Designer, and Engineer.

The original design was concrete guardrail with faces on both sides, reinforced with concrete footing. The guardrail composed of two elements: concrete and stone. The use of concrete in guardrail is to "ensure safety" and the causative function is to "provide barrier", while the use of stone is mainly only to "enhance appearance". After studying numerous possible functions of the guardrail, it was determined that the guardrail should fulfill the followings:
a. Protect traffic.
b. Prevent crossover by errant driver.
c. Deflect vehicle by minimizing (vehicle) damage.
d. Protect property.
e. Enhance appearance.
f. Reduce maintenance.

Since the face of the guardrail that is facing the road receives the impact of vehicle it is assigned the function "deflect vehicle". This face should be readily replaceable after damage. The "deflect vehicle" function could be accomplished at a lesser cost by using concrete. Since all functions are equally important, therefore the cost will be equally divided. However, if one function is significantly more important than the others then the total cost is assigned to that function and other functions will be assigned zero. On the other hand, if each function is weighted differently then the cost will be allocated according to their weightage. The cost of the concrete wall was divided into three functions, which were to protect traffic, prevent crossover, and
reduce maintenance. The metal plate guardrail could achieve "protect traffic" on lower level roadway. The concrete wall footing was built below the grade to eliminate settlement by frost action, and the cost for it was allocated to the function "reduce maintenance".

### 3.2 Function Analysis of Highway Guardrail

Function analysis of highway guardrail is presented in Figure A-22. It consists of four sequential steps in a function analysis. Figure A-22 presents the FAST diagram of highway guardrail that consists of six functions to ensure safety by providing barrier. The functions are 'protect traffic', 'prevent crossover', 'deflect vehicle', 'protect property', 'reduce maintenance', and 'enhance appearance'.


Figure A-22 FAST Diagram of Highway Guardrail

### 3.3 Life Cycle Cost of Highway Guardrail

Based on Equation (2.1) in Chapter Two, a cost driver of highway guardrail was calculated. Table A-15 presents LCC and the initial cost.

Table A-15 Cost of Highway Guardrail

| Cost category | Present Worth (1000USD) |  |  |
| :--- | ---: | ---: | ---: | ---: |
|  | a1 (metal plate) | a2 (concrete wall) | a3 (wooden-faced) |
| Initial | 4900 | 2200 | 3400 |
| LCC | 160000 | 220000 | 350000 |

### 3.4 Highway Guardrail Selection

Figure A- 23 shows that the goal of the problem on highway guardrail selection (G $=$ "to assure safety by provide barrier") is addressed by some alternatives $(A=a 1$; $a 2$; a3) which are metal plate guardrail, concrete wall footing, and wooden-faced guardrail. The problem is split into evaluating criteria (f1; f2; f3; f4; f5; f6; c1; c2) which are protect traffic, prevent crossover, deflect vehicle, protect property, reduce maintenance, enhance appearance, initial cost and Life Cycle Cost (LCC).

The result from the decision is presented in Table A-16. It shows the ranking of each guardrail solution based on individual stakeholder. Group ranking based on aggregation value of all stakeholder value is also presented in this table. This aggregation value will be compared with the value from the coalition formation among stakeholder.

> Guardrail
> "To ensure safety by providing barrier" (G)


Figure A-23 Decision Hierarchy to Choose Highway Guardrail
Table A-16 Weighting Factor of Each Guardrail Solutions for Individual Stakeholder

| Estate Manager |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | f1 | f2 | f3 | f4 | f5 | f6 | c1 | c2 | Weight | Ranking |
|  | 0.100 | 0.095 | 0.076 | 0.072 | 0.347 | 0.022 | 0.029 | 0.259 |  |  |
| a1 | 0.028 | 0.060 | 0.023 | 0.009 | 0.220 | 0.003 | 0.007 | 0.150 | 0.4988 | $1^{\text {st }}$ |
| a2 | 0.059 | 0.025 | 0.012 | 0.017 | 0.090 | 0.005 | 0.019 | 0.080 | 0.3076 | $2^{\text {nd }}$ |
| a3 | 0.013 | 0.010 | 0.041 | 0.047 | 0.037 | 0.015 | 0.004 | 0.028 | 0.1935 | $3^{\text {rd }}$ |
| Project Manager |  |  |  |  |  |  |  |  |  |  |
|  | f1 | f2 | f3 | f4 | f5 | f6 | c1 | c2 | Weight | Ranking |
|  | 0.134 | 0.080 | 0.051 | 0.026 | 0.037 | 0.188 | 0.353 | 0.130 | Weight | Ranking |
| a1 | 0.037 | 0.051 | 0.015 | 0.003 | 0.023 | 0.023 | 0.081 | 0.076 | 0.3095 | $2^{\text {nd }}$ |
| a2 | 0.079 | 0.021 | 0.008 | 0.006 | 0.010 | 0.043 | 0.229 | 0.040 | 0.4369 | $1^{\text {st }}$ |
| a3 | 0.017 | 0.009 | 0.028 | 0.017 | 0.004 | 0.122 | 0.043 | 0.014 | 0.2536 | $3^{\text {rd }}$ |


| QS |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | f1 | f2 | f3 | f4 | f5 | f6 | c1 | c2 | Weight | Ranking |
|  | 0.133 | 0.051 | 0.046 | 0.070 | 0.047 | 0.098 | 0.199 | 0.356 |  |  |
| a1 | 0.037 | 0.032 | 0.014 | 0.009 | 0.030 | 0.012 | 0.046 | 0.207 | 0.3859 | $2^{\text {nd }}$ |
| a2 | 0.079 | 0.013 | 0.008 | 0.016 | 0.012 | 0.022 | 0.129 | 0.110 | 0.3899 | $1^{\text {st }}$ |
| a3 | 0.017 | 0.005 | 0.025 | 0.045 | 0.005 | 0.063 | 0.024 | 0.039 | 0.2243 | $3^{\text {rd }}$ |
| In-house Designer |  |  |  |  |  |  |  |  |  |  |
|  | f1 | f2 | f3 | f4 | f5 | f6 | c1 | c2 | Weight | Ranking |
|  | 0.186 | 0.029 | 0.049 | 0.036 | 0.182 | 0.334 | 0.129 | 0.056 |  |  |
| a1 | 0.051 | 0.018 | 0.015 | 0.004 | 0.115 | 0.041 | 0.030 | 0.032 | 0.3067 | $3{ }^{\text {rd }}$ |
| a2 | 0.110 | 0.008 | 0.008 | 0.008 | 0.047 | 0.077 | 0.083 | 0.017 | 0.3589 | $1^{\text {st }}$ |
| a3 | 0.024 | 0.003 | 0.027 | 0.023 | 0.019 | 0.216 | 0.016 | 0.006 | 0.3343 | $2^{\text {nd }}$ |
| Engineer |  |  |  |  |  |  |  |  |  |  |
|  | f1 | f2 | f3 | f4 | f5 | f6 | c1 | c2 | Weight | Ranking |
|  | 0.107 | 0.272 | 0.176 | 0.069 | 0.100 | 0.187 | 0.042 | 0.047 |  |  |
| a1 | 0.030 | 0.173 | 0.052 | 0.008 | 0.063 | 0.023 | 0.010 | 0.028 | 0.3860 | $1^{\text {st }}$ |
| a2 | 0.064 | 0.071 | 0.029 | 0.016 | 0.026 | 0.043 | 0.027 | 0.015 | 0.2900 | $3^{\text {rd }}$ |
| a3 | 0.014 | 0.029 | 0.095 | 0.045 | 0.011 | 0.121 | 0.005 | 0.005 | 0.3241 | $2^{\text {nd }}$ |
| Aggregation |  |  |  |  |  |  |  |  |  |  |
|  | f1 | f2 | f3 | f4 | f5 | f6 | c1 | c2 |  |  |
|  | 0.107 | 0.272 | 0.176 | 0.069 | 0.100 | 0.187 | 0.042 | 0.047 | Weight | Ranking |
| a1 | 0.036 | 0.067 | 0.024 | 0.007 | 0.090 | 0.020 | 0.035 | 0.099 | 0.3774 | $1^{\text {st }}$ |
| a2 | 0.078 | 0.028 | 0.013 | 0.013 | 0.037 | 0.038 | 0.098 | 0.052 | 0.3567 | $2^{\text {nd }}$ |
| a3 | 0.017 | 0.011 | 0.043 | 0.035 | 0.015 | 0.107 | 0.018 | 0.019 | 0.2660 | $3^{\text {rd }}$ |

### 3.5 Satisfying Option on Value Criteria

In this case study, initial cost and LCC are identified as 'Cost' and the other six functions which are 'protect traffic', 'prevent crossover', 'deflect vehicle', 'protect property', 'reduce maintenance', and 'enhance appearance’ as 'Function'. Table A-17 shows the selectability (Ps) and rejectability (Pr) that represent function and cost of technical solution of highway guardrail respectively.

Table A-17 Cost and Function of Highway Guardrail Options

|  | Cost |  |  |  | Function |  |  |  |  |  | Normalization |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | c1 | c2 | Total | Loss | f1 | f2 | f3 | f4 | f5 | f6 | Cost (Pr) | Function <br> (Ps) |  |
| a1 | 0.230 | 0.581 | 0.811 | 0.378 | 0.277 | 0.633 | 0.297 | 0.122 | 0.633 | 0.122 | 0.241 | 0.347 |  |
| a2 | 0.648 | 0.309 | 0.957 | 0.232 | 0.595 | 0.260 | 0.164 | 0.230 | 0.260 | 0.230 | 0.148 | 0.290 |  |
| a3 | 0.122 | 0.110 | 0.232 | 0.957 | 0.129 | 0.106 | 0.539 | 0.648 | 0.106 | 0.648 | 0.611 | 0.363 |  |

Based on the result presented on Table A-17, Figure A-24 provides a cross plot of function of the technical solution options. In this case the highest basic value is a2.


Figure A-24 Basic Value of Highway Guardrail Options

Figures A-25, A-26, A-27, A-28 and A-29 provide cross plots of function and cost for five stakeholders. It means that the basic value of technical solution presented in Figure A-24 will be changed by preferences of stakeholders.

Estate Manager


Figure A-25 Value of Highway Guardrail Options for Estate Manager

Project Manager


Figure A-26 Value of Highway Guardrail Options for Project Manager


Figure A-27 Value of Highway Guardrail Options for QS

## Design in house



Figure A-28 Value of Highway Guardrail Options for In-house Designer


Figure A-29 Value of Highway Guardrail Options for Engineer

### 3.6 Agreement Options and Coalition

(1) Determining the weighting factor (weight of preferences) of criteria for each stakeholder.

Figure A-30 reveals different preferences among stakeholders.


Figure A-30 Weight of Preferences for Each Stakeholder
(2) Grading alternative for each evaluation criteria.

Figure A-31 shows that a3 is the 'best fit' for $\mathrm{f} 3, \mathrm{f} 4$, and f 6 meanwhile a 1 is the 'best fit' for f 2 , f 5 , and c 2 . The 'best fit' solution for fl and c 1 is a 2 .


Figure A-31 Weighting Factor of Every Alternative for Each Criteria
(3) Scoring every alternative for each stakeholder.

Figure A-32 shows that each stakeholder has different best option as a solution alternative.


Figure A-32 Weighting Factor of Every Alternative for Each Stakeholder

## (4) Determining payoff optimum

Table A-18 and A-19 show process and result for Cost and Function payoff optimum.

Table A-18 Cost Payoff Optimum for Each Coalition on Highway Guardrail Selection

| Coalition |  |  | Alternatives |  | Payoff Optimum |  |
| :--- | :--- | :--- | :--- | :--- | ---: | ---: |
| SH1+2+3+4+5 |  | a 1 | a 2 | a 3 | Max-min | Optimum |
|  | SH1 | 0.442 | 0.225 | 0.333 | 0.217 | 0.442 |
|  | SH2 | 0.360 | 0.266 | 0.374 | 0.108 | 0.374 |
|  | SH3 | 0.503 | 0.152 | 0.345 | 0.351 | 0.503 |
|  | SH4 | 0.491 | 0.085 | 0.423 | 0.406 | 0.491 |
|  | SH5 | 0.567 | 0.137 | 0.297 | 0.430 | 0.553 |
|  | 2.363 | 0.865 | 1.772 |  | 2.363 |  |
| SH1+2 | a 1 | a 2 | a 3 | Max-min | Optimum |  |
|  | SH1 | 0.442 | 0.225 | 0.333 | 0.217 | 0.428 |
|  | SH2 | 0.360 | 0.266 | 0.374 | 0.108 | 0.374 |
|  |  | 0.802 | 0.491 | 0.707 |  | 0.802 |
| SH1+3 |  | a 1 | a 2 | a 3 | Max-min | Optimum |
|  | SH1 | 0.442 | 0.225 | 0.333 | 0.217 | 0.442 |
|  | SH3 | 0.503 | 0.152 | 0.345 | 0.351 | 0.503 |
|  |  | 0.945 | 0.377 | 0.678 |  | 0.945 |
| SH1+4 | a 1 | a 2 | a 3 | Max-min | Optimum |  |
|  | SH1 | 0.442 | 0.225 | 0.333 | 0.217 | 0.442 |
|  | SH4 | 0.491 | 0.085 | 0.423 | 0.406 | 0.491 |
|  |  | 0.933 | 0.310 | 0.757 |  | 0.933 |
| SH1+5 |  | a 1 | a 2 | a 3 | Max-min | Optimum |
|  | SH1 | 0.442 | 0.225 | 0.333 | 0.217 | 0.442 |
|  | SH5 | 0.567 | 0.137 | 0.297 | 0.430 | 0.567 |
|  |  | 1.009 | 0.362 | 0.630 |  | 1.009 |


| SH2+3 |  | a1 | a2 | a3 | Max-min | Optimum |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SH2 | 0.360 | 0.266 | 0.374 | 0.108 | 0.374 |
|  | SH3 | 0.503 | 0.152 | 0.345 | 0.351 | 0.489 |
|  |  | 0.863 | 0.418 | 0.719 |  | 0.863 |
| SH2+4 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH2 | 0.360 | 0.266 | 0.374 | 0.108 | 0.360 |
|  | SH4 | 0.491 | 0.085 | 0.423 | 0.406 | 0.491 |
|  |  | 0.851 | 0.351 | 0.797 |  | 0.851 |
| SH2+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH2 | 0.360 | 0.266 | 0.374 | 0.108 | 0.374 |
|  | SH5 | 0.567 | 0.137 | 0.297 | 0.430 | 0.553 |
|  |  | 0.927 | 0.403 | 0.670 |  |  |
| SH3+4 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH3 | 0.503 | 0.152 | 0.345 | 0.351 | 0.503 |
|  | SH4 | 0.491 | 0.085 | 0.423 | 0.406 | 0.491 |
|  |  | 0.994 | 0.237 | 0.769 |  | 0.994 |
| SH3+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH3 | 0.503 | 0.152 | 0.345 | 0.351 | 0.503 |
|  | SH5 | 0.567 | 0.137 | 0.297 | 0.430 | 0.567 |
|  |  | 1.070 | 0.288 | 0.642 |  |  |
| SH4+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH4 | 0.491 | 0.085 | 0.423 | 0.406 | 0.491 |
|  | SH5 | 0.567 | 0.137 | 0.297 | 0.430 | 0.567 |
|  |  | 1.058 | 0.222 | 0.720 |  | 1.058 |
| SH1+2+3 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.442 | 0.225 | 0.333 | 0.217 | 0.428 |
|  | SH2 | 0.360 | 0.266 | 0.374 | 0.108 | 0.374 |
|  | SH3 | 0.503 | 0.152 | 0.345 | 0.351 | 0.503 |
|  |  | 1.305 | 0.643 | 1.052 |  | 1.305 |
| SH1+2+4 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.442 | 0.225 | 0.333 | 0.217 | 0.428 |
|  | SH2 | 0.360 | 0.266 | 0.374 | 0.108 | 0.374 |
|  | SH4 | 0.491 | 0.085 | 0.423 | 0.406 | 0.491 |
|  |  | 1.293 | 0.576 | 1.130 |  | 1.293 |
| SH1+2+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.442 | 0.225 | 0.333 | 0.217 | 0.428 |
|  | SH2 | 0.360 | 0.266 | 0.374 | 0.108 | 0.374 |
|  | SH5 | 0.567 | 0.137 | 0.297 | 0.430 | 0.567 |
|  |  | 1.369 | 0.628 | 1.004 |  | 1.369 |
| SH1+3+4 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.442 | 0.225 | 0.333 | 0.217 | 0.442 |
|  | SH3 | 0.503 | 0.152 | 0.345 | 0.351 | 0.503 |
|  | SH4 | 0.491 | 0.085 | 0.423 | 0.406 | 0.491 |
|  |  | 1.436 | 0.462 | 1.102 |  | 1.436 |
| SH1+3+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.442 | 0.225 | 0.333 | 0.217 | 0.442 |
|  | SH3 | 0.503 | 0.152 | 0.345 | 0.351 | 0.503 |
|  | SH5 | 0.567 | 0.137 | 0.297 | 0.430 | 0.567 |
|  |  | 1.512 | 0.513 | 0.975 |  |  |


| SH1+4+5 |  | a1 | a2 | a3 | Max-min | Optimum |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SH1 | 0.442 | 0.225 | 0.333 | 0.217 | 0.442 |
|  | SH4 | 0.491 | 0.085 | 0.423 | 0.406 | 0.491 |
|  | SH5 | 0.567 | 0.137 | 0.297 | 0.430 | 0.567 |
|  |  | 1.500 | 0.447 | 1.053 |  | 1.500 |
| SH2+3+4 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH2 | 0.360 | 0.266 | 0.374 | 0.108 | 0.374 |
|  | SH3 | 0.503 | 0.152 | 0.345 | 0.351 | 0.489 |
|  | SH4 | 0.491 | 0.085 | 0.423 | 0.406 | 0.491 |
|  |  | 1.354 | 0.503 | 1.143 |  | 1.354 |
| SH2+3+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH2 | 0.360 | 0.266 | 0.374 | 0.108 | 0.374 |
|  | SH3 | 0.503 | 0.152 | 0.345 | 0.351 | 0.489 |
|  | SH5 | 0.567 | 0.137 | 0.297 | 0.430 | 0.567 |
|  |  | 1.430 | 0.554 | 1.016 |  | 1.430 |
| SH2+4+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH2 | 0.360 | 0.266 | 0.374 | 0.108 | 0.360 |
|  | SH4 | 0.491 | 0.085 | 0.423 | 0.406 | 0.491 |
|  | SH5 | 0.567 | 0.137 | 0.297 | 0.430 | 0.567 |
|  |  | 1.418 | 0.488 | 1.094 |  | 1.418 |
| SH3+4+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH3 | 0.503 | 0.152 | 0.345 | 0.351 | 0.503 |
|  | SH4 | 0.491 | 0.085 | 0.423 | 0.406 | 0.491 |
|  | SH5 | 0.567 | 0.137 | 0.297 | 0.430 | 0.567 |
|  |  | 1.561 | 0.374 | 1.066 |  | 1.561 |
| SH1+2+3+4 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.442 | 0.225 | 0.333 | 0.217 | 0.428 |
|  | SH2 | 0.360 | 0.266 | 0.374 | 0.108 | 0.374 |
|  | SH3 | 0.503 | 0.152 | 0.345 | 0.351 | 0.503 |
|  | SH4 | 0.491 | 0.085 | 0.423 | 0.406 | 0.491 |
|  |  | 1.796 | 0.728 | 1.476 |  | 1.796 |
| SH1+2+3+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.442 | 0.225 | 0.333 | 0.217 | 0.428 |
|  | SH2 | 0.360 | 0.266 | 0.374 | 0.108 | 0.374 |
|  | SH3 | 0.503 | 0.152 | 0.345 | 0.351 | 0.503 |
|  | SH5 | 0.567 | 0.137 | 0.297 | 0.430 | 0.567 |
|  |  | 1.872 | 0.779 | 1.349 |  | 1.872 |
| SH1+2+4+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.442 | 0.225 | 0.333 | 0.217 | 0.428 |
|  | SH2 | 0.360 | 0.266 | 0.374 | 0.108 | 0.374 |
|  | SH4 | 0.491 | 0.085 | 0.423 | 0.406 | 0.491 |
|  | SH5 | 0.567 | 0.137 | 0.297 | 0.430 | 0.567 |
|  |  | 1.860 | 0.713 | 1.427 |  | 1.860 |
| SH1+3+4+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.442 | 0.225 | 0.333 | 0.217 | 0.442 |
|  | SH3 | 0.503 | 0.152 | 0.345 | 0.351 | 0.503 |
|  | SH4 | 0.491 | 0.085 | 0.423 | 0.406 | 0.491 |
|  | SH5 | 0.567 | 0.137 | 0.297 | 0.430 | 0.567 |
|  |  | 2.003 | 0.599 | 1.399 |  | 2.003 |


| SH2 $+3+4+5$ |  | a1 | a2 | a3 | Max-min | Optimum |
| :--- | :--- | :--- | :--- | :--- | ---: | ---: |
|  | SH2 | 0.360 | 0.266 | 0.374 | 0.108 | 0.374 |
|  | SH3 | 0.503 | 0.152 | 0.345 | 0.351 | 0.489 |
|  | SH4 | 0.491 | 0.085 | 0.423 | 0.406 | 0.491 |
|  | SH5 | 0.567 | 0.137 | 0.297 | 0.430 | 0.567 |
|  |  | 1.921 | 0.640 | 1.439 |  | 1.921 |

Table A-19 Function Payoff Optimum for Each Coalition on Highway Guardrail

| Coalition |  | Alternatives |  |  | Payoff Optimum |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SH1+2+3+4+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.557 | 0.260 | 0.183 | 0.374 | 0.557 |
|  | SH2 | 0.568 | 0.257 | 0.175 | 0.393 | 0.568 |
|  | SH3 | 0.544 | 0.266 | 0.190 | 0.354 | 0.544 |
|  | SH4 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  | SH5 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 2.780 | 1.302 | 0.918 |  | 2.780 |
| SH1+2 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.557 | 0.260 | 0.183 | 0.374 | 0.557 |
|  | SH2 | 0.568 | 0.257 | 0.175 | 0.393 | 0.568 |
|  |  | 1.125 | 0.517 | 0.358 |  | 1.125 |
| SH1+3 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.557 | 0.260 | 0.183 | 0.374 | 0.557 |
|  | SH3 | 0.544 | 0.266 | 0.190 | 0.354 | 0.544 |
|  |  | 1.101 | 0.526 | 0.373 |  | 1.101 |
| SH1+4 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.557 | 0.260 | 0.183 | 0.374 | 0.557 |
|  | SH4 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 1.113 | 0.519 | 0.368 |  | 1.113 |
| SH1+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.557 | 0.260 | 0.183 | 0.374 | 0.557 |
|  | SH5 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 1.113 | 0.519 | 0.368 |  | 1.113 |
| SH2+3 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH2 | 0.568 | 0.257 | 0.175 | 0.393 | 0.568 |
|  | SH3 | 0.544 | 0.266 | 0.190 | 0.354 | 0.544 |
|  |  | 1.111 | 0.523 | 0.365 |  | 1.111 |
| SH2+4 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH2 | 0.568 | 0.257 | 0.175 | 0.393 | 0.568 |
|  | SH4 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 1.124 | 0.516 | 0.360 |  | 1.124 |
| SH2+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH2 | 0.568 | 0.257 | 0.175 | 0.393 | 0.568 |
|  | SH5 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 1.124 | 0.516 | 0.360 |  |  |
| SH3+4 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH3 | 0.544 | 0.266 | 0.190 | 0.354 | 0.544 |
|  | SH4 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 1.100 | 0.526 | 0.375 |  | 1.100 |


| SH3+5 |  | a1 | a2 | a3 | Max-min | Optimum |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SH3 | 0.544 | 0.266 | 0.190 | 0.354 | 0.544 |
|  | SH5 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 1.100 | 0.526 | 0.375 |  |  |
| SH4+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH4 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  | SH5 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 1.112 | 0.519 | 0.369 |  | 1.112 |
| SH1+2+3 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.557 | 0.260 | 0.183 | 0.374 | 0.557 |
|  | SH2 | 0.568 | 0.257 | 0.175 | 0.393 | 0.568 |
|  | SH3 | 0.544 | 0.266 | 0.190 | 0.354 | 0.544 |
|  |  | 1.668 | 0.783 | 0.548 |  | 1.668 |
| SH1+2+4 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.557 | 0.260 | 0.183 | 0.374 | 0.557 |
|  | SH2 | 0.568 | 0.257 | 0.175 | 0.393 | 0.568 |
|  | SH4 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 1.681 | 0.776 | 0.543 |  | 1.681 |
| SH1+2+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.557 | 0.260 | 0.183 | 0.374 | 0.557 |
|  | SH2 | 0.568 | 0.257 | 0.175 | 0.393 | 0.568 |
|  | SH5 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 1.681 | 0.776 | 0.543 |  | 1.681 |
| SH1+3+4 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.557 | 0.260 | 0.183 | 0.374 | 0.557 |
|  | SH3 | 0.544 | 0.266 | 0.190 | 0.354 | 0.544 |
|  | SH4 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 1.657 | 0.786 | 0.558 |  | 1.657 |
| SH1+3+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.557 | 0.260 | 0.183 | 0.374 | 0.557 |
|  | SH3 | 0.544 | 0.266 | 0.190 | 0.354 | 0.544 |
|  | SH5 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 1.657 | 0.786 | 0.558 |  |  |
| SH1+4+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.557 | 0.260 | 0.183 | 0.374 | 0.557 |
|  | SH4 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  | SH5 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 1.669 | 0.779 | 0.552 |  | 1.669 |
| SH2+3+4 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH2 | 0.568 | 0.257 | 0.175 | 0.393 | 0.568 |
|  | SH3 | 0.544 | 0.266 | 0.190 | 0.354 | 0.544 |
|  | SH4 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 1.667 | 0.783 | 0.550 |  | 1.667 |
| SH2+3+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH2 | 0.568 | 0.257 | 0.175 | 0.393 | 0.568 |
|  | SH3 | 0.544 | 0.266 | 0.190 | 0.354 | 0.544 |
|  | SH5 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 1.667 | 0.783 | 0.550 |  | 1.667 |


| SH2+4+5 |  | a1 | a2 | a3 | Max-min | Optimum |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SH2 | 0.568 | 0.257 | 0.175 | 0.393 | 0.568 |
|  | SH4 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  | SH5 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 1.680 | 0.776 | 0.545 |  | 1.680 |
| SH3+4+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH3 | 0.544 | 0.266 | 0.190 | 0.354 | 0.544 |
|  | SH4 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  | SH5 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 1.656 | 0.785 | 0.559 |  | 1.656 |
| SH1+2+3+4 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.557 | 0.260 | 0.183 | 0.374 | 0.557 |
|  | SH2 | 0.568 | 0.257 | 0.175 | 0.393 | 0.568 |
|  | SH3 | 0.544 | 0.266 | 0.190 | 0.354 | 0.544 |
|  | SH4 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 2.224 | 1.043 | 0.733 |  | 2.224 |
| SH1+2+3+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.557 | 0.260 | 0.183 | 0.374 | 0.557 |
|  | SH2 | 0.568 | 0.257 | 0.175 | 0.393 | 0.568 |
|  | SH3 | 0.544 | 0.266 | 0.190 | 0.354 | 0.544 |
|  | SH5 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 2.224 | 1.043 | 0.733 |  | 2.224 |
| SH1+2+4+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.557 | 0.260 | 0.183 | 0.374 | 0.557 |
|  | SH2 | 0.568 | 0.257 | 0.175 | 0.393 | 0.568 |
|  | SH4 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  | SH5 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 2.237 | 1.036 | 0.728 |  | 2.237 |
| SH1+3+4+5 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.557 | 0.260 | 0.183 | 0.374 | 0.557 |
|  | SH3 | 0.544 | 0.266 | 0.190 | 0.354 | 0.544 |
|  | SH4 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  | SH5 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 2.213 | 1.045 | 0.742 |  | 2.213 |
| $\mathrm{SH} 2+3+4+5$ |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH2 | 0.568 | 0.257 | 0.175 | 0.393 | 0.568 |
|  | SH3 | 0.544 | 0.266 | 0.190 | 0.354 | 0.544 |
|  | SH4 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  | SH5 | 0.556 | 0.259 | 0.185 | 0.371 | 0.556 |
|  |  | 2.223 | 1.042 | 0.735 |  | 2.223 |

(5) Analyzing the best fit options for every coalition and grand coalition.

The results of analyzing the best fit option using coalition algorithm in Chapter 6 are presented on Table A-20. It shows the priorities that followed the 'best fit' options process including the priorities of the technical solution for highway guardrail in the first negotiation round.

Table A-20 Ranking of Highway Guardrail Solution for Each Coalition

|  | Alternative ranking and coalition | Alternatives |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | a1 | a2 | a3 |
| 1 | 0 | 0 | 0 | 0 |
| 2 | SH 1 (Estate Manager) | $1^{\text {st }}$ | $2^{\text {nd }}$ | $3{ }^{\text {rd }}$ |
| 3 | SH 2 (Project Manager) | $2^{\text {nd }}$ | $1^{\text {st }}$ | $3^{\text {rd }}$ |
| 4 | SH 3 (QS) | $2^{\text {nd }}$ | $1^{\text {st }}$ | $3^{\text {rd }}$ |
| 5 | SH 4 (In-house Designer) | $3^{\text {rd }}$ | $1^{\text {st }}$ | $2^{\text {nd }}$ |
| 6 | SH 5 (Engineer) | $1^{\text {st }}$ | $3^{\text {rd }}$ | $2^{\text {nd }}$ |
| 7 | Coalition SH1 and SH2 | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $1^{\text {st }}$ |
| 8 | Coalition SH1 and SH3 | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $1^{\text {st }}$ |
| 9 | Coalition SH1 and SH4 | $1{ }^{\text {st }}$ | $3^{\text {rd }}$ | $2^{\text {nd }}$ |
| 10 | Coalition SH1 and SH5 | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $1^{\text {st }}$ |
| 11 | Coalition SH2 and SH3 | $3^{\text {rd }}$ | $1{ }^{\text {st }}$ | $2^{\text {nd }}$ |
| 12 | Coalition SH2 and SH4 | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $1^{\text {st }}$ |
| 13 | Coalition SH2 and SH5 | $3^{\text {rd }}$ | $1{ }^{\text {st }}$ | $2^{\text {nd }}$ |
| 14 | Coalition SH3 and SH4 | $1{ }^{\text {st }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ |
| 15 | Coalition SH3 and SH5 | $1^{\text {st }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ |
| 16 | Coalition SH4 and SH5 | $1{ }^{\text {st }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ |
| 17 | Coalition SH1, SH2, and SH3 | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $1^{\text {st }}$ |
| 18 | Coalition SH1, SH2, and SH4 | $3^{\text {rd }}$ | $1^{\text {st }}$ | $2^{\text {nd }}$ |
| 19 | Coalition SH1, SH2, and SH5 | $3^{\text {rd }}$ | $1^{\text {st }}$ | $2^{\text {nd }}$ |
| 20 | Coalition SH1, SH3, and SH4 | $1{ }^{\text {st }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ |
| 21 | Coalition SH1, SH3, and SH5 | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $1{ }^{\text {st }}$ |
| 22 | Coalition SH1, SH4, and SH5 | $1{ }^{\text {st }}$ | $3^{\text {rd }}$ | $2^{\text {nd }}$ |
| 23 | Coalition SH2, SH3, and SH4 | $3^{\text {rd }}$ | $1^{\text {st }}$ | $2^{\text {nd }}$ |
| 24 | Coalition SH2, SH3, and SH5 | $2^{\text {nd }}$ | $1^{\text {st }}$ | $3^{\text {rd }}$ |
| 25 | Coalition SH2, SH4, and SH5 | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $1^{\text {st }}$ |
| 26 | Coalition SH3, SH4, and SH5 | $1{ }^{\text {st }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ |
| 27 | Coalition SH1, SH2, SH3, SH4 | $3^{\text {rd }}$ | $1{ }^{\text {st }}$ | $2^{\text {nd }}$ |
| 28 | Coalition SH1, SH2, SH3, SH5 | $3^{\text {rd }}$ | $1^{\text {st }}$ | $2^{\text {nd }}$ |
| 29 | Coalition SH1, SH2, SH4, SH5 | $1{ }^{\text {st }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ |
| 30 | Coalition SH1, SH3, SH4, SH5 | $1^{\text {st }}$ | $3^{\text {rd }}$ | $2^{\text {nd }}$ |
| 31 | Coalition SH2, SH3, SH4, SH5 | $3^{\text {rd }}$ | $1{ }^{\text {st }}$ | $2^{\text {nd }}$ |
| 32 | Coalition SH1, SH2, SH3, SH4, SH5 | $3^{\text {rd }}$ | $1^{\text {st }}$ | $2^{\text {nd }}$ |
| RESULT |  | $2^{\text {nd }}$ | $1^{\text {st }}$ | $3^{\text {rd }}$ |

### 3.7 Similarity Index

The result of similarity index is presented on Table A-21. The table shows that the coalition algorithm model gives satisfaction to all stakeholders.

Table A-21 Similarity Index Result for Highway Guardrail Selection

|  | Model 1: <br> Single weighting | Model 2: <br> Aggregation | Model 3: <br> Coalition algorithm |
| :---: | :---: | :---: | :---: |
| Stakeholder 1 | $>1=1$ | 0.934065 | 0.772583 |
| Stakeholder 2 | 1 | 0.643977 | 0.55980 |
| Stakeholder 3 | $>1=1$ | $>1=1$ | 0.840685 |
| Stakeholder 4 | $>1=1$ | 0.927939 | 0.80472 |
| Stakeholder 5 | $>1=1$ | $>1=1$ | 0.996691 |

### 3.8 Conclusion of the Case Study

In this case study, concrete wall footing (a2) was the best technical solution for 'ensuring safety by providing barrier' a2 was the 'best fit' solution for the group. The result from the first round of negotiation is presented in Table A-20. The table indicates that all solutions are chosen by more than one stakeholder and coalitions. This means that all solutions become possible solution for the highway guardrail.

Observed on a3 (wooden-faced guardrail), the result is interesting. Even though this solution has no first priority by any stakeholder, this solution is chosen by many coalitions as the best fit option. On the next round of negotiation, stakeholder 1 and 5 can offer different preference by trade-off process. They can also decide to accept a2 as the best fit solution. Under this condition where all stakeholders agree with the result from first round, negotiation end.

## Case study 4: Support Bridge Selection

### 4.1 Background

This case study was on the selection of suitable material for a support bridge structure (Utomo, et al., 2009e) involving three decision makers, who are an Estate Manager, Project Manager, and Engineer. There are three alternative solutions for the material of the support bridge structure, which are (a1) steel, (a2) reinforced concrete and (a3) wood.

### 4.2 Function Analysis of Support Bridge

The functions of Support Bridge are identified by performing FAST analysis on the problem. Fig. 2 shows the FAST diagram; the identified function will become the attributes for decision.


Figure A-33 FAST Diagram of the Support Bridge

### 4.3 Life Cycle Cost of the Support Bridge

The cost of the support bridge was calculated; here the energy cost was not calculated because its cost is not involved in a support bridge. Table A-22 presents LCC and initial cost (including investment cost). Similar to the other three case studies, Equation (2.3) was used to calculate the O\&M cost since these costs have annual
basis. Equation (2.2) was used for replacement cost since this cost has variability in period.

Table A-22 Cost of the Support Bridge

| Cost category | Present Worth (1000USD) |  |  |
| :---: | :---: | :---: | :---: |
|  | a 1 | a 2 | a 3 |
| Initial | 8102 | 5600 | 3720 |
| LCC | 40135 | 22625 | 55320 |

### 4.4 Support Bridge Selection

Figure A-34 shows four levels of decision hierarchy. The goal $(\mathrm{G})$ of the problem is "To select the best choice for Support Bridge". The goal is addressed by some alternatives $(\mathrm{A}=\mathrm{a} 1 ; \mathrm{a} 2 ; \mathrm{a} 3)$ which are steel bridge structure, reinforced bridge structure, and wooden bridge structure respectively. The problem is split into two value criteria namely Function $(\mathrm{Cf})$ and Cost $(\mathrm{Cc})$, which are divided further into respective sub-criteria $\mathrm{f} 1, \mathrm{f} 2, \mathrm{f} 3, \mathrm{f} 4, \mathrm{f} 5, \mathrm{f} 6, \mathrm{f} 7, \mathrm{f} 8$, and c 1 and c 2 .


Figure A-34 Decision Hierarchy to Choose Support Bridge

Table A-23 Weighting Factor of Each Alternative to Each Stakeholder

|  | Synthesis from AHP judgment and calculation on 3 Stakeholders |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (f1) | (f2) | (f3) | (f4) | (f5) | (f6) | (f7) | (f8) | (c1) | (c2) | Weight |
| Stakeholder 1 (Estate Manager) |  |  |  |  |  |  |  |  |  |  |  |
| a1 (steel bridge) | 0.045 | 0.024 | 0.027 | 0.086 | 0.114 | 0.046 | 0.006 | 0.023 | 0.004 | 0.038 | 0.414 |
| a2 (reinforced concrete) | 0.023 | 0.009 | 0.007 | 0.037 | 0.025 | 0.016 | 0.049 | 0.013 | 0.009 | 0.146 | 0.334 |
| a3 (wooden) | 0.008 | 0.005 | 0.014 | 0.023 | 0.053 | 0.010 | 0.028 | 0.059 | 0.029 | 0.024 | 0.252 |
| Stakeholder 2 (Project Manager) |  |  |  |  |  |  |  |  |  |  |  |
| a1 (steel bridge) | 0.020 | 0.016 | 0.013 | 0.021 | 0.003 | 0.011 | 0.008 | 0.026 | 0.093 | 0.021 | 0.232 |
| a2 (reinforced concrete) | 0.012 | 0.006 | 0.005 | 0.012 | 0.015 | 0.035 | 0.040 | 0.021 | 0.410 | 0.080 | 0.634 |
| a3 (wooden) | 0.004 | 0.004 | 0.006 | 0.006 | 0.002 | 0.005 | 0.021 | 0.023 | 0.053 | 0.011 | 0.134 |
| Stakeholder 3 (Engineer) |  |  |  |  |  |  |  |  |  |  |  |
| a1 (steel bridge) | 0.046 | 0.031 | 0.034 | 0.051 | 0.030 | 0.065 | 0.012 | 0.045 | 0.002 | 0.020 | 0.335 |
| a2 (reinforced concrete) | 0.027 | 0.014 | 0.008 | 0.025 | 0.005 | 0.030 | 0.079 | 0.023 | 0.010 | 0.096 | 0.317 |
| a3 (wooden) | 0.008 | 0.009 | 0.013 | 0.013 | 0.010 | 0.020 | 0.044 | 0.217 | 0.004 | 0.012 | 0.349 |

### 4.5 Satisfying Option on Value Criteria

In this case study, initial cost and LCC are identified as 'Cost' and all 6 other functions which are 'received load', 'resist shift', 'receive forced'. Allow mini distortion', 'resist strike', 'resist erosion', 'fix elements', and 'beauty appearance' are identified as 'Function'. Table A-24 shows the selectability (Ps) and rejectability (Pr) that represent function and cost of support bridge solutions. An option will be a rejectability options if the value of the options is below $\mathrm{F} / \mathrm{C}=1$ or the cost is higher than the function. In other word it can be said that there is unnecessary cost in the technical solution option.

Table A-24 Cost and Function of Support Bridge Options

|  | Cost |  |  |  | Function |  |  |  |  |  |  |  | Normalization |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | c1 | c2 | $\sum$ | Loss | f1 | f2 | f3 | f4 | f5 | f6 | f7 | f8 | $\begin{aligned} & \text { Cost } \\ & \text { (Pr) } \\ & \hline \hline \end{aligned}$ | Function (Ps) |
| a1 | 0.10 | 0.18 | 0.28 | 0.91 | 0.60 | 0.62 | 0.57 | 0.59 | 0.59 | 0.64 | 0.08 | 0.24 | 0.57 | 0.49 |
| a2 | 0.21 | 0.70 | 0.91 | 0.28 | 0.30 | 0.24 | 0.14 | 0.25 | 0.13 | 0.23 | 0.59 | 0.14 | 0.18 | 0.25 |
| a3 | 0.69 | 0.11 | 0.80 | 0.40 | 0.10 | 0.14 | 0.29 | 0.16 | 0.28 | 0.14 | 0.33 | 0.62 | 0.25 | 0.26 |

Figure A-35 provides a cross plot of function of the technical solution options. The figure is based on the result from Table A-24. Observe that although al has the highest function, it also has the high cost which resulted in its value below $\mathrm{F} / \mathrm{C}=1$. In this case study, the highest value is a2 since it gives the highest satisfaction due to its low function and low cost.

Basic Value of Support Bridge


Figure A-35 Basic Value of Support Bridge Options

Figures A-36, A-37, and A-38 provide cross plots of function and cost of the estate manager, project manager, and engineer respectively. Observe the influence of the estate manager's preference on a1. Basically that a1 is a rejected option since it has a value less than $\mathrm{F} / \mathrm{C}=1$. The estate manager's preference changes it to a value more than $\mathrm{F} / \mathrm{C}=1$, which made it to fall into selectability options.


Figure A-36 Value of Support Bridge Options for Estate Manager

Project Manager


Figure A-37 Value of Support Bridge Options for Project Manager


Figure A-38 Value of Support Bridge Options for Engineer

### 4.6 Agreement Options and Coalition

(1) Determining the weighting factor (weight of preferences) of each criteria for each stakeholder and the aggregation.

Based on the pair wise comparison of each criterion, Figure A-39 reveals the different preferences among the three stakeholders.


Figure A-39 Weight of Preferences for Each Stakeholder
(2) Grading alternative for each evaluation criteria.

Figure A-40 shows that a1 is the 'best fit' for f1, f2, f3, f4, f5, and f6. The 'best fit' solution for c 1 and f 8 is a 3 , and a 2 for c 2 and f 7 .


Figure A-40 Weighting Factor of Every Alternative for Each Criteria
(3) Scoring every alternative for every stakeholder.

Figure A-41 shows that each stakeholder has different best option as the solution alternative. Here, before conducting negotiation, the estate manager chose steel structure as the best choice; the project manager chose reinforced concrete structure, while the engineer chose wooden bridge structure as the best choice.


Figure A-41 Weighting Factor of Every Alternative for Each Stakeholder

## (4) Determining payoff optimum

The payoff optimum for every stakeholder and every alternative was determined by using Equations 6.1-6.4, and the values are tabulated on Tables A-25 and A26 for Cost and Function respectively.

Table A-25 Cost Payoff Optimum for Each Coalition on Support Bridge Selection

| Coalition |  | Alternatives |  |  | Payoff Optimum |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| SH1+2+3 | a1 |  | a2 |  | a3 | Max-min |
| Optimum |  |  |  |  |  |  |
|  | SH1 | 0.455 | 0.123 | 0.422 | 0.331 | 0.455 |
|  | SH2 | 0.443 | 0.064 | 0.493 | 0.429 | 0.461 |
|  | SH3 | 0.450 | 0.072 | 0.477 | 0.405 | 0.477 |
|  |  | 1.348 | 0.260 | 1.393 |  |  |
| SH1+2 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.455 | 0.123 | 0.422 | 0.331 | 0.455 |
|  | SH2 | 0.443 | 0.064 | 0.493 | 0.429 | 0.461 |
|  |  | 0.897 | 0.188 | 0.915 |  |  |
| SH1+3 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.455 | 0.123 | 0.422 | 0.331 | 0.455 |
|  | SH3 | 0.450 | 0.072 | 0.477 | 0.405 | 0.450 |
|  |  | 0.905 | 0.195 | 0.900 |  |  |
| SH2+3 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH2 | 0.443 | 0.064 | 0.493 | 0.429 | 0.493 |
|  | SH3 | 0.450 | 0.072 | 0.477 | 0.405 | 0.477 |
|  |  | 0.893 | 0.136 | 0.970 |  |  |

Table A-26 Function Payoff Optimum for Each Coalition on Support Bridge Selection

| Coalition |  | Alternatives |  |  | Payoff Optimum |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| SH1+2+3 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.495 | 0.239 | 0.267 | 0.256 | 0.388 |
|  | SH2 | 0.352 | 0.436 | 0.212 | 0.224 | 0.436 |
|  | SH3 | 0.366 | 0.246 | 0.389 | 0.143 | 0.389 |
|  |  | 1.212 | 0.920 | 0.867 |  |  |
| SH1+2 |  | a 1 | a 2 | a 3 | Max-min | Optimum |
|  | SH1 | 0.495 | 0.239 | 0.267 | 0.256 | 0.411 |
|  | SH2 | 0.352 | 0.436 | 0.212 | 0.224 | 0.436 |
|  |  | 0.847 | 0.674 | 0.479 |  |  |
| SH1+3 |  | a 1 | a 2 | a 3 | Max-min | Optimum |
|  | SH1 | 0.495 | 0.239 | 0.267 | 0.256 | 0.471 |
|  | SH3 | 0.366 | 0.246 | 0.389 | 0.143 | 0.389 |
|  |  | 0.860 | 0.484 | 0.655 |  |  |
| SH2+3 |  | a 1 | a 2 | a 2 | Max-min | Optimum |
|  | SH2 | 0.352 | 0.436 | 0.212 | 0.224 | 0.436 |
|  | SH3 | 0.366 | 0.246 | 0.389 | 0.143 | 0.282 |
|  |  | 0.718 | 0.681 | 0.601 |  |  |

(5) Analyzing the best fit options for every coalition and grand coalition.

The results are presented on Table A-27. It shows the best fit option process. It also presents the ranking of the technical solutions for Support Bridge.

Table A-27 Ranking of Support Bridge Solutions for Every Coalition

| Alternative ranking and coalition | Priorities |  |  |
| :--- | :---: | :---: | :---: |
|  | a 1 | a 2 | a 3 |
| SH 1 (Estate Manager) | $1^{\text {st }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ |
| SH 2 (Project Manager) | $2^{\text {nd }}$ | $1^{\text {st }}$ | $3^{\text {rd }}$ |
| SH 3 (Engineer) | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $1^{\text {st }}$ |
| Aggregation | $2^{\text {nd }}$ | $1^{\text {st }}$ | $3^{\text {rd }}$ |
| Coalition SH1 and SH2 | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $1^{\text {st }}$ |
| Coalition SH1 and SH3 | $2^{\text {nd }}$ | $1^{\text {st }}$ | $3^{\text {rd }}$ |
| Coalition SH2 and SH3 | $1^{\text {st }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ |
| Grand coalition | $1^{\text {sd }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ |
| RESULT | $1^{\text {st }}$ | $2^{\text {nd }}$ | $3^{\text {rd }}$ |

### 4.7 Similarity Index

The result of similarity index is presented on Table A-28. The table shows that coalition algorithm model gives satisfaction to all stakeholders.

Table A-28 Similarity Index Result for Support Bridge Selection

|  | Model 1: <br> Single weighting | Model 2: <br> Aggregation | Model 3: <br> Coalition algorithm |
| :---: | :---: | :---: | :---: |
| Stakeholder 1 | $>1=1$ | $>1=1$ | 0.45625 |
| Stakeholder 2 | 1 | 0.588 | 0.384 |
| Stakeholder 3 | $>1=1$ | $>1=1$ | 0.28125 |

### 4.8 Conclusion of the Case Study

Firstly, individually all stakeholder have their own best solution. Finally, as shown on Table A-27, steel structure (a1) is found to be the 'best fit' solution for all stakeholders after coalition. On this case, it can be observed that the best solution based on aggregation is different with the best solution after coalition formation. This finding is supported by the result in Figure A-40. This figure shows that al have the highest weighting factor on the six criteria from the ten criteria.

## Case study 5: Building Energy System Selection

### 5.1 Background

The need to provide energy-efficient design is becoming more important. This is especially true in relationship to the design life of a project. A means of accounting for the energy uses for the construction and operation of a building is therefore needed. New building designs display an increasing awareness of sustainability but invariability assumed a certain level of technical sustainability, and concentrates more on economic and social sustainability. At times it is difficult to quantify and qualify the importance of value other than those relating to only cost. In this case study, decision must be made on the energy system for affordable housing (Utomo, et al., 2008b) involving three groups of decision makers namely Design Management, Facility Management and Project Management.

The available alternatives for a building energy system are:

1. Passive energy. This alternative utilizes an architectural concept of passive energy buildings; maximum opening wall for natural lighting and air conditioning.
2. Electrical equipment. It utilizes electrical equipments for example, lighting and air conditioners.
'User processes'. The utilization of energy for a building depends on the 'user processes'. It processes through out life cycle of buildings; a building is equipped with electrical wiring but no electrical equipments are provided.

### 5.2 Function Analysis of Building Energy System

Based on the process of FAST, there are three sustainability functions that are technical, economic, and social sustainability. Figure A-42 presents the function together with the life cycle cost of technical solution. For some functions it may be decided that a set of generic process is needed to perform the function, each of which will give rise to an associated set of possible specific processes. A number of processes may be identified as being probable candidates for performing the function.

In this case study there are three functions of sustainability, which are technical, economic, and social.


Figure A-42 FAST Diagram of Building Energy System

### 5.3 Life Cycle Cost of Building Energy System

In all of case studies, salvage value was not calculated because it was not a practice in Indonesia. Table A-29 presents LCC and the proportion for each category; initial cost (including investment cost), energy cost, operation and maintenance (O\&M) cost, and replacement cost. It is difficult to separate energy system cost from the total cost of housing because some of the energy system is part of the housing system.

Table A- 29 Life Cycle Cost of Building Energy System

| Cost category | Present Worth of alternatives (USD1000) |  |  |
| :--- | ---: | :---: | :---: |
|  | Passive energy | Electrical equipment | User |
|  |  |  |  |
| Initial | 2102 | 1600 | 1720 |
| Energy | 135 | 625 | 320 |
| Operation \& Maintenance | 1115 | 3200 | 1600 |
| Replacement | 83 | 316 | 236 |
| Total Cost | 3437 | 5741 | 3876 |

### 5.4 Building Energy System Selection

Figure A-43 shows a model of decision hierarchy based on LCC and sustainable function for an affordable public housing and infrastructure in Indonesia. Each of the
objects in this model contains attribute representing their various properties and different preferences. The goal of the problem ( $\mathrm{G}=$ ="to select energy system of a building in sustainability function") is addressed by some alternatives ( $\mathrm{A}=\mathrm{a}$; ; a ; a3). The problem is split into subproblems (c1, c2, c3, c4, f1, f2, f3) which are the evaluation criteria. Three stakeholders were involved and each has their own preference. The result based on individual judgment is presented on Table A-30.


Figure A-43 Decision Hierarchy of Building Energy System Selection

Table A-30 Weighting Factor of Each Alternative for Individual Stakeholder

|  | c1 | c2 | c3 | c4 | f1 | f2 | f3 | WEIGTH |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Stakeholder 1 (Facility Management) |  |  |  |  |  |  |  |  |
| a1 | 0.0020 | 0.0286 | 0.0642 | 0.2499 | 0.0136 | 0.0496 | 0.0335 | 0.4415 |
| a2 | 0.0075 | 0.0054 | 0.0054 | 0.0471 | 0.0504 | 0.0202 | 0.0145 | 0.1506 |
| a3 | 0.0172 | 0.0152 | 0.0192 | 0.0887 | 0.0216 | 0.1206 | 0.1256 | 0.4079 |
| Stakeholder 2 (Design Management) |  |  |  |  |  |  |  |  |
| a1 | 0.0030 | 0.0293 | 0.2182 | 0.0575 | 0.0292 | 0.0578 | 0.0219 | 0.4168 |
| a2 | 0.0114 | 0.0055 | 0.0185 | 0.0108 | 0.1080 | 0.0235 | 0.0095 | 0.1872 |
| a3 | 0.0260 | 0.0156 | 0.0651 | 0.0204 | 0.0462 | 0.1405 | 0.0822 | 0.3959 |
| Stakeholder 3 (Project Management) |  |  |  |  |  |  |  |  |
| a1 | 0.0255 | 0.0135 | 0.0532 | 0.0259 | 0.0436 | 0.0410 | 0.0168 | 0.2194 |
| a2 | 0.0977 | 0.0026 | 0.0045 | 0.0049 | 0.1611 | 0.0167 | 0.0072 | 0.2946 |
| a3 | 0.2223 | 0.0072 | 0.0159 | 0.0092 | 0.0689 | 0.0997 | 0.0629 | 0.4860 |

### 5.5 Satisfying Option on Value Criteria

The technical solution options for building energy system were categorized into 'Cost' identified by initial cost, replacement cost, energy cost, and operation and
maintenance cost; and 'Function' by all three functions. Table A-31 shows the selectability (Ps) and rejectability (Pr) that represent function and cost of technical solution of building energy system respectively.

Table A-31 Cost and Function of Building Energy Options

|  | Cost |  |  |  |  | Function |  |  |  | Normalization |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | c 1 | c 2 | c 3 | c 4 | $\sum$ | Loss | F1 | F2 | F3 | Cost (Pr) | Function (Ps) |
| a1 (passive) | 0.07 | 0.58 | 0.72 | 0.65 | 2.03 | 0.58 | 0.16 | 0.26 | 0.19 | 0.151 | 0.204 |
| a2 (electric) | 0.28 | 0.11 | 0.06 | 0.12 | 0.58 | 2.03 | 0.59 | 0.11 | 0.08 | 0.532 | 0.259 |
| a3 (user) | 0.64 | 0.31 | 0.22 | 0.23 | 1.40 | 1.20 | 0.25 | 0.63 | 0.72 | 0.316 | 0.536 |

Based on the result presented on Table A-31, Figure A-44 provides a cross plots of function of the technical solution options. In this case the highest value is a3. It gives highest satisfaction since it has the highest function and medium cost.


Figure A-44 Basic Value of Building Energy System

Figures A-45, A-46, and A-47 provide a cross plots of function and cost of facility management, design management, and project management respectively. Observe the influence of project management preference influence on al. Basically al has value more than $\mathrm{F} / \mathrm{C}=1$. The project management's preference changed it to a value of less than $\mathrm{F} / \mathrm{C}=1$.

Facility Management


Figure A-45 Value of Building Energy System Options for Facility Management

Design Management


Figure A-46 Value of Building Energy System Options for Design Management


Figure A-47 Value of Building Energy System Options for Project Management

### 5.6 Agreement Options and Coalition

(1) Determining the weighting factor (weight of preferences) of criteria for each decision-maker.

Figure A-48 reveals different preferences among stakeholders.


- initialcost ■ replacost 图 energycost 目omcost $\square$ tech sus soci sus

Figure A-48 Weight of Building Energy Criteria for Individual Stakeholder
(2) Grading alternative for each evaluation criteria.

Figure A-49 shows that every criteria has different priorities of options.


Figure A-49 Weighting Factor of Every Alternative for Each Criteria
(3) Scoring every alternative for every decision-maker.

Figure A-50 shows that every stakeholder has different alternative solutions. But only two alternatives are identified as the best options, which are aland a3.


Figure A-50 Weighting Factor of Every Alternative for Each Stakeholder
(4) Determining payoff optimum

Table A-32 and A-33 present the process and result of payoff optimum for Cost and Function respectively.

Table A-32 Cost Payoff Optimum on Building Energy System Selection for Each Coalition

| Coalition |  | Alternatives |  |  | Payoff Optimum |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| SH1+2+3 |  | a1 | a2 |  | a3 | Max-min |
|  | Optimum |  |  |  |  |  |
|  | SH1 | 0.096 | 0.507 | 0.397 | 0.410 | 0.507 |
|  | SH2 | 0.080 | 0.530 | 0.391 | 0.450 | 0.530 |
|  | SH3 | 0.403 | 0.417 | 0.180 | 0.237 | 0.417 |
|  |  | 0.579 | 1.454 | 0.967 |  | 1.454 |
| SH1+2 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.096 | 0.507 | 0.397 | 0.410 | 0.507 |
|  | SH2 | 0.080 | 0.530 | 0.391 | 0.450 | 0.530 |
|  |  | 0.176 | 1.036 | 0.788 |  | 1.036 |
| SH1+3 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.096 | 0.507 | 0.397 | 0.410 | 0.507 |
|  | SH3 | 0.403 | 0.417 | 0.180 | 0.237 | 0.417 |
|  |  | 0.500 | 0.924 | 0.577 |  | 0.924 |
| SH2+3 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH2 | 0.080 | 0.530 | 0.391 | 0.450 | 0.530 |
|  | SH3 | 0.403 | 0.417 | 0.180 | 0.237 | 0.417 |
|  |  | 0.483 | 0.947 | 0.570 |  | 0.947 |

Table A-33 Function Payoff Optimum on Building Energy Selection for Each Coalition

| Coalition |  | Alternatives |  |  | Payoff Optimum |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| SH1+2+3 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.215 | 0.189 | 0.596 | 0.406 | 0.596 |
|  | SH2 | 0.210 | 0.272 | 0.518 | 0.308 | 0.518 |
|  | SH3 | 0.196 | 0.357 | 0.447 | 0.251 | 0.447 |
|  |  | 0.621 | 0.818 | 1.561 |  | 1.561 |
| SH1+2 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.215 | 0.189 | 0.596 | 0.406 | 0.596 |
|  | SH2 | 0.210 | 0.272 | 0.518 | 0.308 | 0.518 |
|  |  | 0.425 | 0.461 | 1.114 |  | 1.114 |
| SH1+3 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH1 | 0.215 | 0.189 | 0.596 | 0.406 | 0.596 |
|  | SH3 | 0.196 | 0.357 | 0.447 | 0.251 | 0.447 |
|  |  | 0.411 | 0.547 | 1.042 |  | 1.042 |
| SH2+3 |  | a1 | a2 | a3 | Max-min | Optimum |
|  | SH2 | 0.210 | 0.272 | 0.518 | 0.308 | 0.518 |
|  | SH3 | 0.196 | 0.357 | 0.447 | 0.251 | 0.447 |
|  |  | 0.406 | 0.629 | 0.965 |  | 0.965 |

(5) Analyzing the best fit options for every coalition and grand coalition.

The result is presented on Table A-34. It also presents the result of priorities of the technical solution for building energy system selection in the first negotiation round.

Table A-34 Ranking of Building Energy System Solution on Each Coalition

| Alternatives ranking for each <br> stakeholder and coalition | Ranking of alternatives |  |  |
| :--- | :---: | :---: | :---: |
|  | a 1 | a 2 | a 3 |
|  | $1^{\text {st }}$ | $3^{\text {rd }}$ | $2^{\text {nd }}$ |
| SH2 (Design Management) | $1^{\text {st }}$ | $3^{\text {rd }}$ | $2^{\text {nd }}$ |
| SH3 (Project Management) | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $1^{\text {st }}$ |
| Coalition SH1 and SH2 | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $1^{\text {st }}$ |
| Coalition SH1 and SH3 | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $1^{\text {st }}$ |
| Coalition SH2 and SH3 | $3^{\text {rd }}$ | $2^{\text {nd }}$ | $1^{\text {st }}$ |
| Grand Coalition | $2^{\text {nd }}$ | $3^{\text {rd }}$ | $1^{\text {st }}$ |
| RESULT | $2^{\text {nd }}$ | - | $1^{\text {st }}$ |

### 5.7 Similarity Index

The result of similarity index is presented on Table A-35. The table shows that coalition algorithm model gives satisfaction to all stakeholders.

Table A-35 Similarity Index Result for Building Energy System Selection

|  | Model 1: <br> Single weighting | Model 2: <br> Aggregation | Model 3: <br> Coalition algorithm |
| :---: | :---: | :---: | :---: |
| Stakeholder 1 | $>1=1$ | 0.960261 | 0.884608 |
| Stakeholder 2 | $>1=1$ | $>1=1$ | 0.961113 |
| Stakeholder 3 | 1 | 0.789802 | 0.707244 |

### 5.8 Conclusion of the case study

In this case, electrical equipment (a2) is not an option because no one or coalition selects this solution as an option. Table A-34 indicates that 'user process' (a3) is the best solution. The results are supported by Figure A-49. This figure indicates that both a3 and a1 (passive energy) have the highest weighting factor on three criteria. Solution a2 has only one criteria with highest weighting factor which is technical sustainability.

