

UNIVERSITI  
TEKNOLOGI  
PETRONAS

## FINAL EXAMINATION MAY 2024 SEMESTER

**COURSE : CEB2063/CFB2063 - SEPARATION PROCESS II**  
**DATE : 5 AUGUST 2024 (MONDAY)**  
**TIME : 9.00 AM - 12.00 NOON (3 HOURS)**

### INSTRUCTIONS TO CANDIDATES

1. Answer **ALL** questions in the Answer Booklet.
2. Begin **EACH** answer on a new page in the Answer Booklet.
3. Indicate clearly answers that are cancelled, if any.
4. Where applicable, show clearly steps taken in arriving at the solutions and indicate **ALL** assumptions, if any.
5. **DO NOT** open this Question Booklet until instructed.

**Note :**

- i. There are **NINE (9)** pages in this Question Booklet including the cover page and appendices.
- ii. **DOUBLE-SIDED** Question Booklet.
- iii. **Graph paper will be provided.**

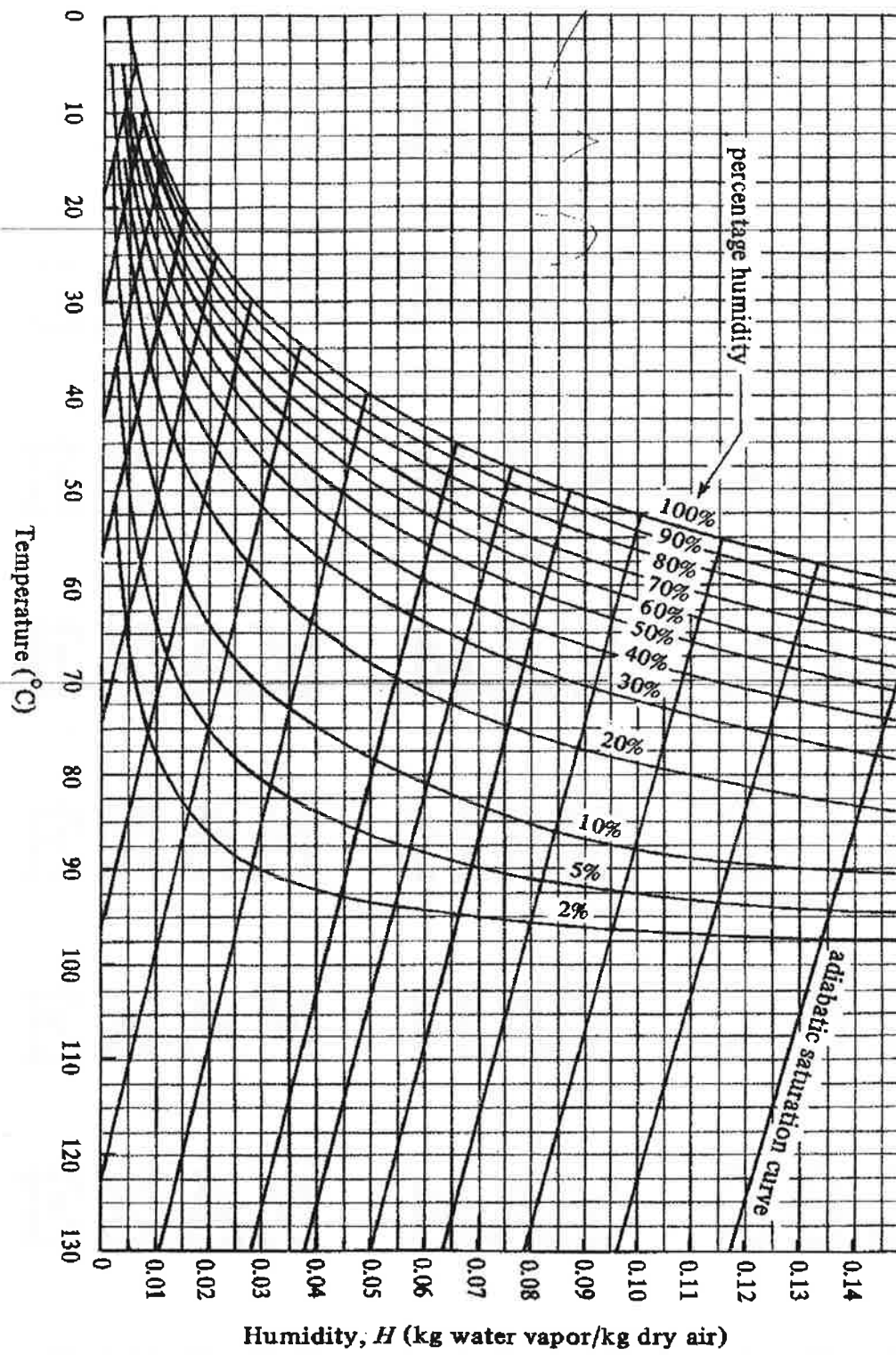
4. In the process of producing dried herbs, two proposed air dryer designs (parallel and perpendicular) will be evaluated. The herbs have an initial free moisture content of 0.25 kg H<sub>2</sub>O/kg dry solid. Both dryer types are designed to operate at a constant drying rate with a well-insulated oven and an exposed surface area of 35 m<sup>2</sup>. Air with an initial humidity of 0.018 kg water vapor/kg dry air at 50°C will be brought into contact with the wet herbs at a velocity of 1.15 m/s to remove 20% of the free moisture content.
- a. Differentiate between drying and evaporation process.  
[4 marks]
- b. Propose the best type of dryer that could yield high amount of dry herbs. Justify your answer with appropriate calculations.  
[16 marks]
- c. By using the best dryer configuration proposed in **part (b)**, describe the effect of air temperature towards the yield of dried herbs with relevant calculations.  
[6 marks]

– END OF PAPER –

Properties of Saturated Steam and Water (Steam Table), SI Units

| Temperature<br>(°C) | Vapor<br>Pressure<br>(kPa) | Specific Volume<br>(m <sup>3</sup> /kg) |             | Enthalpy<br>(kJ/kg) |             | Entropy<br>(kJ/kg·K) |             |
|---------------------|----------------------------|---|-------------|---------------------|-------------|----------------------|-------------|
|                     |                            | Liquid                                  | Sat'd Vapor | Liquid              | Sat'd Vapor | Liquid               | Sat'd Vapor |
| 0.01                | 0.6113                     | 0.0010002                               | 206.136     | 0.00                | 2501.4      | 0.0000               | 9.1562      |
| 3                   | 0.7577                     | 0.0010001                               | 168.132     | 12.57               | 2506.9      | 0.0457               | 9.0773      |
| 6                   | 0.9349                     | 0.0010001                               | 137.734     | 25.20               | 2512.4      | 0.0912               | 9.0003      |
| 9                   | 1.1477                     | 0.0010003                               | 113.386     | 37.80               | 2517.9      | 0.1362               | 8.9253      |
| 12                  | 1.4022                     | 0.0010005                               | 93.784      | 50.41               | 2523.4      | 0.1806               | 8.8524      |
| 15                  | 1.7051                     | 0.0010009                               | 77.926      | 62.99               | 2528.9      | 0.2245               | 8.7814      |
| 18                  | 2.0640                     | 0.0010014                               | 65.038      | 75.58               | 2534.4      | 0.2679               | 8.7123      |
| 21                  | 2.487                      | 0.0010020                               | 54.514      | 88.14               | 2539.9      | 0.3109               | 8.6450      |
| 24                  | 2.985                      | 0.0010027                               | 45.883      | 100.70              | 2545.4      | 0.3534               | 8.5794      |
| 25                  | 3.169                      | 0.0010029                               | 43.360      | 104.89              | 2547.2      | 0.3674               | 8.5580      |
| 27                  | 3.567                      | 0.0010035                               | 38.774      | 113.25              | 2550.8      | 0.3954               | 8.5156      |
| 30                  | 4.246                      | 0.0010043                               | 32.894      | 125.79              | 2556.3      | 0.4369               | 8.4533      |
| 33                  | 5.034                      | 0.0010053                               | 28.011      | 138.33              | 2561.7      | 0.4781               | 8.3927      |
| 36                  | 5.947                      | 0.0010063                               | 23.940      | 150.86              | 2567.1      | 0.5188               | 8.3336      |
| 40                  | 7.384                      | 0.0010078                               | 19.523      | 167.57              | 2574.3      | 0.5725               | 8.2570      |
| 45                  | 9.593                      | 0.0010099                               | 15.258      | 188.45              | 2583.2      | 0.6387               | 8.1648      |
| 50                  | 12.349                     | 0.0010121                               | 12.032      | 209.33              | 2592.1      | 0.7038               | 8.0763      |
| 55                  | 15.758                     | 0.0010146                               | 9.568       | 230.23              | 2600.9      | 0.7679               | 7.9913      |
| 60                  | 19.940                     | 0.0010172                               | 7.671       | 251.13              | 2609.6      | 0.8312               | 7.9096      |
| 65                  | 25.03                      | 0.0010199                               | 6.197       | 272.06              | 2618.3      | 0.8935               | 7.8310      |
| 70                  | 31.19                      | 0.0010228                               | 5.042       | 292.98              | 2626.8      | 0.9549               | 7.7553      |
| 75                  | 38.58                      | 0.0010259                               | 4.131       | 313.93              | 2635.3      | 1.0155               | 7.6824      |
| 80                  | 47.39                      | 0.0010291                               | 3.407       | 334.91              | 2643.7      | 1.0753               | 7.6122      |
| 85                  | 57.83                      | 0.0010325                               | 2.828       | 355.90              | 2651.9      | 1.1343               | 7.5445      |
| 90                  | 70.14                      | 0.0010360                               | 2.361       | 376.92              | 2660.1      | 1.1925               | 7.4791      |
| 95                  | 84.55                      | 0.0010397                               | 1.9819      | 397.96              | 2668.1      | 1.2500               | 7.4159      |
| 100                 | 101.35                     | 0.0010435                               | 1.6729      | 419.04              | 2676.1      | 1.3069               | 7.3549      |
| 105                 | 120.82                     | 0.0010475                               | 1.4194      | 440.15              | 2683.8      | 1.3630               | 7.2958      |
| 110                 | 143.27                     | 0.0010516                               | 1.2102      | 461.30              | 2691.5      | 1.4185               | 7.2387      |
| 115                 | 169.06                     | 0.0010559                               | 1.0366      | 482.48              | 2699.0      | 1.4734               | 7.1833      |
| 120                 | 198.53                     | 0.0010603                               | 0.8919      | 503.71              | 2706.3      | 1.5276               | 7.1296      |
| 125                 | 232.1                      | 0.0010649                               | 0.7706      | 524.99              | 2713.5      | 1.5813               | 7.0775      |
| 130                 | 270.1                      | 0.0010697                               | 0.6685      | 546.31              | 2720.5      | 1.6344               | 7.0269      |

Humidity Chart (air + water vapor mixture)



## Equations

| Parameters                 | Equations  |
|----------------------------|--|
| <b>Membrane Separation</b> |  |
| Conversion unit            | 1 Barrer = $10^{-10} \text{ cm}^3 \text{ (STP) cm} / (\text{cm}^2 \text{ s cmHg})$   |
| Permeate composition       | $y_p = \frac{\alpha_{AB} (x_o - r y_p)}{1 - y_p - (1 - x_o) - r (1 - y_p)}$  |
| Retentate composition      | $x_o = \frac{x_f - \theta y_p}{1 - \theta}$  |
| Membrane area              | $A_m = \frac{\theta L_r y_p}{(P_A/t) (p_h x_o - p_l y_p)}$   |
| Quadratic equations        | $y_p = \frac{-b + \sqrt{b^2 - 4ac}}{2a}$ $a = 1 - \alpha$ $b = -1 + \alpha + \frac{1}{r} + \frac{x_o}{r} (\alpha - 1)$ $c = \frac{-\alpha x_o}{r}$ |
| <b>Drying</b>              |  |
| Humid volume               | $v_H = (2.83 \times 10^{-3} + 4.56 \times 10^{-3} H) T \text{ K}$  |
| Heat transfer coefficient  | $h = 0.0204 G^{0.8} ; h = 1.17 G^{0.37}$   |
| Drying time                | $t = \frac{L_s}{AR_c} (X_1 - X_2)$   |
| Constant rate of drying    | $R_c = \frac{h}{\Delta H_w^{\text{vap}}} (T - T_w)$ $R_{c2} = R_{c1} \frac{H_{w2} - H_2}{H_{w1} - H_1} = R_{c1} \frac{T_2 - T_{w2}}{T_1 - H_{w1}}$ |
| Mass velocity              | $G = \frac{\mu_{\text{avg}}}{v_H}$   |

